# MORNINGSIDE DRIVE EXTENSION FROM FORT KING ROAD TO US HIGHWAY 301

# **ROUTE STUDY AND POND SITING** ANALYSIS AND REPORT **APPENDIX**

(Report 2 of 2)

Work Order No.: X11196.10 Task Order No.: EDO20-036



Pasco County Board of County Commissioners/ Pasco County Engineering Services/ **Project Management** 5418 Sunset Road New Port Richey, FL 34652-1733

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**APPENDIX 1 – SOILS REPORT** 



USDA United States Department of Agriculture

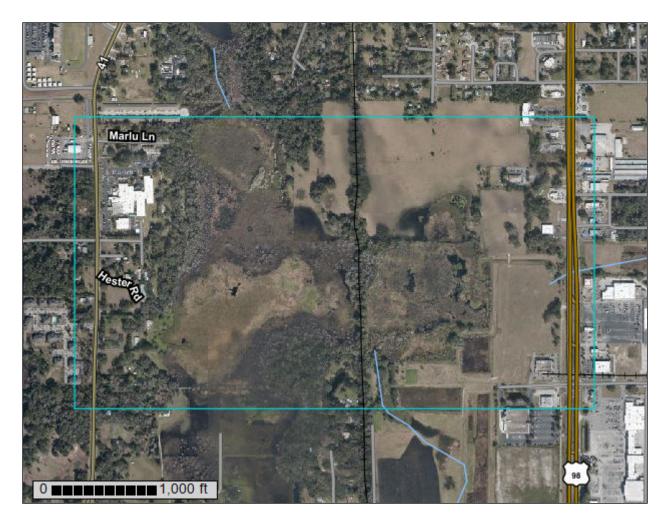
> Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# **Custom Soil Resource Report for** Pasco County, Florida

**Morningside Drive Extension** 



# Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2\_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

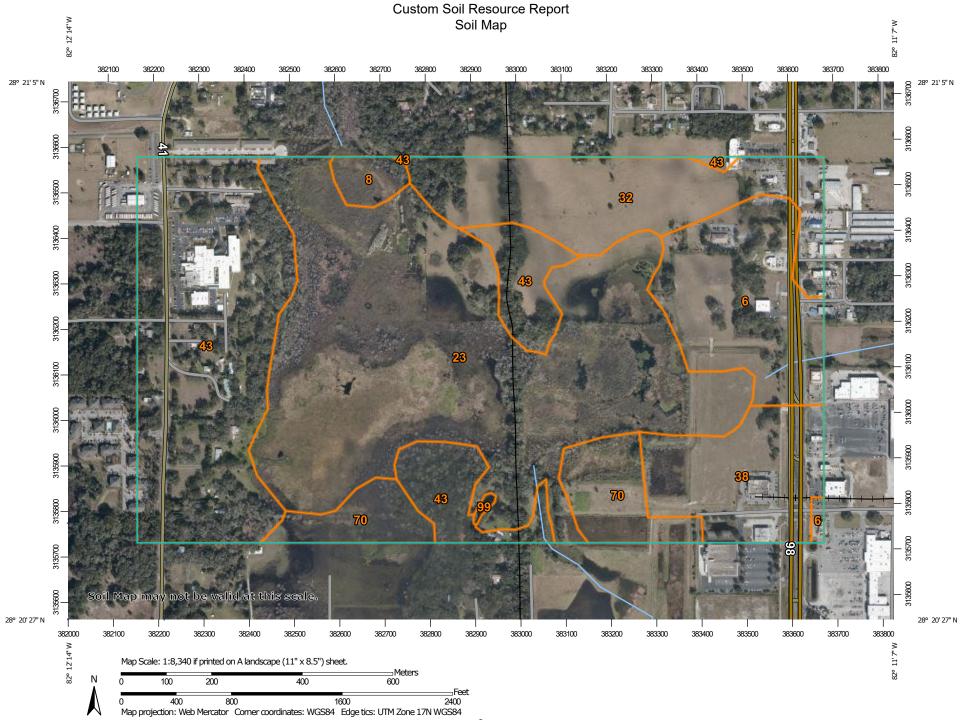
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND	)	MAP INFORMATION
Area of In	terest (AOI)	8	Spoil Area	The soil surveys that comprise your AOI were mapped at
	Area of Interest (AOI)	٥	Stony Spot	1:20,000.
Soils	Soil Map Unit Polygons	0	Very Stony Spot	Warning: Soil Map may not be valid at this scale.
~	Soil Map Unit Lines	Ŷ	Wet Spot	
	Soil Map Unit Points	$\triangle$	Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil
	·		Special Line Features	line placement. The maps do not show the small areas of
Special	Point Features Blowout	Water Fea	atures	contrasting soils that could have been shown at a more detailed scale.
×	Borrow Pit	$\sim$	Streams and Canals	
<u>م</u>	Clay Spot	Transpor	tation Rails	Please rely on the bar scale on each map sheet for map measurements.
$\diamond$	Closed Depression	~	Interstate Highways	
X	Gravel Pit	~	US Routes	Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
0 0 0	Gravelly Spot	~	Major Roads	Coordinate System: Web Mercator (EPSG:3857)
0	Landfill	~	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator
٨.	Lava Flow	Backgrou		projection, which preserves direction and shape but distorts
عله	Marsh or swamp	Buckgrou	Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more
Ŕ	Mine or Quarry			accurate calculations of distance or area are required.
0	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as
0	Perennial Water			of the version date(s) listed below.
$\sim$	Rock Outcrop			Soil Survey Area: Pasco County, Florida
+	Saline Spot			Survey Area Data: Version 19, Jun 9, 2020
0 0 0 0	Sandy Spot			Soil map units are labeled (as space allows) for map scales
-	Severely Eroded Spot			1:50,000 or larger.
0	Sinkhole			Date(s) aerial images were photographed: Jan 19, 2019—Jan
≯	Slide or Slip			29, 2019
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
6	Tavares sand, 0 to 5 percent slopes	31.4	9.8%		
8	Sellers mucky loamy fine sand	3.8	1.2%		
23	Basinger fine sand, depressional, 0 to 1 percent slopes	122.3	38.3%		
32	Lake fine sand, 0 to 5 percent slopes	35.4	11.1%		
38	Urban land, 0 to 2 percent slopes	23.8	7.5%		
43	Arredondo fine sand, 0 to 5 percent slopes	82.8	25.9%		
70	Placid fine sand	19.3	6.1%		
99	Water	0.4	0.1%		
Totals for Area of Interest		319.1	100.0%		

## Map Unit Legend

# Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit

descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

### Pasco County, Florida

#### 6—Tavares sand, 0 to 5 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2v173 Elevation: 0 to 180 feet Mean annual precipitation: 44 to 56 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Tavares and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Tavares**

#### Setting

Landform: Flats on marine terraces, ridges on marine terraces, knolls on marine terraces
 Landform position (two-dimensional): Shoulder, backslope
 Landform position (three-dimensional): Interfluve, base slope
 Down-slope shape: Convex
 Across-slope shape: Linear
 Parent material: Eolian or sandy marine deposits

#### **Typical profile**

*A - 0 to 7 inches:* sand *C - 7 to 80 inches:* sand

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 50.02 in/hr)
Depth to water table: About 42 to 72 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water capacity: Very low (about 1.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3s
Hydrologic Soil Group: A
Forage suitability group: Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL)
Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL)

Hydric soil rating: No

#### **Minor Components**

#### Apopka

Percent of map unit: 6 percent

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Shoulder, summit, footslope Landform position (three-dimensional): Nose slope, side slope, crest Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) Hydric soil rating: No

#### Candler

Percent of map unit: 4 percent

Landform: Ridges on marine terraces, knolls on marine terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Interfluve, side slope, tread

*Down-slope shape:* Convex

Across-slope shape: Convex

*Other vegetative classification:* Longleaf Pine-Turkey Oak Hills (R155XY002FL), Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G155XB111FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL)

Hydric soil rating: No

#### Adamsville

Percent of map unit: 3 percent Landform: Knolls on flatwoods, rises on flatwoods Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, rise, talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Upland Hardwood Hammock (R154XY008FL), Upland Hardwood Hammock (R155XY008FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL) Hydric soil rating: No

#### Zolfo

Percent of map unit: 2 percent Landform: Flats on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on rises and knolls of mesic uplands (G154XB131FL) Hydric soil rating: No

#### 8-Sellers mucky loamy fine sand

#### Map Unit Setting

National map unit symbol: bvcf Elevation: 0 to 180 feet Mean annual precipitation: 50 to 58 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 324 to 354 days Farmland classification: Not prime farmland

#### Map Unit Composition

Sellers and similar soils: 95 percent Minor components: 5 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Sellers**

#### Setting

Landform: Drainageways on marine terraces, depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy marine deposits

#### **Typical profile**

A1 - 0 to 9 inches: mucky loamy fine sand A2 - 9 to 24 inches: fine sand C - 24 to 80 inches: fine sand

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water capacity: Low (about 5.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A/D Forage suitability group: Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL) *Other vegetative classification:* Freshwater Marshes and Ponds (R154XY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL) *Hydric soil rating:* Yes

#### **Minor Components**

#### Basinger, depressional

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL) Hydric soil rating: Yes

#### 23—Basinger fine sand, depressional, 0 to 1 percent slopes

#### Map Unit Setting

National map unit symbol: 2v16t Elevation: 0 to 150 feet Mean annual precipitation: 48 to 56 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 287 to 317 days Farmland classification: Not prime farmland

#### Map Unit Composition

Basinger, depressional, and similar soils: 92 percent Minor components: 8 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Basinger, Depressional**

#### Setting

Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy marine deposits

#### **Typical profile**

A - 0 to 3 inches: fine sand E - 3 to 8 inches: fine sand E/Bh - 8 to 24 inches: fine sand C - 24 to 80 inches: fine sand

#### **Properties and qualities**

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 50.02 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water capacity: Low (about 4.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Forage suitability group: Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL)
Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL)
Hydric soil rating: Yes

#### **Minor Components**

#### Smyrna

Percent of map unit: 3 percent Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Ecological site: R155XY003FL - South Florida Flatwoods Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

#### Immokalee, hydric

Percent of map unit: 3 percent Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Linear Ecological site: R154XY003FL - South Florida Flatwoods Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G154XB141FL) Hydric soil rating: Yes

#### Floridana, hydric

Percent of map unit: 2 percent Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Sandy over loamy soils on stream terraces, flood plains, or in depressions (G154XB245FL) Hydric soil rating: Yes

#### 32—Lake fine sand, 0 to 5 percent slopes

#### Map Unit Setting

National map unit symbol: 2v17f Elevation: 10 to 200 feet Mean annual precipitation: 44 to 56 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Lake and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Lake**

#### Setting

Landform: Ridges on marine terraces, hills on marine terraces Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear Parent material: Eolian deposits or sandy marine deposits

#### **Typical profile**

A - 0 to 9 inches: fine sand

C - 9 to 80 inches: fine sand

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 50.02 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water capacity: Very low (about 3.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4s Hydrologic Soil Group: A Forage suitability group: Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) *Other vegetative classification:* Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) *Hydric soil rating:* No

#### **Minor Components**

#### Arredondo

Percent of map unit: 8 percent Landform: Ridges on marine terraces, hills on marine terraces Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope, interfluve Down-slope shape: Convex, linear Across-slope shape: Convex Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) Hydric soil rating: No

#### Tavares

Percent of map unit: 5 percent Landform: Ridges on marine terraces, flats on marine terraces Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Interfluve Down-slope shape: Convex, linear Across-slope shape: Linear, convex Other vegetative classification: Sandy soils on rises, knolls, and ridges of mesic uplands (G155XB121FL) Hydric soil rating: No

#### Jonesville

Percent of map unit: 2 percent Landform: Rises on marine terraces Landform position (two-dimensional): Backslope Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Shallow or moderately deep, sandy or loamy soils on rises and ridges of mesic uplands (G154XB521FL) Hydric soil rating: No

#### 38—Urban land, 0 to 2 percent slopes

#### Map Unit Setting

National map unit symbol: 2x9fc Elevation: 0 to 200 feet Mean annual precipitation: 40 to 68 inches Mean annual air temperature: 68 to 79 degrees F Frost-free period: 345 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Urban land:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Urban Land**

#### Setting

Landform: Flatwoods on marine terraces, hills on marine terraces, ridges on marine terraces, knolls on marine terraces, rises on marine terraces Landform position (two-dimensional): Summit, backslope Landform position (three-dimensional): Interfluve, side slope, riser, talf, rise Down-slope shape: Linear, convex Across-slope shape: Linear Parent material: No parent material

#### Interpretive groups

Land capability classification (irrigated): None specified Forage suitability group: Forage suitability group not assigned (G155XB999FL) Other vegetative classification: Forage suitability group not assigned (G155XB999FL) Hydric soil rating: Unranked

#### **Minor Components**

#### Matlacha

Percent of map unit: 3 percent Landform: Flats on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: Forage suitability group not assigned (G155XB999FL) Hydric soil rating: No

#### St. augustine

Percent of map unit: 3 percent Landform: Marine terraces Landform position (three-dimensional): Tread, rise Down-slope shape: Linear Across-slope shape: Convex Other vegetative classification: Forage suitability group not assigned (G155XB999FL) Hydric soil rating: No

#### Воса

Percent of map unit: 1 percent

Landform: Drainageways on marine terraces, flats on marine terraces

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Linear, convex

Across-slope shape: Concave, linear

*Other vegetative classification:* South Florida Flatwoods (R155XY003FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

#### Immokalee

Percent of map unit: 1 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Riser, talf

Down-slope shape: Linear

Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

#### Paola

Percent of map unit: 1 percent Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Backslope, summit Landform position (three-dimensional): Side slope, interfluve, riser Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: Sand Pine Scrub (R155XY001FL), Sandy soils on ridges and dunes of xeric uplands (G155XB111FL) Hydric soil rating: No

#### Hallandale

Percent of map unit: 1 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Linear Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: Yes

#### Myakka

Percent of map unit: 1 percent

Landform: Drainageways on flatwoods on marine terraces

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Linear

Across-slope shape: Concave, linear

*Other vegetative classification:* South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) *Hydric soil rating:* No

#### Apopka

Percent of map unit: 1 percent Landform: Hills on marine terraces, ridges on marine terraces Landform position (two-dimensional): Summit, backslope Landform position (three-dimensional): Interfluve, side slope, riser Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R155XY002FL), Sandy soils on ridges and dunes of xeric uplands (G155XB111FL) Hydric soil rating: No

#### Pomello

Percent of map unit: 1 percent Landform: Ridges on marine terraces, knolls on marine terraces Landform position (two-dimensional): Backslope, summit Landform position (three-dimensional): Side slope, interfluve, riser Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: Sand Pine Scrub (R155XY001FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL) Hydric soil rating: No

#### Adamsville

Percent of map unit: 1 percent Landform: Rises on marine terraces, knolls on marine terraces Landform position (three-dimensional): Tread, rise Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Upland Hardwood Hammock (R155XY008FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL) Hydric soil rating: No

#### Eaugallie

Percent of map unit: 1 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

#### 43—Arredondo fine sand, 0 to 5 percent slopes

#### Map Unit Setting

National map unit symbol: 2w0q0 Elevation: 30 to 160 feet Mean annual precipitation: 44 to 56 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 290 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Arredondo and similar soils:* 82 percent *Minor components:* 18 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Arredondo**

#### Setting

Landform: Hills on marine terraces, ridges on marine terraces Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope, interfluve, riser Down-slope shape: Linear, convex Across-slope shape: Linear, convex Parent material: Sandy marine deposits and/or loamy marine deposits

#### **Typical profile**

A - 0 to 8 inches: fine sand E - 8 to 62 inches: fine sand Bt1 - 62 to 69 inches: loamy fine sand Bt2 - 69 to 80 inches: sandy clay

#### **Properties and qualities**

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water capacity: Low (about 3.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3s
Hydrologic Soil Group: A
Forage suitability group: Sandy soils on ridges and dunes of xeric uplands (G154XB111FL)
Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL)
Hydric soil rating: No

#### **Minor Components**

#### Candler

Percent of map unit: 7 percent Landform: Ridges on marine terraces, knolls on marine terraces Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, tread Down-slope shape: Convex, linear Across-slope shape: Concave, convex, linear Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) Hydric soil rating: No

#### Lake

Percent of map unit: 5 percent Landform: Ridges, hills, marine terraces Landform position (three-dimensional): Interfluve Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) Hydric soil rating: No

#### Sparr

Percent of map unit: 4 percent

#### **Custom Soil Resource Report**

Landform: Rises on marine terraces, flats on marine terraces Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: Sandy soils on rises and knolls of mesic uplands (G154XB131FL) Hydric soil rating: No

#### Fort meade

Percent of map unit: 2 percent Landform: Ridges on marine terraces Landform position (three-dimensional): Interfluve Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: Sandy soils on ridges and dunes of xeric uplands (G154XB111FL) Hydric soil rating: No

#### 70—Placid fine sand

#### Map Unit Setting

National map unit symbol: bvc6 Elevation: 50 to 210 feet Mean annual precipitation: 50 to 58 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 324 to 354 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Placid and similar soils:* 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Placid**

#### Setting

Landform: Drainageways on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Concave Parent material: Sandy marine deposits

#### **Typical profile**

*A - 0 to 18 inches:* fine sand *C - 18 to 80 inches:* fine sand

#### Properties and qualities

Slope: 0 to 2 percent Depth to restrictive feature: More than 80 inches Drainage class: Very poorly drained Runoff class: High

#### **Custom Soil Resource Report**

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum: 4.0
Available water capacity: Moderate (about 6.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Forage suitability group: Sandy soils on flats of mesic or hydric lowlands (G154XB141FL)
Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL), Sandy soils on flats of mesic or hydric lowlands (G154XB141FL)

Hydric soil rating: Yes

#### **Minor Components**

#### Basinger

Percent of map unit: 10 percent Landform: Drainageways on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Concave Other vegetative classification: Slough (R154XY011FL), Sandy soils on flats of mesic or hydric lowlands (G154XB141FL) Hydric soil rating: Yes

#### Samsula

Percent of map unit: 10 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL), Organic soils in depressions and on flood plains (G154XB645FL) Hydric soil rating: Yes

#### 99—Water

#### Map Unit Composition

*Water (fresh):* 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Water (fresh)**

#### Interpretive groups Land capability classification (irrigated): None specified

 Forage suitability group: Forage suitability group not assigned (G154XB999FL)
 Other vegetative classification: Forage suitability group not assigned (G154XB999FL)
 Hydric soil rating: Unranked

# Soil Information for All Uses

## **Soil Reports**

The Soil Reports section includes various formatted tabular and narrative reports (tables) containing data for each selected soil map unit and each component of each unit. No aggregation of data has occurred as is done in reports in the Soil Properties and Qualities and Suitabilities and Limitations sections.

The reports contain soil interpretive information as well as basic soil properties and qualities. A description of each report (table) is included.

## **Construction Materials**

This folder contains a collection of tabular reports that present soil interpretations related to sources of construction materials. The reports (tables) include all selected map units and components for each map unit, limiting features and interpretive ratings. Construction materials interpretations are tools designed to provide guidance to users in selecting a site for potential source of various materials. Individual soils or groups of soils may be selected as a potential source because they are close at hand, are the only source available, or they meets some or all of the physical or chemical properties required for the intended application. Example interpretations include roadfill, sand and gravel, topsoil and reclamation material.

### Source of Reclamation Material, Roadfill, and Topsoil

This table gives information about the soils as potential sources of reclamation material, roadfill, and topsoil. Normal compaction, minor processing, and other standard construction practices are assumed.

The soils are rated *good*, *fair*, or *poor* as potential sources of reclamation material, roadfill, and topsoil. The features that limit the soils as sources of these materials are specified in the table. Numerical ratings between 0.00 and 0.99 are given after the specified features. These numbers indicate the degree to which the features limit the soils as sources of topsoil, reclamation material, or roadfill. The lower the number, the greater the limitation.

*Reclamation material* is used in areas that have been drastically disturbed by surface mining or similar activities. When these areas are reclaimed, layers of soil material or unconsolidated geological material, or both, are replaced in a vertical sequence. The reconstructed soil favors plant growth. The ratings in the table do

not apply to quarries and other mined areas that require an offsite source of reconstruction material. The ratings are based on the soil properties that affect erosion and stability of the surface and the productive potential of the reconstructed soil. These properties include the content of sodium, salts, and calcium carbonate; reaction; available water capacity; erodibility; texture; content of rock fragments; and content of organic matter and other features that affect fertility.

*Roadfill* is soil material that is excavated in one place and used in road embankments in another place. In this table, the soils are rated as a source of roadfill for low embankments, generally less than 6 feet high and less exacting in design than higher embankments. The ratings are for the whole soil, from the surface to a depth of about 5 feet. It is assumed that soil layers will be mixed when the soil material is excavated and spread.

The ratings are based on the amount of suitable material and on soil properties that affect the ease of excavation and the performance of the material after it is in place. The thickness of the suitable material is a major consideration. The ease of excavation is affected by large stones, depth to a water table, and slope. How well the soil performs in place after it has been compacted and drained is determined by its strength (as inferred from the AASHTO classification of the soil) and linear extensibility (shrink-swell potential).

*Topsoil* is used to cover an area so that vegetation can be established and maintained. The upper 40 inches of a soil is evaluated for use as topsoil. Also evaluated is the reclamation potential of the borrow area. The ratings are based on the soil properties that affect plant growth; the ease of excavating, loading, and spreading the material; and reclamation of the borrow area. Toxic substances, soil reaction, and the properties that are inferred from soil texture, such as available water capacity and fertility, affect plant growth. The ease of excavating, loading, and spreading is affected by rock fragments, slope, depth to a water table, soil texture, and thickness of suitable material. Reclamation of the borrow area is affected by slope, depth to a water table, rock fragments, depth to bedrock or a cemented pan, and toxic material.

The surface layer of most soils is generally preferred for topsoil because of its organic matter content. Organic matter greatly increases the absorption and retention of moisture and nutrients for plant growth.

Information in this table is intended for land use planning, for evaluating land use alternatives, and for planning site investigations prior to design and construction. The information, however, has limitations. For example, estimates and other data generally apply only to that part of the soil between the surface and a depth of 5 to 7 feet. Because of the map scale, small areas of different soils may be included within the mapped areas of a specific soil.

The information is not site specific and does not eliminate the need for onsite investigation of the soils or for testing and analysis by personnel experienced in the design and construction of engineering works.

Government ordinances and regulations that restrict certain land uses or impose specific design criteria were not considered in preparing the information in this table. Local ordinances and regulations should be considered in planning, in site selection, and in design.

### Report—Source of Reclamation Material, Roadfill, and Topsoil

[Onsite investigation may be needed to validate the interpretations in this table and to confirm the identity of the soil on a given site. The numbers in the value columns range from 0.00 to 0.99. The smaller the value, the greater the limitation]

Source of Reclamation Material, Roadfill, and Topsoil–Pasco County, Florida										
Map symbol and soil name	Pct. of map	Potential as a sour reclamation mate		Potential as a sou roadfill	rce of	Potential as a source of topsoil				
	unit	Rating class and limiting features	Value	Rating class and limiting features	Value	Rating class and limiting features	Value			
6—Tavares sand, 0 to 5 percent slopes										
Tavares	85	Poor		Good		Poor				
		Too sandy	0.00			Too sandy	0.00			
		Wind erosion	0.00			Exchange capacity	0.24			
		Droughty	0.00			Too acid	0.99			
		Low content of organic matter	0.07							
		Too acid	0.50							
8—Sellers mucky loamy fine sand										
Sellers	95	Poor		Poor		Poor				
		Too sandy	0.00	Wetness	0.00	Wetness	0.00			
		Wind erosion	0.00			Too sandy	0.00			
		Low content of organic matter	0.13			Exchange capacity	0.49			
		Too acid	0.50			Too acid	0.60			
23—Basinger fine sand, depressional, 0 to 1 percent slopes										
Basinger, depressional	92	Poor		Poor		Poor				
		Too sandy	0.00	Wetness	0.00	Wetness	0.00			
		Wind erosion	0.00			Too sandy	0.00			
		Low content of organic matter	0.05			Exchange capacity	0.30			
		Too acid	0.68							

Source of Reclamation Material, Roadfill, and Topsoil–Pasco County, Florida         Map symbol and soil       Pct. of       Potential as a source of       Potential as a source of										
name	map	reclamation mate		roadfill	rce of	topsoil				
	unit	Rating class and limiting features	Value	Rating class and limiting features	Value	Rating class and limiting features	Value			
32—Lake fine sand, 0 to 5 percent slopes										
Lake	85	Poor		Good		Poor				
		Too sandy	0.00			Too sandy	0.00			
		Wind erosion	0.00			Exchange capacity	0.36			
		Low content of organic matter	0.21			Too acid	0.88			
		Droughty	0.25							
		Too acid	0.50							
38—Urban land, 0 to 2 percent slopes										
Urban land	85	Not rated		Not rated		Not rated				
43—Arredondo fine sand, 0 to 5 percent slopes										
Arredondo	82	Poor		Good		Poor				
		Too sandy	0.00			Too sandy	0.00			
		Wind erosion	0.00			Exchange capacity	0.15			
		Low content of organic matter	0.13			Too acid	0.98			
		Too acid	0.54							
70—Placid fine sand										
Placid	80	Poor		Poor		Poor				
		Too sandy	0.00	Wetness	0.00	Wetness	0.00			
		Wind erosion	0.00			Too sandy	0.00			
		Low content of organic matter	0.13			Exchange capacity	0.34			
		Too acid	0.50			Too acid	0.83			
99—Water										
Water (fresh)	100	Not rated		Not rated		Not rated				

## **Soil Chemical Properties**

This folder contains a collection of tabular reports that present soil chemical properties. The reports (tables) include all selected map units and components for each map unit. Soil chemical properties are measured or inferred from direct observations in the field or laboratory. Examples of soil chemical properties include pH, cation exchange capacity, calcium carbonate, gypsum, and electrical conductivity.

### **Chemical Soil Properties**

This table shows estimates of some chemical characteristics and features that affect soil behavior. These estimates are given for the layers of each soil in the survey area. The estimates are based on field observations and on test data for these and similar soils.

Depth to the upper and lower boundaries of each layer is indicated.

*Cation-exchange capacity* is the total amount of extractable cations that can be held by the soil, expressed in terms of milliequivalents per 100 grams of soil at neutrality (pH 7.0) or at some other stated pH value. Soils having a low cation-exchange capacity hold fewer cations and may require more frequent applications of fertilizer than soils having a high cation-exchange capacity. The ability to retain cations reduces the hazard of ground-water pollution.

*Effective cation-exchange capacity* refers to the sum of extractable cations plus aluminum expressed in terms of milliequivalents per 100 grams of soil. It is determined for soils that have pH of less than 5.5.

*Soil reaction* is a measure of acidity or alkalinity. It is important in selecting crops and other plants, in evaluating soil amendments for fertility and stabilization, and in determining the risk of corrosion.

*Calcium carbonate* equivalent is the percent of carbonates, by weight, in the fraction of the soil less than 2 millimeters in size. The availability of plant nutrients is influenced by the amount of carbonates in the soil.

*Gypsum* is expressed as a percent, by weight, of hydrated calcium sulfates in the fraction of the soil less than 20 millimeters in size. Gypsum is partially soluble in water. Soils that have a high content of gypsum may collapse if the gypsum is removed by percolating water.

Salinity is a measure of soluble salts in the soil at saturation. It is expressed as the electrical conductivity of the saturation extract, in millimhos per centimeter at 25 degrees C. Estimates are based on field and laboratory measurements at representative sites of nonirrigated soils. The salinity of irrigated soils is affected by the quality of the irrigation water and by the frequency of water application. Hence, the salinity of soils in individual fields can differ greatly from the value given in the table. Salinity affects the suitability of a soil for crop production, the stability of soil if used as construction material, and the potential of the soil to corrode metal and concrete.

Sodium adsorption ratio (SAR) is a measure of the amount of sodium (Na) relative to calcium (Ca) and magnesium (Mg) in the water extract from saturated soil paste. It is the ratio of the Na concentration divided by the square root of one-half of the Ca + Mg concentration. Soils that have SAR values of 13 or more may be characterized by an increased dispersion of organic matter and clay particles, reduced saturated hydraulic conductivity and aeration, and a general degradation of soil structure.

Chemical Soil Properties–Pasco County, Florida									
Map symbol and soil name	Depth	Cation- exchange capacity	Effective cation- exchange capacity	Soil reaction	Calcium carbonate	Gypsum	Salinity	Sodium adsorption ratio	
	In	meq/100g	meq/100g	pН	Pct	Pct	mmhos/cm		
6—Tavares sand, 0 to 5 percent slopes									
Tavares	0-7	_	0.7-1.3	3.5-6.0	0	0	0.0-2.0	0-4	
	7-80	1.0-2.8	—	3.5-6.0	0	0	0.0-2.0	0-4	
8—Sellers mucky loamy fine sand									
Sellers	0-9	_	0.6-7.3	3.5-5.5	0	0	0.0-2.0	0-4	
	9-24	_	0.4-4.2	3.5-5.5	0	0	0.0-2.0	0-4	
	24-80	_	0.1-4.9	3.5-5.5	0	0	0.0-2.0	0-4	
23—Basinger fine sand, depressional, 0 to 1 percent slopes									
Basinger, depressional	0-3	0.1-4.1	_	3.5-7.3	0	0	0.0-2.0	0-4	
	3-8	0.1-3.4	_	3.5-7.3	0	0	0.0-2.0	0-4	
	8-24	0.1-4.5	_	3.5-7.3	0	0	0.0-2.0	0-4	
	24-80	0.1-2.6	_	3.5-7.3	0	0	0.0-2.0	0-4	
32—Lake fine sand, 0 to 5 percent slopes									
Lake	0-9	_	1.4-3.2	4.5-5.5	0	0	0.0-2.0	0-4	
	9-80	_	0.4-2.0	4.5-5.5	0	0	0.0-2.0	0-4	
38—Urban land, 0 to 2 percent slopes									
Urban land	_	_	_	_	_	_	_	_	

Chemical Soil Properties–Pasco County, Florida									
Map symbol and soil name	Depth	Cation- exchange capacity	Effective cation- exchange capacity	Soil reaction	Calcium carbonate	Gypsum	Salinity	Sodium adsorption ratio	
	In	meq/100g	meq/100g	pН	Pct	Pct	mmhos/cm		
43—Arredondo fine sand, 0 to 5 percent slopes									
Arredondo	0-8	—	0.2-1.6	4.5-6.0	0	0	0.0-2.0	0-4	
	8-62	—	0.0-2.8	4.5-6.0	0	0	0.0-2.0	0-4	
	62-69	—	1.9-4.2	4.5-6.0	0	0	0.0-2.0	0-4	
	69-80	—	2.9-9.7	4.5-6.0	0	0	0.0-2.0	0-4	
70—Placid fine sand									
Placid	0-18	—	0.1-7.7	3.5-6.0	0	0	0.0-2.0	0-4	
	18-80	—	0.0-4.9	3.5-6.5	0	0	0.0-2.0	0-4	
99—Water									
Water (fresh)	—	—	_	_	—	-	—	_	

## **Soil Physical Properties**

This folder contains a collection of tabular reports that present soil physical properties. The reports (tables) include all selected map units and components for each map unit. Soil physical properties are measured or inferred from direct observations in the field or laboratory. Examples of soil physical properties include percent clay, organic matter, saturated hydraulic conductivity, available water capacity, and bulk density.

## **Engineering Properties**

This table gives the engineering classifications and the range of engineering properties for the layers of each soil in the survey area.

Hydrologic soil group is a group of soils having similar runoff potential under similar storm and cover conditions. The criteria for determining Hydrologic soil group is found in the National Engineering Handbook, Chapter 7 issued May 2007(http:// directives.sc.egov.usda.gov/OpenNonWebContent.aspx?content=17757.wba). Listing HSGs by soil map unit component and not by soil series is a new concept for the engineers. Past engineering references contained lists of HSGs by soil series. Soil series are continually being defined and redefined, and the list of soil series names changes so frequently as to make the task of maintaining a single national list virtually impossible. Therefore, the criteria is now used to calculate the HSG using the component soil properties and no such national series lists will be maintained. All such references are obsolete and their use should be discontinued. Soil properties that influence runoff potential are those that influence the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to a seasonal high water table, saturated hydraulic conductivity after prolonged wetting, and depth to a layer with a very slow water transmission rate. Changes in soil properties caused by land management or climate changes also cause the hydrologic soil group to change. The influence of ground cover is treated independently. There are four hydrologic soil groups, A, B, C, and D, and three dual groups, A/D, B/D, and C/D. In the dual groups, the first letter is for drained areas and the second letter is for undrained areas.

The four hydrologic soil groups are described in the following paragraphs:

*Group A.* Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

*Group B.* Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

*Group C.* Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

*Group D.* Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell

potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

Depth to the upper and lower boundaries of each layer is indicated.

*Texture* is given in the standard terms used by the U.S. Department of Agriculture. These terms are defined according to percentages of sand, silt, and clay in the fraction of the soil that is less than 2 millimeters in diameter. "Loam," for example, is soil that is 7 to 27 percent clay, 28 to 50 percent silt, and less than 52 percent sand. If the content of particles coarser than sand is 15 percent or more, an appropriate modifier is added, for example, "gravelly."

*Classification* of the soils is determined according to the Unified soil classification system (ASTM, 2005) and the system adopted by the American Association of State Highway and Transportation Officials (AASHTO, 2004).

The Unified system classifies soils according to properties that affect their use as construction material. Soils are classified according to particle-size distribution of the fraction less than 3 inches in diameter and according to plasticity index, liquid limit, and organic matter content. Sandy and gravelly soils are identified as GW, GP, GM, GC, SW, SP, SM, and SC; silty and clayey soils as ML, CL, OL, MH, CH, and OH; and highly organic soils as PT. Soils exhibiting engineering properties of two groups can have a dual classification, for example, CL-ML.

The AASHTO system classifies soils according to those properties that affect roadway construction and maintenance. In this system, the fraction of a mineral soil that is less than 3 inches in diameter is classified in one of seven groups from A-1 through A-7 on the basis of particle-size distribution, liquid limit, and plasticity index. Soils in group A-1 are coarse grained and low in content of fines (silt and clay). At the other extreme, soils in group A-7 are fine grained. Highly organic soils are classified in group A-8 on the basis of visual inspection.

If laboratory data are available, the A-1, A-2, and A-7 groups are further classified as A-1-a, A-1-b, A-2-4, A-2-5, A-2-6, A-2-7, A-7-5, or A-7-6. As an additional refinement, the suitability of a soil as subgrade material can be indicated by a group index number. Group index numbers range from 0 for the best subgrade material to 20 or higher for the poorest.

*Percentage of rock fragments* larger than 10 inches in diameter and 3 to 10 inches in diameter are indicated as a percentage of the total soil on a dry-weight basis. The percentages are estimates determined mainly by converting volume percentage in the field to weight percentage. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

*Percentage (of soil particles) passing designated sieves* is the percentage of the soil fraction less than 3 inches in diameter based on an ovendry weight. The sieves, numbers 4, 10, 40, and 200 (USA Standard Series), have openings of 4.76, 2.00, 0.420, and 0.074 millimeters, respectively. Estimates are based on laboratory tests of soils sampled in the survey area and in nearby areas and on estimates made in the field. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

*Liquid limit* and *plasticity index* (Atterberg limits) indicate the plasticity characteristics of a soil. The estimates are based on test data from the survey area or from nearby areas and on field examination. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

References:

American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.

American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.

Absence of an entry indicates that the data were not estimated. The asterisk '\*' denotes the representative texture; other possible textures follow the dash. The criteria for determining the hydrologic soil group for individual soil components is found in the National Engineering Handbook, Chapter 7 issued May 2007(http://directives.sc.egov.usda.gov/ OpenNonWebContent.aspx?content=17757.wba). Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

				Enginee	ring Propert	ies–Pasco C	ounty, Flo	orida						
Map unit symbol and	Pct. of	Hydrolo	Depth	USDA texture	Classi	fication	Pct Fra	igments	Percent	age passi	ng sieve r	number—	Liquid	Plasticit
soil name	map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200	limit	y index
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
6—Tavares sand, 0 to 5 percent slopes														
Tavares	85	A	0-7	Sand	SM, SP- SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	95-98-1 00	73-79-1 00	5-14- 15	0-0 -14	NP
			7-80	Sand	SP-SM, SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	95-98-1 00	73-79-1 00	5-12- 13	0-0 -16	NP-0 -1
8—Sellers mucky loamy fine sand														
Sellers	95	A/D	0-9	Mucky loamy fine sand	SM, SP- SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	85-93-1 00	5-13- 20	0-7 -14	NP
			9-24	Sand, fine sand, loamy fine sand	SM, SP- SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	85-93-1 00	5-13- 20	0-7 -14	NP
			24-80	Sand, fine sand, loamy fine sand	SM, SP- SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	85-93-1 00	5-13- 20	0-7 -14	NP
23—Basinger fine sand, depressional, 0 to 1 percent slopes														
Basinger, depressional	92	A/D	0-3	Fine sand	SP-SM	A-2-4	0- 0- 0	0- 0- 0	100-100 -100	95-100- 100	87-89- 96	2-12- 12	0-0 -33	NP-0 -1
			3-8	Fine sand	SP, SP- SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	95-100- 100	87-91- 96	2- 8- 12	0-0 -17	NP-0 -1
			8-24	Fine sand	SP, SP- SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	95-100- 100	88-90- 97	2-10- 13	0-0 -21	NP-0 -2
			24-80	Fine sand	SP, SP- SM	A-3	0- 0- 0	0- 0- 0	100-100 -100	95-100- 100	89-91- 95	2- 8- 10	0-0 -14	NP

	Engineering Properties–Pasco County, Florida													
Map unit symbol and	Pct. of map unit	Hydrolo	Depth	USDA texture	Class	ification	Pct Fra	gments	Percenta	age passi	ng sieve r	number—	Liquid	Plasticit
soil name		gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200	limit	y index
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
32—Lake fine sand, 0 to 5 percent slopes														
Lake	85	А	0-9	Fine sand	SP-SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	85-85-1 00	7- 9- 11	0-14 -24	NP-1 -1
			9-80	Fine sand	SP-SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	85-85-1 00	5- 9- 11	0-10 -18	NP-1 -1
43—Arredondo fine sand, 0 to 5 percent slopes														
Arredondo	82	A	0-8	Fine sand	SM, SP- SM	A-3, A-2-4	0- 0- 0	0- 0- 0	95-100- 100	92-100- 100	83-96-1 00	10-17- 20	0-17 -22	NP-1 -3
			8-62	Fine sand	SM, SP- SM	A-3, A-2-4	0- 0- 0	0- 0- 0	95-100- 100	92-100- 100	82-96-1 00	8-11- 16	0-15 -19	NP-1 -3
			62-69	Loamy sand, sandy loam, loamy fine sand, fine sandy loam	SC-SM, SC	A-2-4, A-2-6	0- 0- 0	0- 0- 0	95-100- 100	92-100- 100	85-96-1 00	16-20- 29	20-24 -29	6-8 -12
			69-80	Sandy loam, sandy clay, sandy clay loam	SC	A-6, A-7-6, A-2-4	0- 0- 0	0- 0- 0	95-100- 100	92-100- 100	82-97-1 00	31-41- 49	25-45 -48	9-26-28
70—Placid fine sand														
Placid	80	A/D	0-18	Fine sand	SM, SP, SP-SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	90-95-1 00	1-11- 20	0-7 -14	NP
			18-80	Sand, fine sand, loamy fine sand	SM, SP, SP-SM	A-2-4, A-3	0- 0- 0	0- 0- 0	100-100 -100	100-100 -100	90-95-1 00	1-11- 20	0-7 -14	NP

### **Physical Soil Properties**

This table shows estimates of some physical characteristics and features that affect soil behavior. These estimates are given for the layers of each soil in the survey area. The estimates are based on field observations and on test data for these and similar soils.

Depth to the upper and lower boundaries of each layer is indicated.

Particle size is the effective diameter of a soil particle as measured by sedimentation, sieving, or micrometric methods. Particle sizes are expressed as classes with specific effective diameter class limits. The broad classes are sand, silt, and clay, ranging from the larger to the smaller.

*Sand* as a soil separate consists of mineral soil particles that are 0.05 millimeter to 2 millimeters in diameter. In this table, the estimated sand content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

*Silt* as a soil separate consists of mineral soil particles that are 0.002 to 0.05 millimeter in diameter. In this table, the estimated silt content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

*Clay* as a soil separate consists of mineral soil particles that are less than 0.002 millimeter in diameter. In this table, the estimated clay content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

The content of sand, silt, and clay affects the physical behavior of a soil. Particle size is important for engineering and agronomic interpretations, for determination of soil hydrologic qualities, and for soil classification.

The amount and kind of clay affect the fertility and physical condition of the soil and the ability of the soil to adsorb cations and to retain moisture. They influence shrink-swell potential, saturated hydraulic conductivity (Ksat), plasticity, the ease of soil dispersion, and other soil properties. The amount and kind of clay in a soil also affect tillage and earthmoving operations.

*Moist bulk density* is the weight of soil (ovendry) per unit volume. Volume is measured when the soil is at field moisture capacity, that is, the moisture content at 1/3- or 1/10-bar (33kPa or 10kPa) moisture tension. Weight is determined after the soil is dried at 105 degrees C. In the table, the estimated moist bulk density of each soil horizon is expressed in grams per cubic centimeter of soil material that is less than 2 millimeters in diameter. Bulk density data are used to compute linear extensibility, shrink-swell potential, available water capacity, total pore space, and other soil properties. The moist bulk density of a soil indicates the pore space available for water and roots. Depending on soil texture, a bulk density of more than 1.4 can restrict water storage and root penetration. Moist bulk density is influenced by texture, kind of clay, content of organic matter, and soil structure.

Saturated hydraulic conductivity (Ksat) refers to the ease with which pores in a saturated soil transmit water. The estimates in the table are expressed in terms of micrometers per second. They are based on soil characteristics observed in the field, particularly structure, porosity, and texture. Saturated hydraulic conductivity (Ksat) is considered in the design of soil drainage systems and septic tank absorption fields.

Available water capacity refers to the quantity of water that the soil is capable of storing for use by plants. The capacity for water storage is given in inches of water per inch of soil for each soil layer. The capacity varies, depending on soil properties that affect retention of water. The most important properties are the content of organic matter, soil texture, bulk density, and soil structure. Available water capacity is an important factor in the choice of plants or crops to be grown and in the design and management of irrigation systems. Available water capacity is not an estimate of the quantity of water actually available to plants at any given time.

*Linear extensibility* refers to the change in length of an unconfined clod as moisture content is decreased from a moist to a dry state. It is an expression of the volume change between the water content of the clod at 1/3- or 1/10-bar tension (33kPa or 10kPa tension) and oven dryness. The volume change is reported in the table as percent change for the whole soil. The amount and type of clay minerals in the soil influence volume change.

Linear extensibility is used to determine the shrink-swell potential of soils. The shrink-swell potential is low if the soil has a linear extensibility of less than 3 percent; moderate if 3 to 6 percent; high if 6 to 9 percent; and very high if more than 9 percent. If the linear extensibility is more than 3, shrinking and swelling can cause damage to buildings, roads, and other structures and to plant roots. Special design commonly is needed.

*Organic matter* is the plant and animal residue in the soil at various stages of decomposition. In this table, the estimated content of organic matter is expressed as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter. The content of organic matter in a soil can be maintained by returning crop residue to the soil.

Organic matter has a positive effect on available water capacity, water infiltration, soil organism activity, and tilth. It is a source of nitrogen and other nutrients for crops and soil organisms.

*Erosion factors* are shown in the table as the K factor (Kw and Kf) and the T factor. Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and Ksat. Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

*Erosion factor Kw* indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

*Erosion factor Kf* indicates the erodibility of the fine-earth fraction, or the material less than 2 millimeters in size.

*Erosion factor T* is an estimate of the maximum average annual rate of soil erosion by wind and/or water that can occur without affecting crop productivity over a sustained period. The rate is in tons per acre per year.

*Wind erodibility groups* are made up of soils that have similar properties affecting their susceptibility to wind erosion in cultivated areas. The soils assigned to group 1 are the most susceptible to wind erosion, and those assigned to group 8 are the least susceptible. The groups are described in the "National Soil Survey Handbook."

*Wind erodibility index* is a numerical value indicating the susceptibility of soil to wind erosion, or the tons per acre per year that can be expected to be lost to wind erosion. There is a close correlation between wind erosion and the texture of the surface layer, the size and durability of surface clods, rock fragments, organic matter, and a calcareous reaction. Soil moisture and frozen soil layers also influence wind erosion.

#### Reference:

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. (http://soils.usda.gov)

	Physical Soil Properties–Pasco County, Florida													
Map symbol and soil name	Depth	th Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter	Erosion factors			Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	т	group	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
6—Tavares sand, 0 to 5 percent slopes														
Tavares	0-7	93-94- 96	2- 4- 5	2- 2- 2	1.58-1.59- 1.60	42.34-198.00-3 53.00	0.02-0.04-0.1	0.1- 0.1- 0.1	0.5- 1.5- 2.0	.10	.10	5	1	220
	7-80	95-96- 97	1- 2- 3	1- 2- 3	1.62-1.64- 1.66	42.34-198.00-3 53.00	0.01-0.03-0.0 5	0.1- 0.1- 0.3	0.0- 0.2- 0.5	.05	.05			
8—Sellers mucky loamy fine sand														
Sellers	0-9	-78-	0-16- 30	1- 6- 10	1.25-1.40- 1.55	42.00-92.00-14 1.00	0.15-0.18-0.2 0	0.0- 1.5- 2.9	5.0- 7.5-10. 0	.15	.15	5	2	134
	9-24	-93-	0- 1- 15	1- 6- 10	1.30-1.43- 1.55	42.00-92.00-14 1.00	0.10-0.13-0.1 5	0.0- 1.5- 2.9	1.0- 1.5- 2.0	.02	.02			
	24-80	-93-	0- 1- 15	1- 6- 10	1.45-1.58- 1.70	42.00-92.00-14 1.00	0.03-0.06-0.0 8	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.02	.02			

Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

	Physical Soil Properties–Pasco County, Florida													
Map symbol and soil name	Depth	Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter	Erosion factors			Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	Т	group	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
23—Basinger fine sand, depressional, 0 to 1 percent slopes														
Basinger, depressional	0-3	90-92-100	0- 5- 10	0- 3- 4	1.40-1.48- 1.55	42.34-91.74-35 3.00	0.03-0.07-0.1 0	0.0- 0.3- 0.5	0.5- 4.5- 8.0	.05	.05	5	1	250
	3-8	90-98-100	0- 1- 10	0- 1- 4	1.40-1.48- 1.55	42.34-91.74-35 3.00	0.03-0.07-0.1 0	0.0- 0.2- 0.4	0.0- 0.3- 0.8	.02	.02			
	8-24	90-96-100	0- 1- 9	0- 3- 5	1.40-1.53- 1.79	42.34-91.74-35 3.00	0.03-0.09-0.1 5	0.0- 0.2- 0.4	0.1- 1.3- 2.0	.02	.02			
	24-80	95-98-100	0- 1- 4	0- 1- 3	1.50-1.60- 1.70	42.34-91.74-35 3.00	0.03-0.07-0.1 0	0.0- 0.1- 0.3	0.0- 0.2- 0.5	.02	.02			
32—Lake fine sand, 0 to 5 percent slopes														
Lake	0-9	92-95- 97	0- 2- 5	2- 3- 4	1.50-1.51- 1.52	42.34-197.67-3 53.00	0.05-0.05-0.1 4	0.2- 0.2- 0.3	1.5- 2.1- 3.6	.02	.02	5	1	250
	9-80	92-94- 97	0- 2- 5	2- 4- 4	1.60-1.64- 1.68	42.34-197.67-3 53.00	0.05-0.05-0.1 2	0.1- 0.2- 0.3	0.1- 0.3- 1.1	.02	.02			
38—Urban land, 0 to 2 percent slopes														
Urban land	_	_	-	_	-	_	_	-	-					

					Physic	al Soil Properties	s–Pasco Coun	ty, Florida						
Map symbol and soil name	Depth	Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter		Erosic factor		Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	т	group	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
43—Arredondo fine sand, 0 to 5 percent slopes														
Arredondo	0-8	85-90- 99	0- 6- 10	1- 4- 7	1.56-1.57- 1.58	42.00-92.00-14 1.00	0.05-0.07-0.0 8	0.1- 0.2- 0.4	0.0- 1.0- 2.0	.05	.05	5	1	250
	8-62	85-95- 99	0- 2- 10	1- 3- 7	1.56-1.58- 1.60	42.00-92.00-14 1.00	0.05-0.06-0.0 8	0.0- 0.2- 0.6	0.0- 0.3- 0.5	.02	.02			
	62-69	65-86- 90	0- 1- 21	10-13- 18	1.62-1.65- 1.68	14.00-28.00-42. 00	0.10-0.12-0.1 5	0.5- 0.7- 1.0	0.0- 0.3- 0.5	.10	.10			
	69-80	55-62- 80	0- 1- 20	15-37- 40	1.62-1.66- 1.71	4.00-23.00-42.0 0	0.12-0.13-0.1 7	0.7- 1.8- 2.1	0.0- 0.3- 0.5	.05	.05			
70—Placid fine sand														
Placid	0-18	-94-	0- 1- 15	0- 5- 10	1.20-1.30- 1.40	42.00-92.00-14 1.00	0.15-0.18-0.2 0	0.0- 1.5- 2.9	2.0- 6.0-10. 0	.02	.02	5	1	250
	18-80	-94-	0- 1- 15	0- 5- 10	1.30-1.45- 1.60	42.00-92.00-14 1.00	0.05-0.07-0.0 8	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.02	.02			
99—Water														
Water (fresh)	_	—	_	_	_	—	_	_	_					

## **Water Features**

This folder contains tabular reports that present soil hydrology information. The reports (tables) include all selected map units and components for each map unit. Water Features include ponding frequency, flooding frequency, and depth to water table.

## Hydrologic Soil Group and Surface Runoff

This table gives estimates of various soil water features. The estimates are used in land use planning that involves engineering considerations.

*Hydrologic soil groups* are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The four hydrologic soil groups are:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas.

*Surface runoff* refers to the loss of water from an area by flow over the land surface. Surface runoff classes are based on slope, climate, and vegetative cover. The concept indicates relative runoff for very specific conditions. It is assumed that the surface of the soil is bare and that the retention of surface water resulting from irregularities in the ground surface is minimal. The classes are negligible, very low, low, medium, high, and very high.

#### Report—Hydrologic Soil Group and Surface Runoff

Absence of an entry indicates that the data were not estimated. The dash indicates no documented presence.

Hydrologic Soil Group and Surface Runoff–Pasco County, Florida									
Map symbol and soil name	Pct. of map unit	Surface Runoff	Hydrologic Soil Group						
6—Tavares sand, 0 to 5 percent slopes									
Tavares	85	Negligible	A						
8—Sellers mucky loamy fine sand									
Sellers	95	Negligible	A/D						
23—Basinger fine sand, depressional, 0 to 1 percent slopes									
Basinger, depressional	92	Negligible	A/D						
32—Lake fine sand, 0 to 5 percent slopes									
Lake	85	Very low	A						
38—Urban land, 0 to 2 percent slopes									
Urban land	85	Very high	—						
43—Arredondo fine sand, 0 to 5 percent slopes									
Arredondo	82	Very low	A						
70—Placid fine sand									
Placid	80	High	A/D						
99—Water									
Water (fresh)	100		_						

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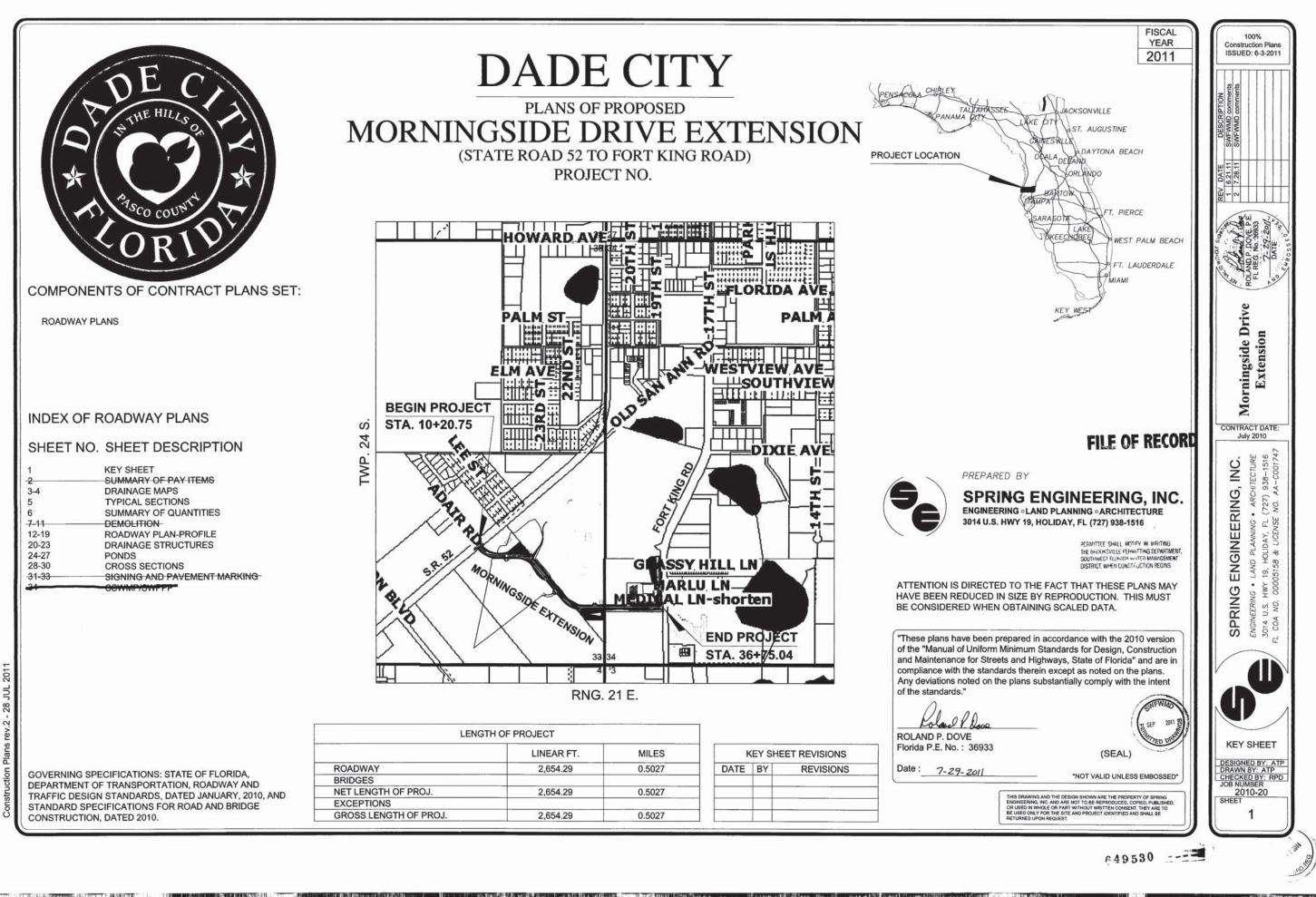
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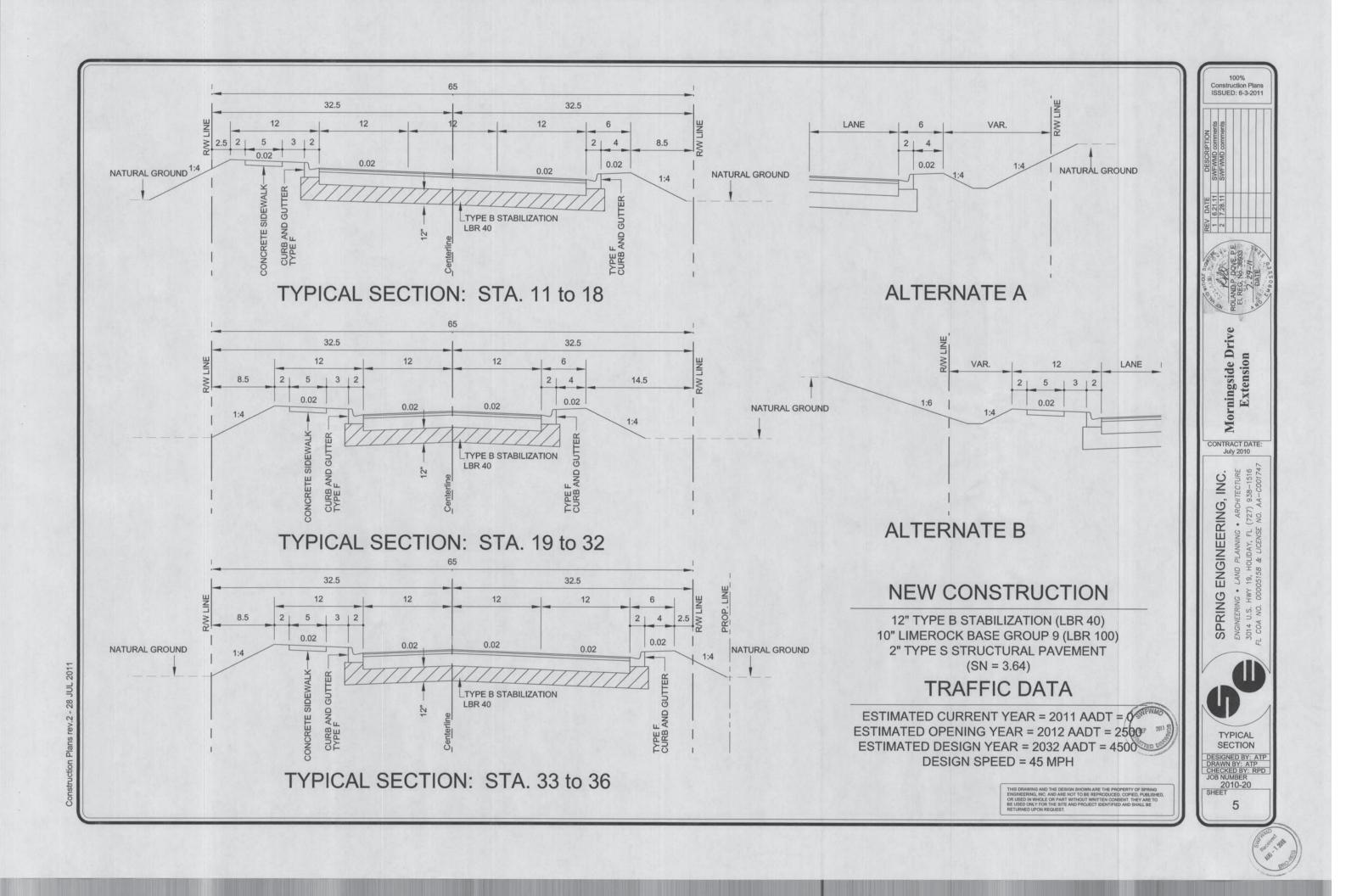
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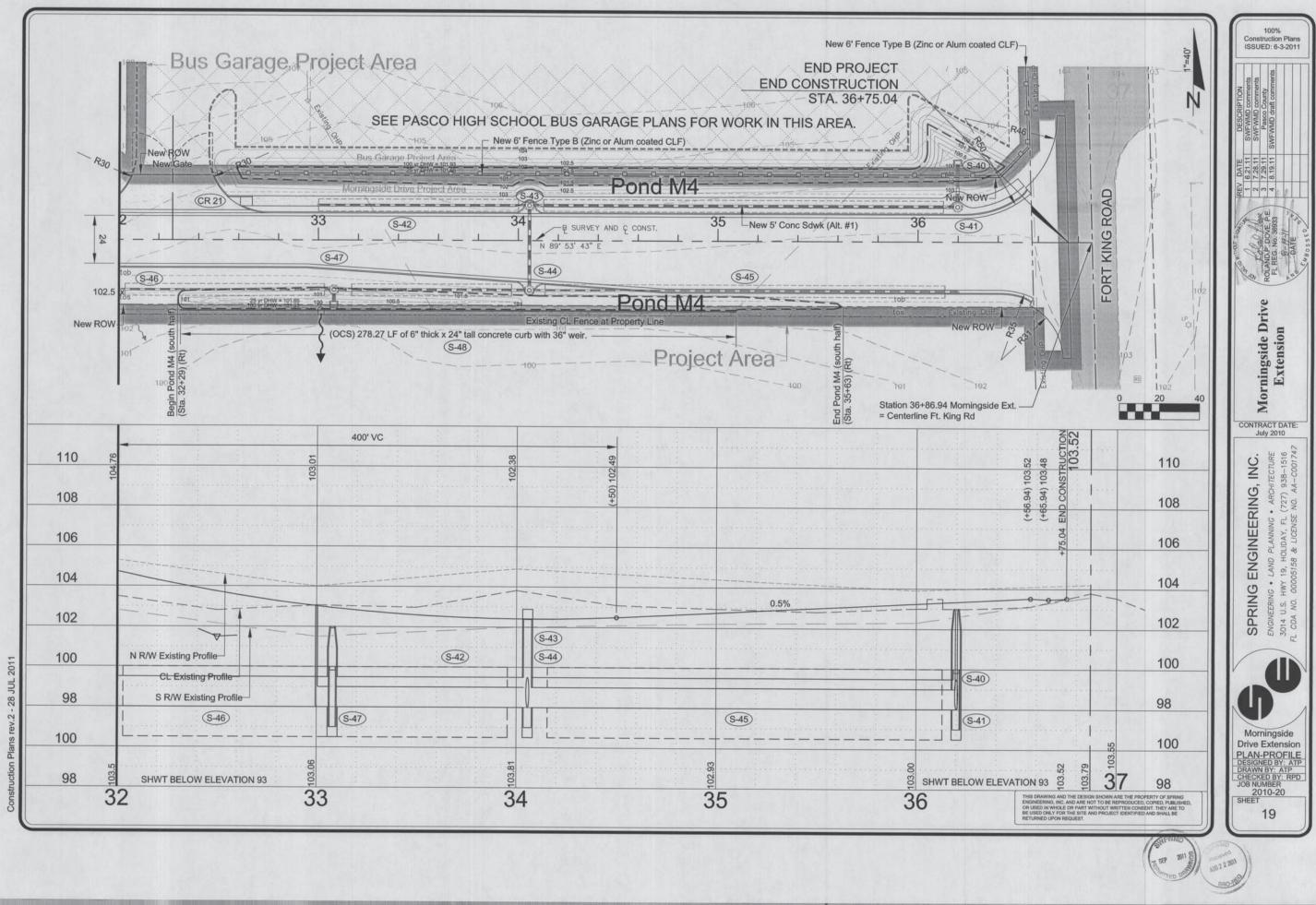
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## APPENDIX 2 – MORNINGSIDE DRIVE WEST PLANS EXCERPT







## **APPENDIX 3 – ROADWAY PLANS EXCERPT FOR US 301**

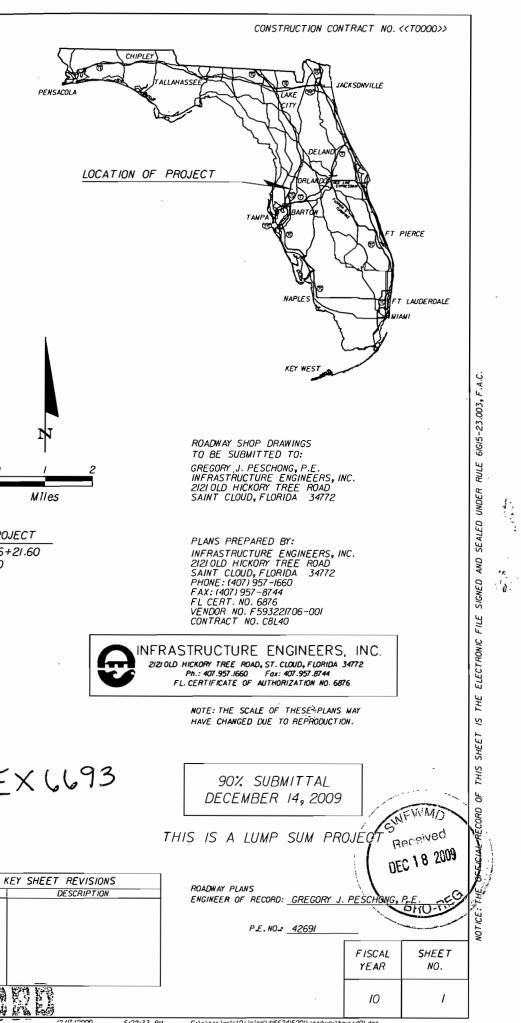
#### COMPONENTS OF CONTRACT PLANS SET

SIGNING AND PAVEMENT MARKING PLANS SIGNALIZATION PLANS

A DETAILED INDEX APPEARS ON THE KEY SHEET OF EACH COMPONENT

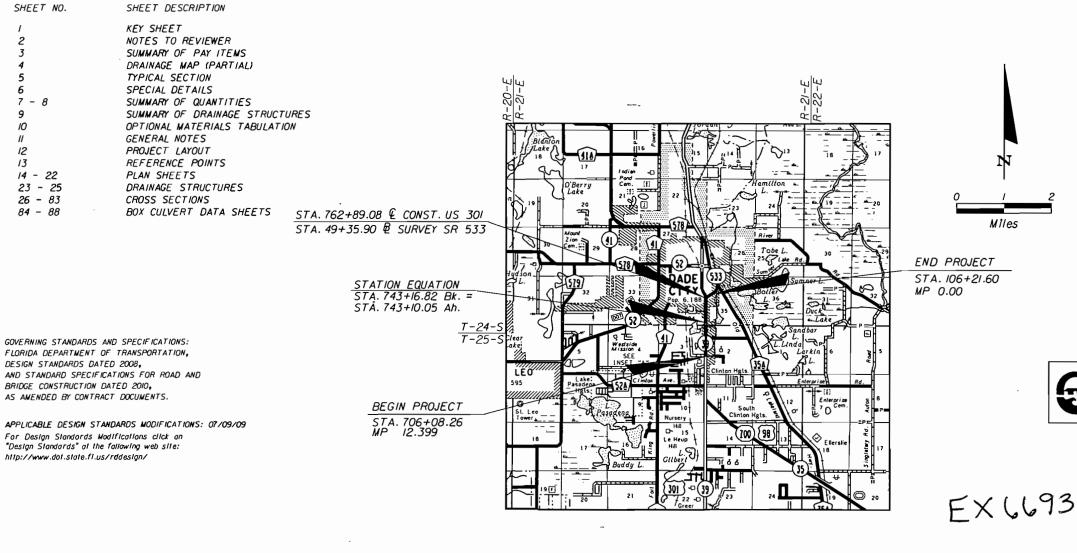
INDEX OF ROADWAY PLANS

# STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION



## CONTRACT PLANS

FINANCIAL PROJECT ID 416624-1-52-01 PASCO COUNTY (14050) STATE ROAD NO. 41 (US301)



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PROJECT LENGTH IS BASED ON €	0F	CONSTRUCT IO
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LENGTH (	OF PROJE	СT
	LINEAR FEET	MILES
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BRIDGES	-	-
NET LENGTH OF PROJECT	6007.13	1.138
EXCEPTIONS	-	-
GROSS LENGTH OF PROJECT	6007.13	1.138
FDOT PROJECT MANAGER: STE	PHANIE PIERCE	IR MB

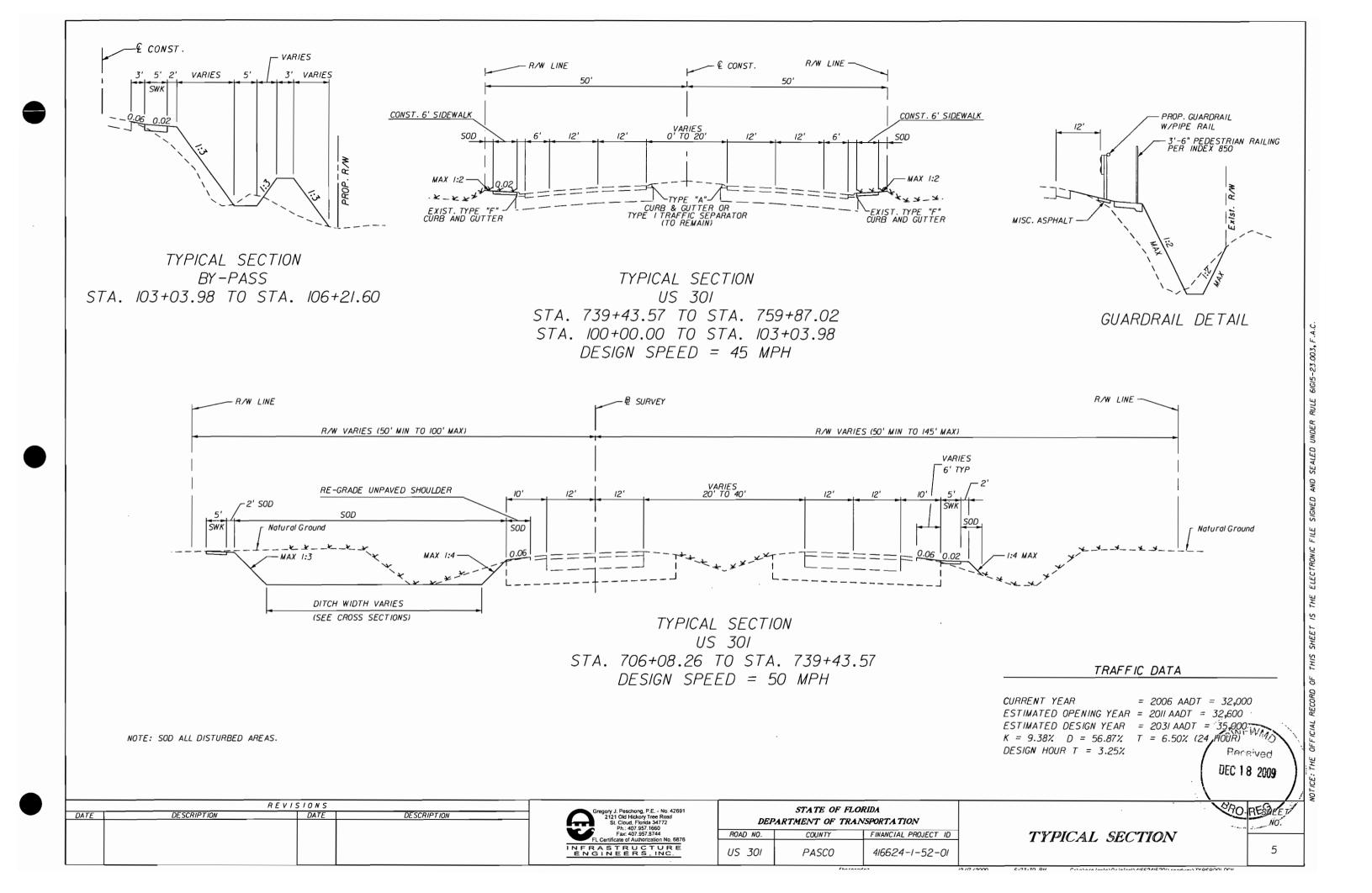


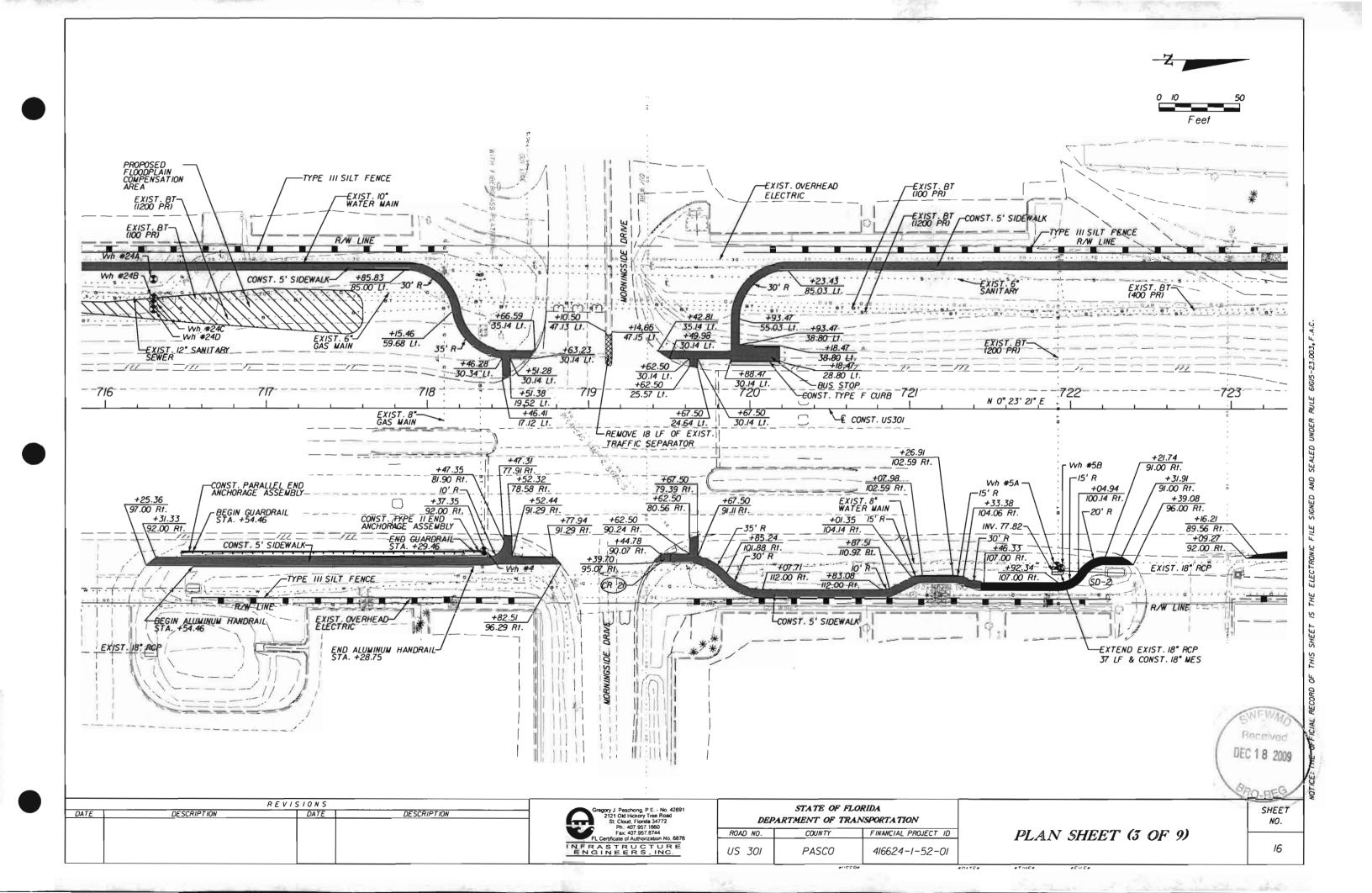
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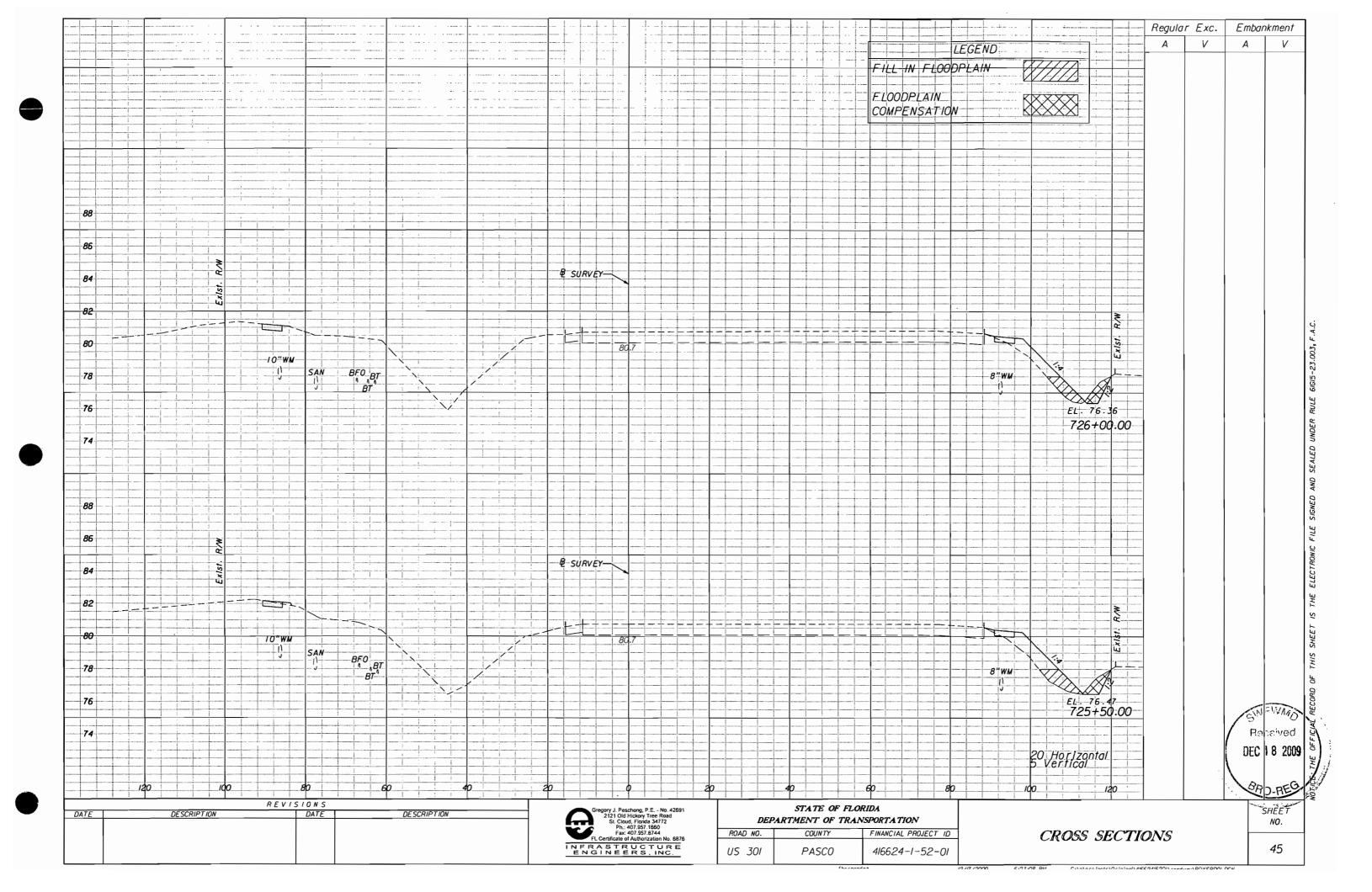
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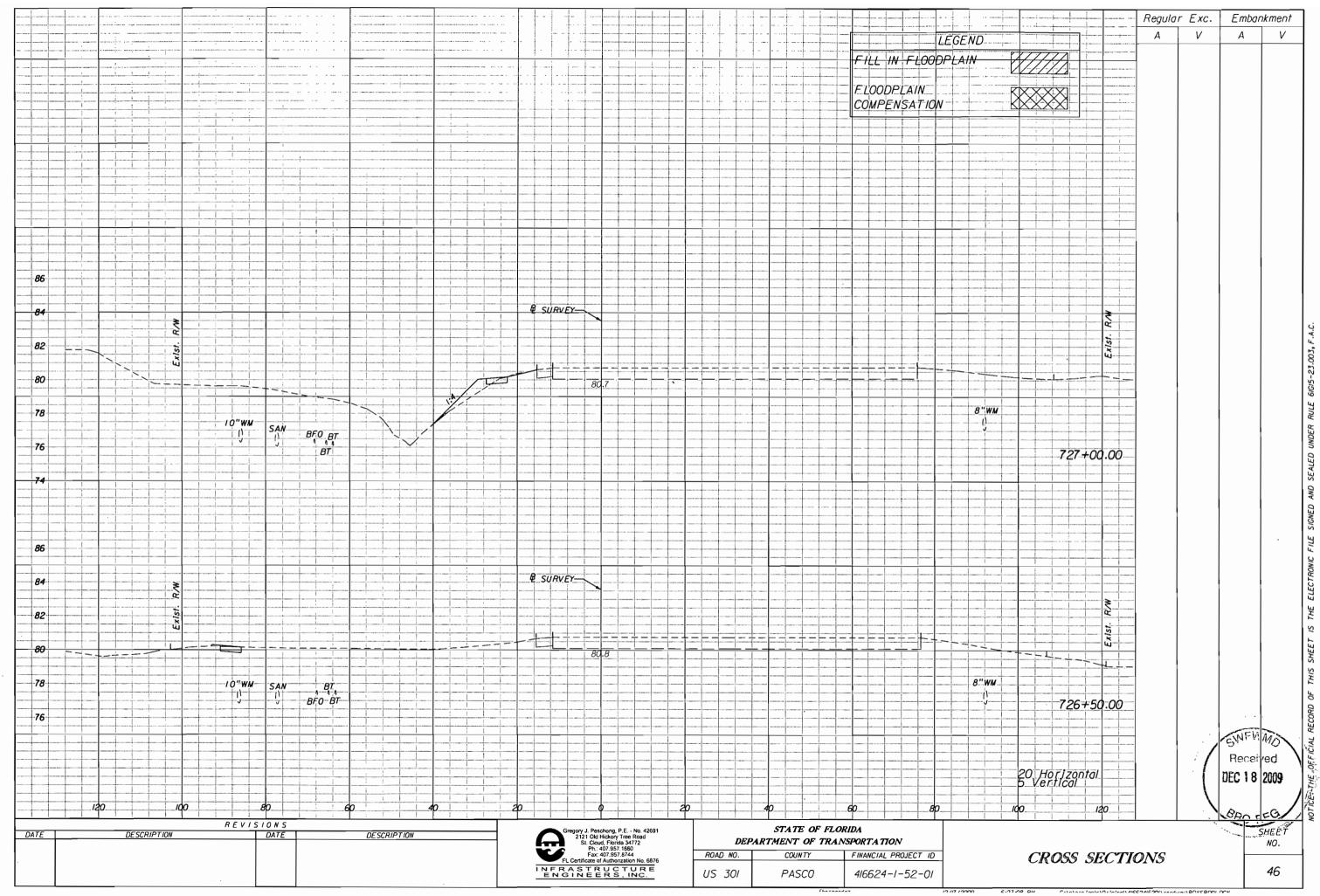
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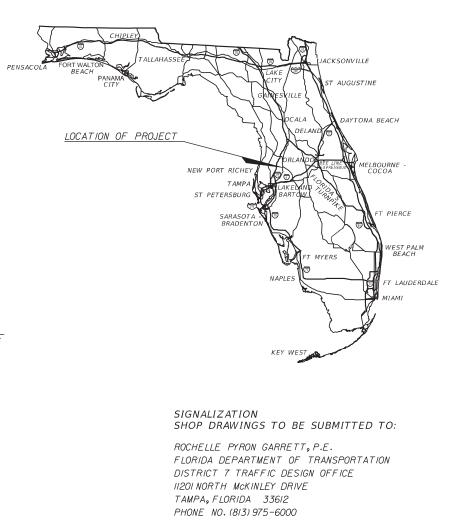






# APPENDIX 4 – MDS & US 301 SIGNAL PLAN EXCERPT

## STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION



## CONTRACT PLANS

FINANCIAL PROJECT ID 431243-1-52-01 FINANCIAL PROJECT ID 431243-1-52-02 (FEDERAL FUNDS) PASCO COUNTY (14050)

STATE ROAD NO. 39/700/35 (US 301/98) FROM NORTH OF KOSSIK ROAD TO BOUGAINVILLEA AVENUE

## SIGNALIZATION PLANS

#### INDEX OF SIGNALIZATION PLANS

SHEET NO.	SHEET DESCRIPTION
$\begin{array}{cccccccc} T-1 \\ T-2 \\ T-3 \\ T-9A &- T-9C \\ T-9A &- T-9C \\ T-10 &- T-13 \\ T-14 \\ T-15 &- T-16 \\ T-17 \\ T-18 &- T-21 \\ T-22 \\ T-23 \\ T-24 \end{array}$	KEY SHEET TABULATION OF QUANTITIES GENERAL NOTE SHEET SIGNALIZATION PLAN SHEET PORTABLE TRAFFIC MONITORING SITE GUIDE SIGN WORK SHEET CONCRETE STRAIN POLE SCHEDULE SIGN BRACKET ARM ASSEMBLY SIGN BRACKET ARM SIGN PANEL DETAILS REPORT OF CORE BORINGS LIGHTING GENERAL NOTE SHEET POLE DATA AND LEGEND SHEET SERVICE POINT DETAIL SHEET

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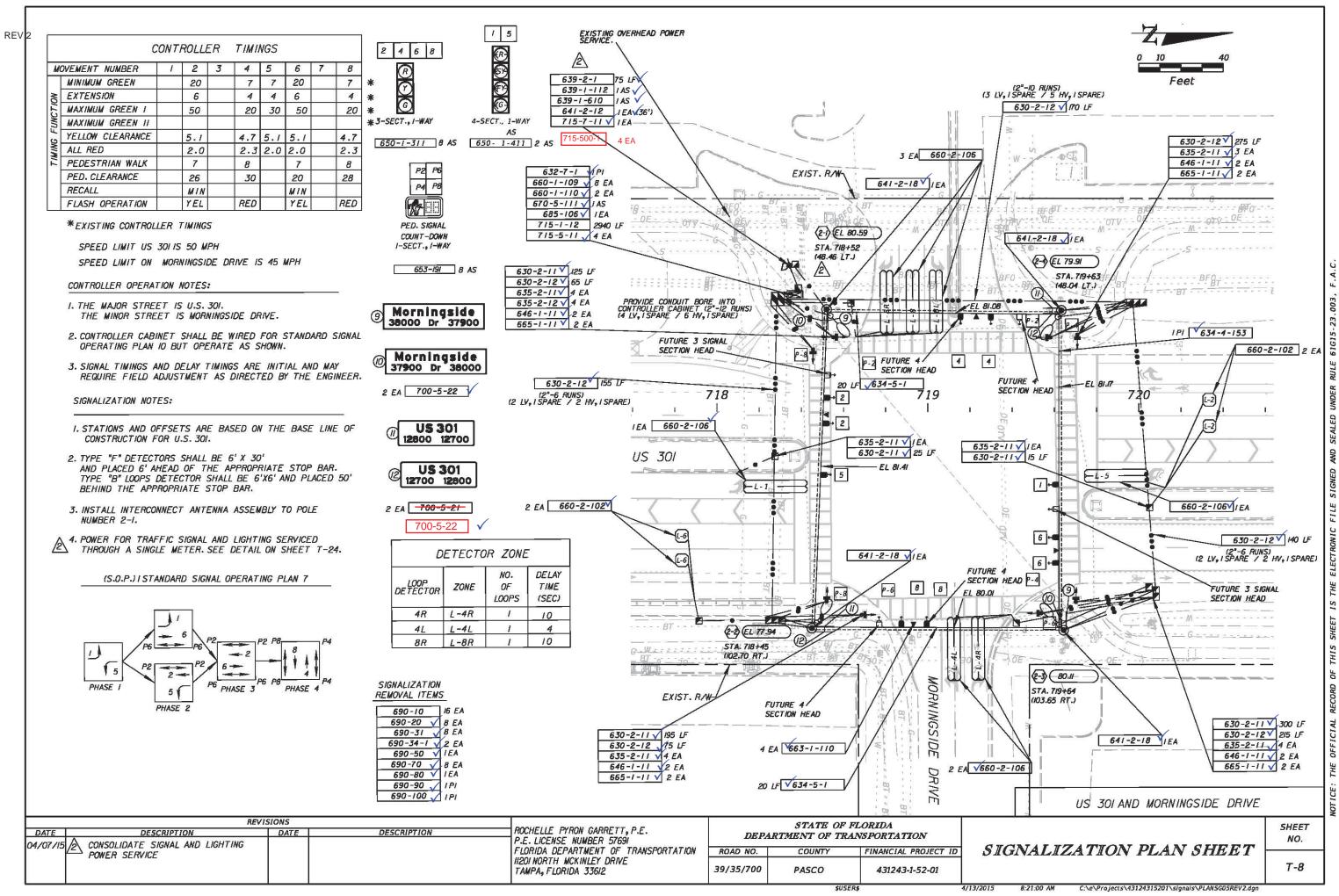
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PLANS PREPARED BY:

FLORIDA DEPARTMENT OF TRANSPORTATION DISTRICT 7 TRAFFIC DESIGN OFFICE II20I NORTH MCKINLEY DRIVE TAMPA, FLORIDA 33612 PHONE NO. (813) 975-6000

NOTE: THE SCALE OF THESE PLANS MAY HAVE CHANGED DUE TO REPRODUCTION.

KEY	SHEET REVISIONS	SIGNALIZATION PLANS		
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# **APPENDIX 5 – TRAFFIC TECHNICAL MEMORANDUM**

# TRAFFIC TECHNICAL MEMORANDUM

# MORNINGSIDE DRIVE EXTENSION ROUTE STUDY AND POND SITING REPORT FROM FORT KING ROAD TO US 301

Prepared For

PASCO COUNTY ENGINEERING SERVICES PROJECT MANAGEMENT

Prepared By



LINCKS & ASSOCIATES, INC. Engineers - Planners Tampa, Florida

#### TRAFFIC TECHNICAL MEMORANDUM

#### MORNINGSIDE DRIVE EXTENSION ROUTE STUDY AND POND SITING REPORT FROM FORT KING ROAD TO US 301

**Prepared For** 

#### PASCO COUNTY ENGINEERING SERVICES PROJECT MANAGEMENT

Prepared By

LINCKS & ASSOCIATES, INC. 5023 West Laurel Street Tampa, Florida 33607 813-289-0039 State of Florida Authorization No. EB0004638

February, 2021

Project No. 20128

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This item has been electronically signed and sealed by Ali Altefi, P.E. on the time and date stamp using the digital signature. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.

Ali Altefi, P.E. Florida Registration Number 43854 5023 West Laurel Street Tampa, Florida 33607



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2045 Model Volumes (without Morningside Extension)
2015 Model Volumes
Model Correction Factor
Intersection Analysis (2045)
NCHRP Report #279
FDOT Design Manual Exhibit 212-1



# Section 1.0 INTRODUCTION

The purpose of this memorandum is to document the Traffic Operational Analysis results for the segment of Morningside Drive from SR 52 to US 301 and the intersections of Morningside Drive and SR 52, Morningside Drive and Fort King Road and Morningside Drive and US 301. This information will be included in the Route Study and Pond Siting Analysis Report (RSPSAR) for Morningside Drive Extension from Fort King Road to US 301. The study area is shown on Figure 1-1.

## 1.1 TRANSPORTATION PLAN CONSISTENCY

The construction of Morningside Drive Extension as a two (2) lane road from Fort King Road to US 301 is identified in the Pasco County Metropolitan Planning Organization (MPO) 2045 Cost Affordable Long-Range Transportation Plan (LRTP). In addition, the Pasco County Highway Vision Plan and Functional Classification Map included in the County's Comprehensive Plan shows Morningside Drive as a future collector roadway.

Sheets from the referenced LRTP and the County's Comprehensive Plan are provided in the Appendix A.







2

### Section 2.0 <u>EXISTING ROADWAY CONDITIONS</u>

### 2.1 EXISTING ROADWAY CHARACTERISTICS

The following describes the characteristics of the roadway network in the study area:

### <u>SR 52</u>

SR 52 is currently a state, two (2) lane undivided rural roadway that runs in a northsouth direction in the vicinity of existing Morningside Drive. According to Pasco County Highway Vision Plan and Functional Classification Map, SR 52 is classified as a collector roadway. The posted speed limit on SR 52 is 45 MPH in the vicinity of Morningside Drive.

### Fort King Road

Fort King Road is a County, two (2) lane undivided rural roadway that runs in a northsouth direction. According to Pasco County Highway Vision Plan and Functional Classification Map, Fort King Road is classified as a collector roadway. The posted speed limit on Fort King Road is 35 MPH in the vicinity of Morningside Drive.

### <u>US 301</u>

US 301 is currently a State, four (4) lane divided rural roadway that runs in a northsouth direction. According to Pasco County Highway Vision Plan and Functional Classification Map, US 301 is classified as an arterial roadway. The posted speed limit on US 301 is 45 MPH in the vicinity of Morningside Drive.

### Morningside Drive

Morningside Drive is currently a County, two (2) lane undivided roadway that runs in an east-west direction with urban cross section from SR 52 to Fort King Road and rural cross section east of US 301. According to Pasco County Highway Vision Plan and Functional Classification Map, Morningside Drive is classified as a collector roadway. The posted speed limit on Morningside Drive is 30 MPH between SR 52 and Fort King Road and 45 MPH east of US 301.



### 2.2 EXISTING INTERSECTION TRAFFIC CONTROLS

### SR 52 and Morningside Drive/Adair Road

SR 52 and Morningside Drive intersection is currently a four-leg intersection with stopsign control on Morningside Drive on the east side of SR 52 and Adair Road on the west side of SR 52. There are exclusive southbound and northbound left turn lanes on SR 52 and exclusive westbound left turn lane and a shared westbound through and right turn lane on Morningside Drive. There is a shared eastbound left/through/right lane on Adair Road.

### Fort King Road and Morningside Drive

Fort King Road and Morningside Drive intersection is currently a three-leg intersection with stop-sign control on Morningside Drive. The Advent Health hospital driveway is located immediately to the north side of this intersection, and on the east side of Fort King Road. There are no exclusive turn lanes on Fort King Road. The hospital's access driveway, which also serves as the emergency room access driveway, is located south of the intersection, on the east side of Fort King Road. There is an exclusive eastbound left turn lane on Morningside Drive.

### US 301 and Morningside Drive

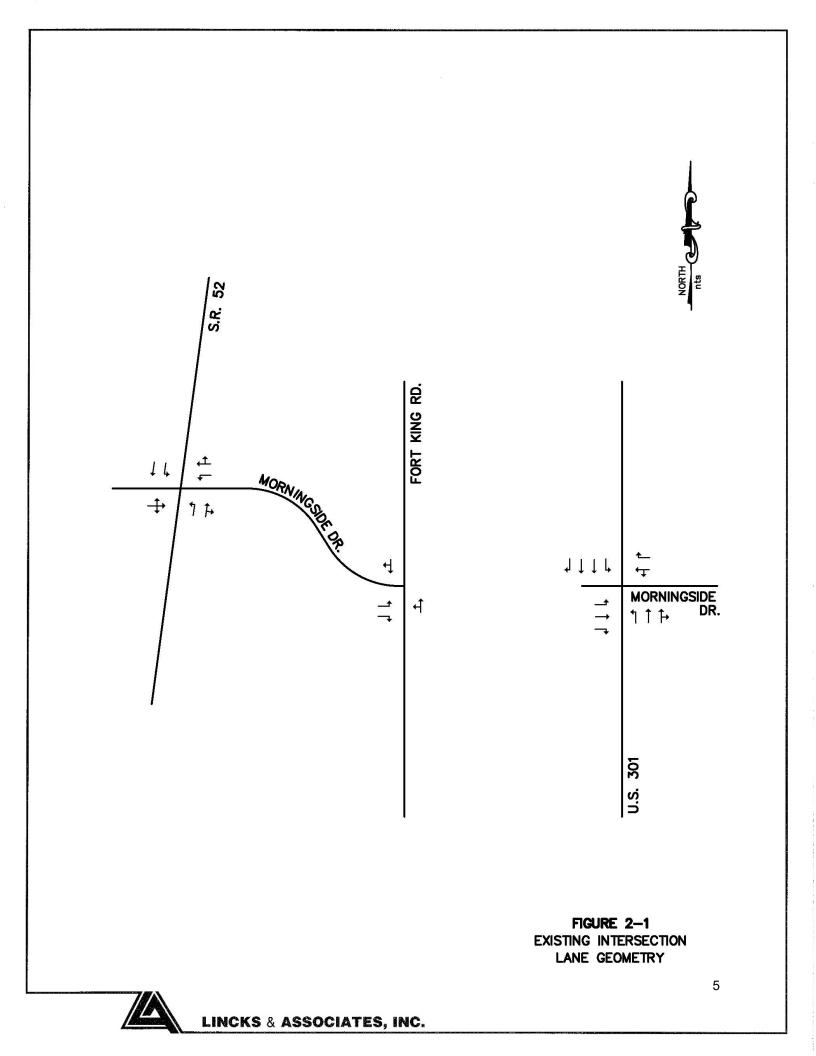
US 301 and Morningside Drive is a four-leg intersection and is currently signalized. There are exclusive northbound and southbound left turn lanes and a southbound right turn lane on US 301. The Morningside Drive leg on the east side of US 301 has an exclusive right turn lane and a shared left and through lane. There is an existing retail center driveway located on the west side of this intersection and aligns with Morningside Drive located on the east side of this intersection. This driveway has exclusive eastbound left and right turn lanes and a through lane.

Figure 2-1 illustrates the existing geometry at the intersections described above.

### 2.3 TRAFFIC DATA COLLECTION

Traffic data and characteristics for the study area were obtained from FDOT Traffic Information Online and traffic counts. Daily vehicle counts were conducted for 48 hours and peak hour turning movement counts were conducted from 7:00 AM to 9:00 AM and from 4:00 to 6:00 PM for the morning and evening street peak hours, respectively. All counts were taken on Tuesday, Wednesday, or Thursday only to represent typical weekday traffic conditions. Traffic counts were conducted at the following locations:





Two Day Bi-Directional Machine Counts

- SR 52 North of Morningside Drive (2)
- SR 52 South of Morningside Drive (1)
- US 301 North of Morningside Drive (2)
- Fort King Road North of Morningside Drive (2)
- Fort King Road South of Morningside Drive (2)
- Morningside Drive East of SR 52 (2)
- Morningside Drive East of US 301 (2)

(1) FDOT Counts: February 4-5, 2019(2) Other Counts: September 22-23, 2020

### Intersection Counts

- Morningside Drive and SR 52
- Morningside Drive and Fort King Road
- Morningside Drive and US 301

Counts Date: October 1, 2020

Figure 2-2 provides the location and type of each traffic count conducted in the study area.

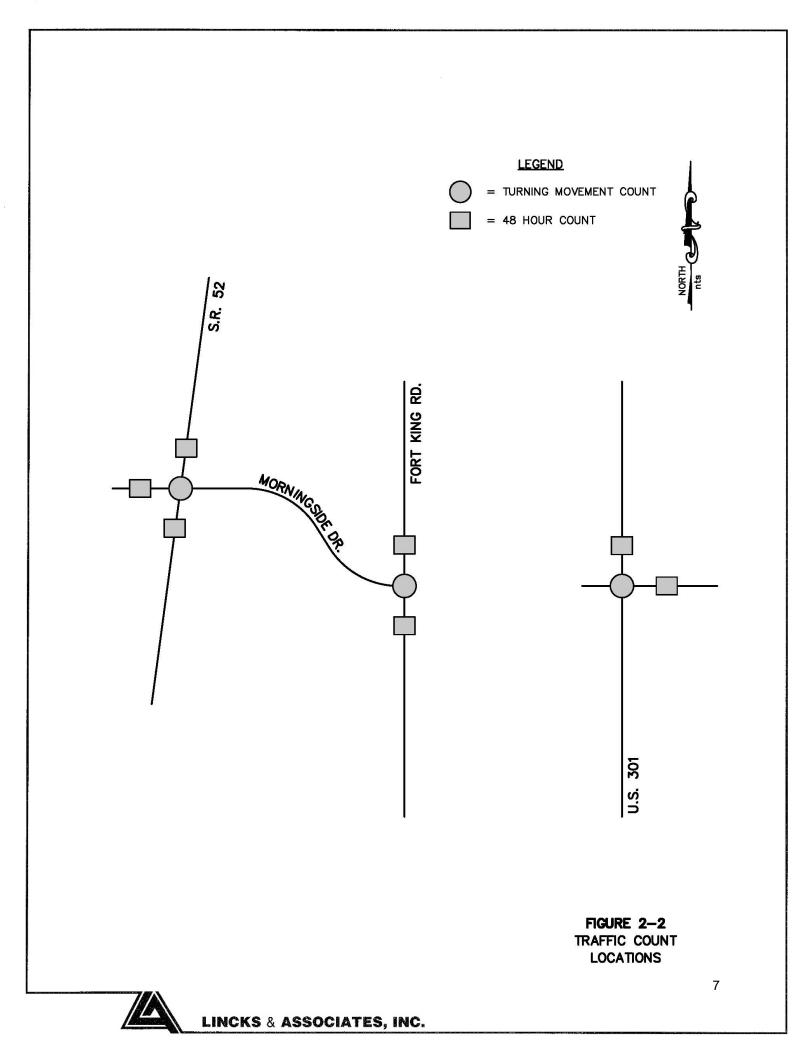
### 2.4 DESIGN TRAFFIC CHARACTERISTICS

The Existing year (2019 and 2020) traffic counts were utilized to develop the peak hour traffic characteristics. These factors provide the ratio of the Annual Average Daily Traffic (AADT) that occurs during the design hour K-factor, the proportion of traffic traveling in the peak direction D-Factor during the design hour and the percentage of trucks during the design hour T-factor.

### 2.4.1 DESIGN HOUR K-FACTOR

Based on information obtained from the FDOT Traffic Information Online, a standard K-Factor of 9.0 percent was used for the development of the future year Design Hour Volumes (DHV) for this study. This is the recommended K-Factor for urbanized and transitioning to urbanized areas, and it represents a typical weekday peak hour.





### 2.4.2 DIRECTIONAL DISTRIBUTION D-FACTOR

The Directional Distribution Factor, D-Factor, is a representation of the percentage of vehicles traveling in the peak direction during the peak hour of the day. The D-Factor used in the analysis was derived by considering existing measured traffic characteristics from traffic counts. All relevant traffic data collected for the project are provided in the Appendix C.

The average D-Factor of 0.53 was used for the segment of Morningside Drive which does not exist today. Table 2-1 represents the calculation of D-Factor used to compute the Directional Design Hour Volumes (DDHV).

### 2.4.3 TRUCK PERCENTAGE T-FACTOR

The T-Factor is the percentage of trucks during the design hour. The percentage of trucks in the design hourly volume were determined utilizing the percentage of trucks in the existing turning movement counts and assumption that those percentages will remain constant through the design year. A T-Factor of 6% was calculated and provided in Appendix C.

### 2.5 EXISTING TRAFFIC VOLUMES

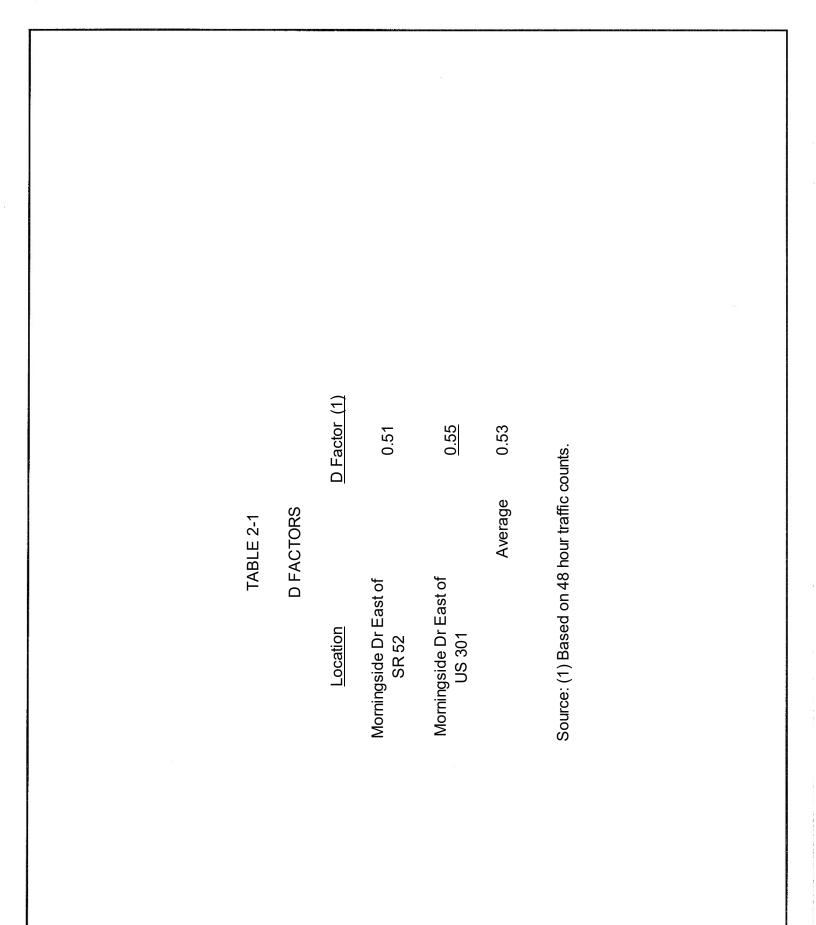
The existing Average Annual Daily Traffic (AADT) volumes were obtained by applying the weekly Seasonal Factor (SF) and Axle Correction Factor, as documented in FDOT's Florida Traffic Information Online to the Average Daily Counts (ADT) and provided in the Appendix C. Figure 2-3 shows the Existing Year AADT for the roadway segments adjacent to the Morningside Drive intersections and Table 2-2 illustrates the calculation of the Existing Year AADT's.

The existing AM and PM peak hour turning movement counts are shown in Figure 2-4. The existing AM and PM peak hour turning movement counts were converted to peak season utilizing FDOT peak season adjustment factors, as shown in Figure 2-5.

### 2.6 EXISTING CONDITIONS TRAFFIC OPERATIONS ANALYSIS

Traffic operations analysis for the AM and PM peak hours were conducted to document the levels of service (Level of Service) within the study area for the Existing Year (2020). Level of Service is a qualitative measure of traffic operations. Level of Service designations range from A to F, with Level of Service A representing the best operating





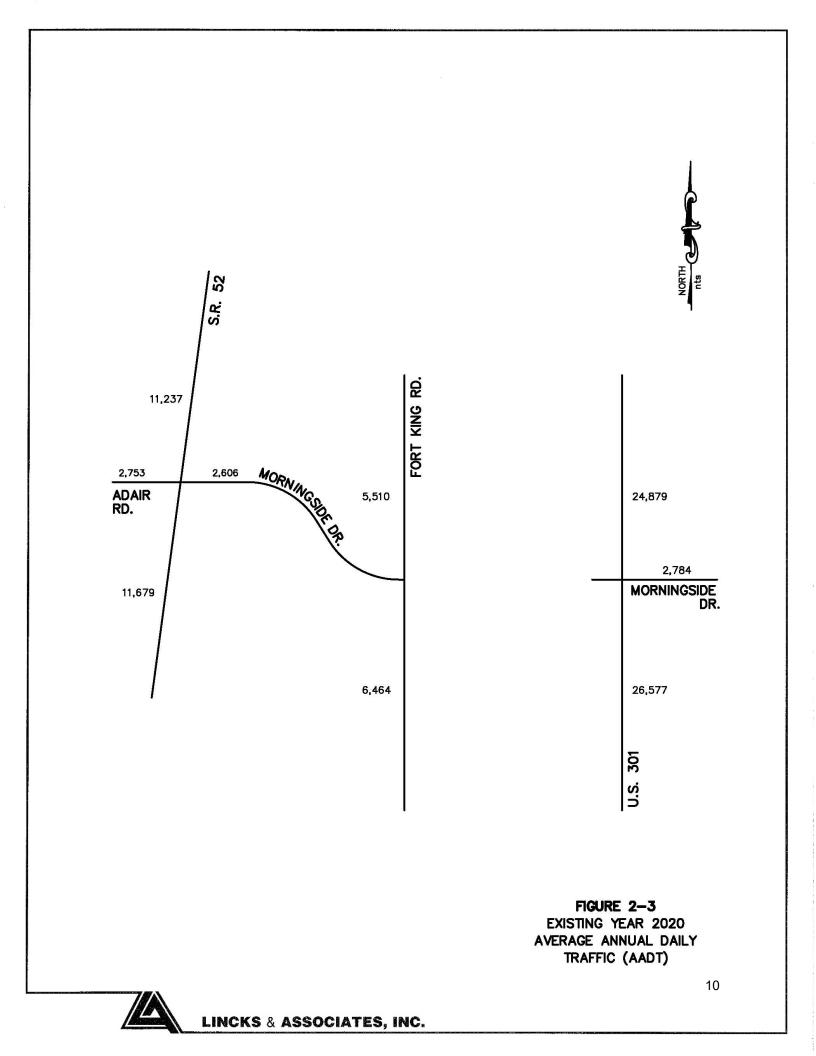


TABLE 2-2

EXISTING YEAR AADT CALCULATION

Axle Factor AADT	0.98 11,237	0.98 11,679	0.90 (2) 5,510	0.90 (2) 6,464	0.90 (2) 2,606	0.90 (2) 2,784	0.96 24,879	- 26,577	- 2,753
	0	0	0.0	0.6	0.0	0.0	0		
<u>Seasonal Factor</u>	1.06	0.97	1.06	1.06	1.06	1.06	1.06	1.05	1.05
Average ADT	10,817	12,286	5,775	6,775	2,732	2,919	24,449	25,311	2,622
Existing ADT	10,707 10,927	12,402 12,169	5,708 5,842	6,758 6,792	2,748 2,716	2,937 2,901	24,385 24,513	25,311 (1)	2,622(1)
Count Date	Sept. 22, 2020 Sept. 23, 2020	Feb. 11, 2020 Feb. 12, 2020	Sept. 22, 2020 Sept. 23, 2020	Sept. 22, 2020 Sept. 23, 2020	Sept. 22, 2020 Sept. 23, 2020	Sept. 22, 2020 Sept. 23, 2020	Sept. 22, 2020 Sept. 23, 2020	Oct. 1, 2020	Oct. 1, 2020
<u>Location</u>	SR 52 North of Morningside Dr	SR 52 South of Morningside Dr	Fort King Road North of Morningside Dr	Fort King Rd South of Morningside Dr	Morningside Dr East of SR 52	Morningside Dr East of US 301	US 301 North of Morningside Dr	US 301 South of Morningside Dr	Adair Rd West of SR 52

1) Based on PM peak turning movement count and K = 0.09. 2) Based on eastern Pasco data by FDOT.



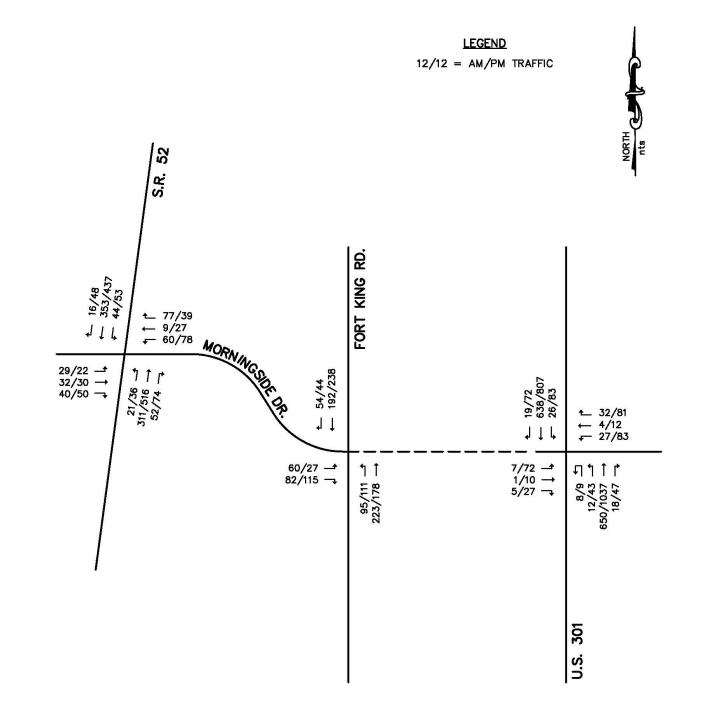


FIGURE 2-4 EXISTING YEAR 2020 AM/PM TURNING MOVEMENT VOLUMES



LINCKS & ASSOCIATES, INC.

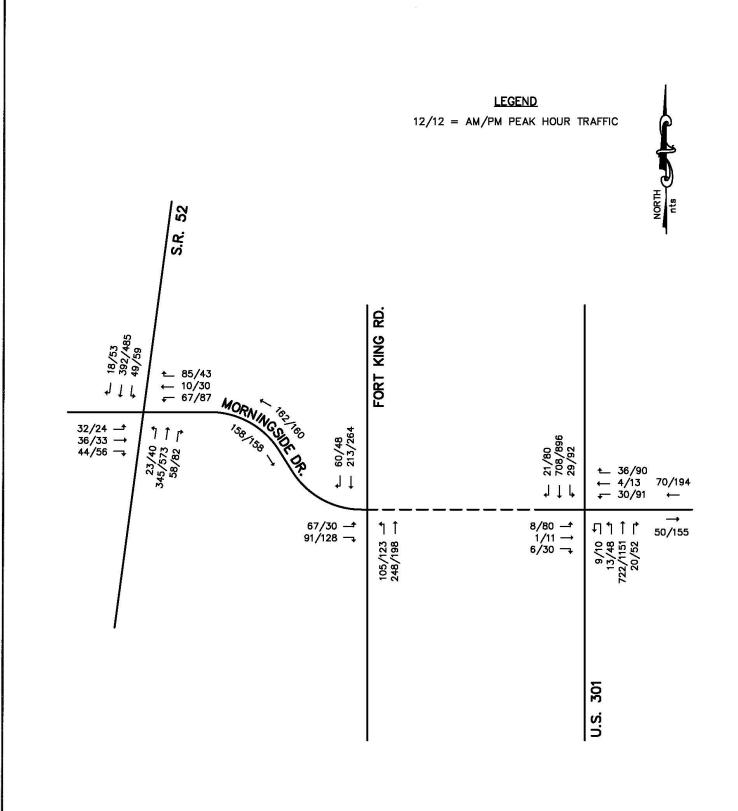


FIGURE 2-5 PEAK SEASON 2020 AM/PM PEAK HOUR TURNING MOVEMENT VOLUMES



conditions and Level of Service F representing the worst operating conditions. The existing conditions analysis was performed using the methodologies described in Chapters 18 and 19, signalized and unsignalized intersections of the Transportation Research Board (TRB) Special Report, the 2010 Highway Capacity Manual, and HCS Software for unsignalized intersections and SYNCHRO for signalized intersections.

### 2.6.1 INTERSECTION OPERATIONS ANALYSIS

An intersection capacity analysis was conducted at the following intersections:

- Morningside Drive/Adair Road and SR 52
- Morningside Drive and Fort King Road
- Morningside Drive and US 301

The turning movement counts provided in Figure 2-5 were used to perform the operational analysis. Level of Service Standard D or better, for each movement was considered acceptable for the purpose of the analysis.

As shown in Table 2-3, the intersections operate within an acceptable Level of Service during AM and PM peak hours except for the following:

Morningside Drive and SR 52/Adair Road intersection

- Eastbound left, through and right movements during the AM and PM peak hours
- Westbound through and right movements during the PM peak hour
- Westbound left movement during the AM and PM peak hours

Morningside Drive and Fort King Road

• Eastbound left movement during the AM peak hour

The SYNCHRO and Highway Capacity Software (HCS) output files are provided in the Appendix D.

### 2.6.2 SEGMENT ANALYSIS

Roadway segment analysis was conducted for the following roadway segments:



LINCKS & ASSOCIATES, INC.

TABLE 2-3

### INTERSECTION ANALYSIS (2020 EXISTING PEAK SEASON)

Right	Ш * *	ы.	$\triangleleft$ $\triangleleft$ $\bigcirc$ $\triangleleft$
PM LOS Through	шш* * шш* * шш <b> 4</b>	- ∢	U D U m
Left	шшҳҳ	0 ∢	$\Box \Box \land \blacksquare$
Right	ш ш * *	ы Ч	ৰ ৰ ৰ ৰ
AM LOS Through	Щ Ш * *	- X	
Left	шцζζ	ш∢	
Movement	iir Rd EB F F F WB F F B B A * * B B S SB A * * B F SB A * * B S	EB NB	EB NB SB
Intersection	Momingside Dr/Adair Rd and SR 52	Morningside Dr and Fort King Rd	Morningside Dr and US 301

\* Free flow, therefore LOS was not calculated.

- Morningside Drive from SR 52 to Fort King Road
- Morningside Drive from US 301 to Old Lakeland Highway

The analysis was conducted utilizing the peak season peak hour volumes and the latest version of FDOT Generalized Capacity Tables. Table 2-4 illustrates the results of the analysis. As shown, Morningside Drive is expected to operate at an acceptable Level of Service, during the AM and PM peak hours.



TABLE 2-4

SEGMENT LOS ANALYSIS (PEAK SEASON TRAFFIC)

(Hour	U	O
PM Peak Hour Volume (3) LOS	318 C	349
•		
(Hour	U	O
AM Peak Hour Volume (3) LOS	320 C	120 C
Capacity (1)	1,440	1,440
No. of <u>Lanes</u>	2 LU (2)	2 LU (2)
민	Fort King Rd	Aorningside Dr US 301 Old Lakeland Hwy
From	SR 52	US 301
Road	Morningside Dr SR 52	Morningside Dr

Based on FDOT 2020 Generalized Capacity Tables and 40 MPH or higher posted speed limit.
 2 LU: 2 lane undivided.
 Based on Figure 2-5 volumes.

### Section 3.0 <u>TRAFFIC FORECASTS</u>

This section describes the travel demand modeling procedure, as well as the development of future year traffic. The year of the forecast was assumed to be 2045.

### 3.1 FUTURE TRAVEL DEMAND

The development of future year traffic projections involved the review of the current adopted 2045 Florida Standard Urban Transportation Model Structure (FSUTMS) travel demand model [Tampa Bay Regional Planning Model (TBRPM 9.0)]. The TBRPM is recognized by FDOT District Seven, as well as the Tampa Bay Area MPOs, as the accepted travel demand forecasting tool. The roadway network used reflects the latest available adopted Cost Affordable LRTPs for all counties in the region.

The TBRPM 9.0 model 2045 land use data and roadway traffic volume loadings were adjusted based on comments received by City of Dade City staff and review of Traffic Analysis Zones (TAZ) boundaries and centroid connections in the vicinity of Morningside Drive. The following specific adjustments were made:

- 1) Dade City staff requested 180 additional dwelling units to be added to TAZ #2045. The new extension of Morningside Drive will bisect TAZ #2045 which was causing unrealistic traffic loadings, therefore a new TAZ #2500 was created.
- 2) The additional 180 dwelling units were added to TAZ #2500 and the land uses in TAZ #2045 were modified by mainly transferring non-residential land use data to TAZ #2500 based on land use characteristics and expected growth of the area.
- 3) The location of one of the centroid connections to SR 52 for TAZ #2400 was adjusted to represent Adair Road located on the westside of SR 52.

The documentation of the above changes is provided in the Appendix F.

The model volumes were compared to existing AADT's for all segments within the study area, as shown in Table 3-1. As shown, there are segments where the future AADTs are less than existing AADTs. This was expected because of future construction of



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TABLE 3-1

## PRELIMINARY GROWTH RATE

Location	Existing AADT	2045 <u>Model AD T</u>	2045 Model AADT (1)	Average Annual <u>Growth Rate</u>
SR 52 North of Morningside Dr	11,237	11,297	10,732	Negative
SR 52 South of Morningside Dr	11,679	13,430	12,759	0.36
Fort King Road North of Morningside Dr	5,510	4,858	4,615	Negative
Fort King Rd South of Morningside Dr	6,464	2,117	2,011	Negative
Morningside Dr East of SR 52	2,606	4,769	4,531	2.95
Morningside Dr East of Fort King Road		1,855	1,762	ı
Morningside Dr West of US 301		2,057	1,954	·
Morningside Dr East of US 301	2,784	545	518	Negative
US 301 North of Morningside Dr	24,879	28,655	27,222	0.38
US 301 South of Morningside Dr	26,577	29,824	28,334	0.26
Adair Rd	2,753	2,131	2,024	Negative



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1) Based on MOCF of 0.95

Clinton Avenue Extension (realigned SR 52) which is a major east-west roadway and is expected to result in significant traffic division in the area. Furthermore, this area of the County is not expected to experience significant growth compared to central and south market areas. After discussions with County staff, it was decided to apply an average growth rate to existing turning moving counts to obtain the future travel demand. The calculation of the average growth rate was based on 2015 Model Volumes and 2045 Model Volumes (without Morningside Drive Extension). An average annual growth rate of 1.32 percent was calculated and used in the analysis, as shown in Table 3-2.

### 3.2 FUTURE YEAR DHVS AND DDHVS

The following methodology was utilized to obtain the DDHV for the intersections in the study area.

- 1. The average growth rate was applied to existing peak season turning movement counts to obtain the initial DDHV's.
- 2. The 2045 Model ADT for the new segment of Morningside Drive was converted to AADT based on MOCF and further converted to AM and PM DDHV by applying appropriate K and D factors.
- 3. The final 2045 turning movements were estimated utilizing the combination of model approach DDHV's for new segment of Morningside Drive, the estimated growth rate, and the general expected travel patterns in the area.

Figure 3-1 represents the year 2045 Directional Design Hour Volumes (DDHVs) used in the analysis.



TABLE 3-2

# AVERAGE ANNUAL GROWTH RATE

Average Annual <u>Growth Rate</u>	1.74	2.25	2.49	0.55	0.28	1.34	0.56
2045 <u>Model Volume</u>	11,299	13,368	4,553	28,955	28,798	4,705	3,572
2015 <u>Model Volume</u>	7,420	7,974	2,606	24,879	26,577	3,358	3,056
Location	SR 52 North of Morningside Dr	SR 52 South of Morningside Dr	Morningside Dr East of SR 52	US 301 North of Morningside Dr	US 301 South of Morningside Dr	Fort King Rd North of Morningside Dr	Fort King Rd South of Morningside Dr



21

1.32

Average

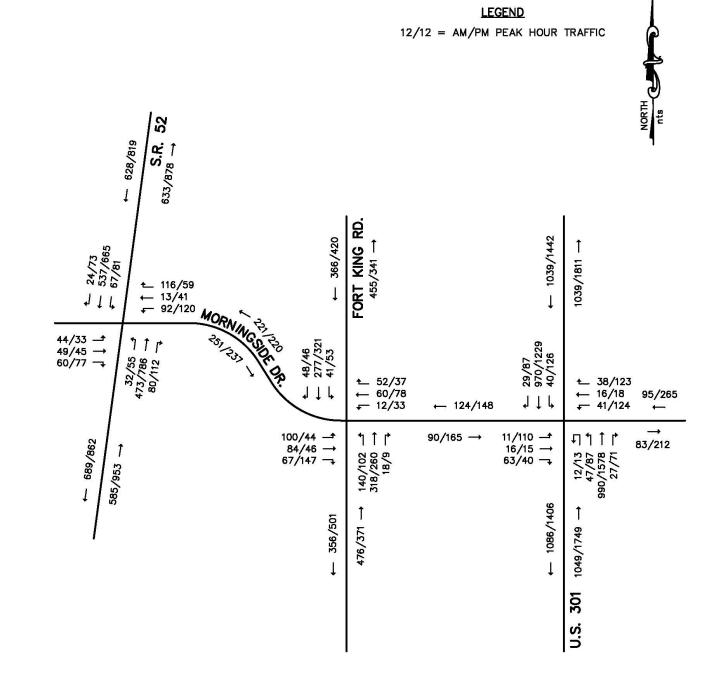


FIGURE 3-1 2045 DIRECTIONAL DESIGN HOUR VOLUMES (DDHV's)

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### Section 4.0 FUTURE CONDITIONS TRAFFIC OPERATIONS ANALYSIS

A future conditions traffic operations analysis was conducted to evaluate the performance of the following intersections and segments.

Intersections:

- Morningside Drive/Adair Road and SR 52
- Morningside Drive and Fort King Road
- Morningside Drive and US 301

Segments:

- Morningside Drive from SR 52 to Fort King Road
- Morningside Drive from Fort King Road to US 301
- Morningside Drive from US 301 to Old Lakeland Highway

The future conditions intersection analysis was performed using Synchro software for signalized intersections and roundabouts and HCS Software for unsignalized intersections and FDOT Generalized Capacity Tables was utilized for segment analysis.

The Level of Service standard of D was assumed for the analysis.

### 4.1 **OPERATIONS ANALYSIS FOR INTERSECTIONS**

Based on discussions with Pasco County staff three configurations were used to evaluate the study intersections per the following:



Interception	Option A Unsignalized	Option B Signalized	Option C Roundabout
Intersection	Unsignalized	Signalizeu	Roundabout
Morningside	$\checkmark$	$\checkmark$	-
Drive/Adair Road			
and SR52			
Morningside Drive	$\checkmark$	$\checkmark$	$\checkmark$
and Fort King			
Road			
Morningside Drive	-	$\checkmark$	-
and US 301			

The HCS and SYNCHRO output files are provided in Appendix G.

### SR 52 and Morningside Drive/Adair Road

### Option A - Unsignalized

Unsignalized intersection analysis was conducted using HCS software and lane geometry in Figure 4-1. Table 4-1 provides Level of Service results. The results indicate that all movements are projected to operate at or above acceptable Level of Service during AM and PM peak hours through design year (2045) except for the following:

- Eastbound left, through and right movements during the AM and PM peak hours
- Westbound left movement during the AM and PM peak hours
- Westbound through and right movements during the PM peak hour

### Option B – Signalized

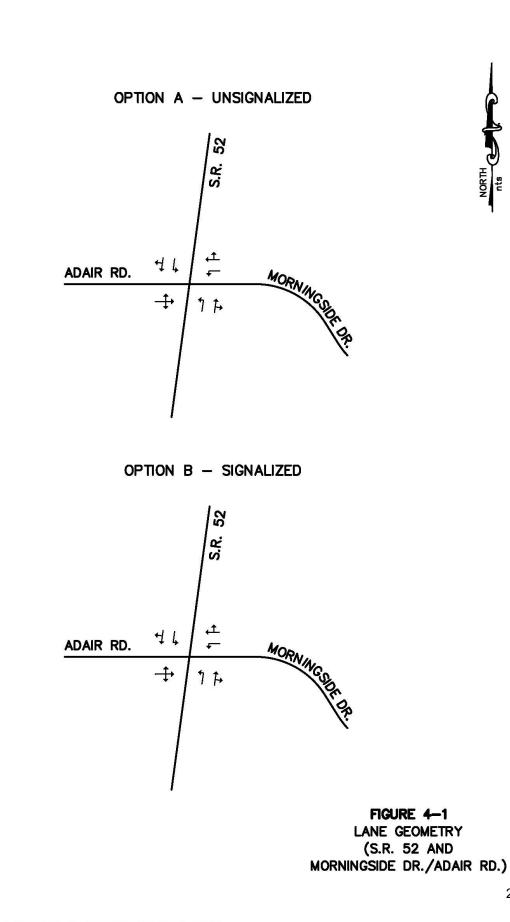
The signalized intersection analysis was conducted using the SYNCHRO Software and the lane geometry shown in Figure 4-1. Table 4-2 provides Level of Service results. The results indicate that the conventional signalized intersection with the assumption that a signal is warranted should operate at or above acceptable Level of Service during the AM and PM peak hours through the Design Year (2045).

### Fort King Road and Morningside Drive

### Option A – Unsignalized

The unsignalized intersection analysis was conducted using HCS Software and the lane geometry shown in Figure 4-2. In addition, based on NCHRP Report # 279, a northbound left turn lane and southbound left turn lane are warranted, which was included in the analysis. A westbound left turn lane is not warranted. However, it is







25

NORTH

TABLE 4-1

### INTERSECTION ANALYSIS - UNSIGNALIZED (OPTION A) (2045 TRAFFIC)

L	Right	ш	ш	*	*	U	Δ	*	*
PM Peak Hou	Left Through Right	ш	ш	*	*	U	۵	*	*
		ш	ш	۷	В	ш	ш	A	۷
ır	Right	ш	U	*	*	ш	۵	*	*
AM Peak Hou	t Left Through Right	ш	o	*	*	Ш	۵	*	*
	Left	ш	ш	A	۷	ш	ш	A	۷
	Movement			NB	SB	EB	WB	NB	SB
	<u>Intersection</u>	Morningside Dr/Adair Rd	and SR 52			Morningside Dr	and Fort King Rd		

\* Free flow, therefeore LOS was not calculated.

TABLE 4-2

### INTERSECTION ANALYSIS - SIGNALIZED (OPTION B) (2045 TRAFFIC)

Intersection     Movement     Left     Through     Right     Left     Through       Moningside Dr/Adair Rd     EB     C     C     C     B     B       Moningside Dr/Adair Rd     EB     C     C     C     B     B       Moningside Dr/Adair Rd     EB     C     C     C     B     B       Moningside Dr/Adair Rd     EB     C     C     C     B     B       Moningside Dr     NB     A     A     A     A     B       Moningside Dr     WB     D     D     A     B     A       Moningside Dr     WB     B     B     C     C     C       Moningside Dr     WB     D     D     A     D     C       Moningside Dr     WB     B     B     C     C     C       Moningside Dr     WB     D     D     D     C     C	L									
AM Peak Hour       Movement     Left     Through       EB     C     C       WB     C     A       WB     C     C       WB     C     C       WB     A     A       NB     A     A       WB     D     D       WB     D     D       WB     B     B       NB     B     B	PM Peak Hou	Through	В	В	В	۷	U	Δ	U	В
Movement EB WB NB SB NB SB SB		Left	В	Δ	۷	В	۵	۵	U	۵
Movement EB WB NB SB NB SB SB	IL	Right	U	۷	۷	۷	A	A	В	۷
Movement EB WB NB SB NB SB SB	NM Peak Hou	Through	U	۷	۷	A	۵	۵	В	ш
Movement EB WB NB SB NB SB SB	٩	Left	U	ပ	A	A	Ω	Δ	A	۷
Intersection Morningside Dr/Adair Rd and SR 52 Morningside Dr and US 301		Movement	EB	WB	NB	SB	EB	WB	NB	SB
			Morningside Dr/Adair Rd	and SR 52			Morningside Dr	and US 301		

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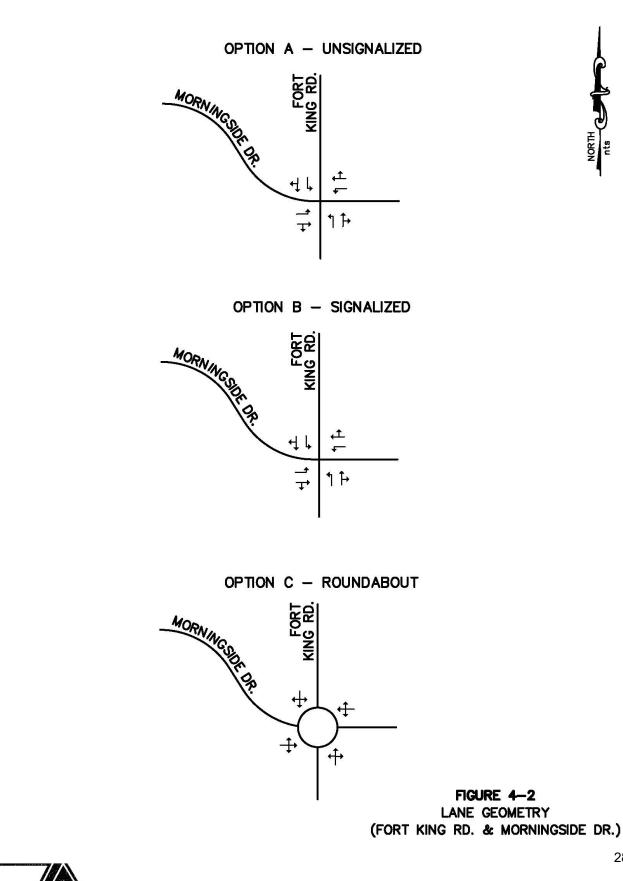
SB WB SB

Morningside Dr and Fort King Rd

Right

**P B B** 





28

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recommended a westbound left turn lane be included to create a balance of lane geometry with the eastbound approach. Table 4-1 provides the Level of Service results. The results indicate that all movements are projected to operate at or above an acceptable Level of Service during AM and PM peak hours through design year (2045) except for the following:

- Eastbound left movement during the AM and PM peak hours
- Eastbound through and right movements during the AM peak hour
- Westbound left movement during the AM and PM peak hours

### Option B - Signalized

The signalized intersection analysis was conducted utilizing SYNCHRO software and lane geometry shown in Figure 4-2. Table 4-2 provides the Level of Service results. The results indicate that the conventional signalized intersection, with the assumption that a signal is warranted, would operate at or above an acceptable Level of Service during the AM and PM peak hours through the design year (2045).

### Option C – Roundabout

The Roundabout intersection analysis was conducted using the SYNCHRO Software and the lane geometry shown in Figure 4-2. Table 4-3 provides the Level of Service results. The results indicate that the roundabout intersection is projected to operate at or above an acceptable Level of Service during AM and PM peak hours through the Design Year (2045).

### Morningside Drive and US 301

### **Option B - Signalized**

The signalized intersection analysis was conducted using the SYNCHRO Software and the lane geometry shown in Figure 4-3. The existing number of lanes and signal timings were utilized in the analysis except for signal timings during the PM peak hour. Table 4-2 provides the Level of Service results. The results indicate that the signalized intersection is projected to operate at or above an acceptable Level of Service during AM and PM peak hours through the Design Year (2045).

### 4.2 ANALYSIS FOR SEGMENTS

Capacity analysis was conducted for the segment of Morningside Drive from SR 52 to Old Lakeland Highway using FDOT Generalized Capacity Tables.



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F	-

# INTERSECTION ANALYSIS - ROUNDABOUT (OPTION C) (2045 TRAFFIC)

PM Peak hour	< < < 0
AM Peak Hour	< < ₪ <
Movement	EB WB SB
Intersection	Morningside Dr and Fort King Rd



### OPTION B - SIGNALIZED

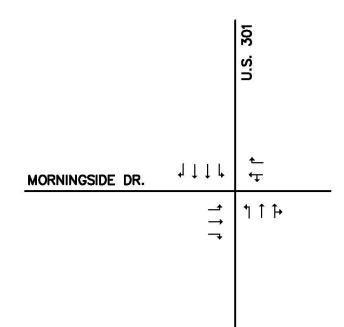


FIGURE 4-3 LANE GEOMETRY (U.S. 301 & MORNINGSIDE DR.)





The results of the analysis are provided in Table 4-4. The results indicate that Morningside Drive is projected to operate at or above acceptable Level of Service during AM and PM peak hours through design year (2045), as a two (2) lane undivided roadway.

### 4.3 STORAGE LENGTHS

Turn lane length analysis was conducted for the studied intersections based on signalized intersection (Option B). The results are provided in Table 4-5.



TABLE 4-4

### SEGMENT ANALYSIS (2045 TRAFFIC)

PM Peak Hour	Volume (3) LOS	416 C	286 C	435 C	
Hour	<u>LOS</u>	O	U	U	
AM Peak I	Volume (3) LOS	472 C	214	178	
	Capacity (1)	2 LU (2) 1,440	2 LU (2) 1,440	1,440	
No. of	<u>Lanes</u> (		2 LU (2)	· 2 LU (2)	
	<u>T</u>	Fort King Rd	US 301	Morningside Dr US 301 Old Lakelane Hwy 2 LU (2) 1,440	
	From	SR 52	Fort King Rd	US 301	
	Road	Morningside Dr	Morningside Dr Fort King Rd	Morningside Dr	

Based on FDOT 2020 Generalized Capacity Tables and 40 MPH or higher posted speed limit.
 2 LU - 2 lane undivided.
 Figure 3-1 volumes.

### TABLE 4-5

### STORAGE LENGTH

Intersection	<u>Movement</u>	Volume <u>AM/PM</u>	Deceleration Length (1)	Storage Length (2)	Total <u>Length</u>	Existing <u>Length</u>				
SR 52 and Morningside Dr/Adair Rd	WBL NBL SBL	92/120 32/55 67/81	145' 240' 240'	100' 150' 150'	245' 390' 390'	235' 350' 260'				
Fort King Rd and Morningside Dr	EBL	100/44	145'	75'	220'	175'				
	WBL	12/33	Urban: 145' Rural: 290'	50'	Urban: 195' Rural: 340'	-				
	NBL SBL	140/102 41/53	290' 290'	125' 75'	415' 365'	-				
US 301 and Morningside Dr	EBL	11/110	Urban: 145' Rural: 290'	100'	Urban: 245' Rural: 390'	270'				
	EBR	63/40	Urban: 145' Rural: 290'	50'	Urban: 195' Rural: 340'	250'				
	WBR NBL SBL SBR	38/123 59/100 40/126 29/87	290' 290' 290' 290'	100' 125' 125' 25'	390' 415' 415' 315'	205' 475' 340' 405'				
SR 52 - 50 MP US 301 - 50 M Morningside D Morningside D Fort King Rd (2) Storage length signalize	<ul> <li>(1) Based on following design speeds (posted plus 5 MPH) and FDOT Design Manual Exhibit 212-1: SR 52 - 50 MPH US 301 - 50 MPH Morningside Dr (East of US 301) - 50 MPH Morningside Dr (West of US 301) - Urban: 35 MPH Rural: 50 MPH</li> <li>Fort King Rd - 40 MPH</li> <li>(2) Storage length signalized: SR 52 and Morningside Dr Based on SimTraffic.</li> </ul>									

NBL: 151' Use 150' SBL: 154' Use 150' Fort King Rd and Morningside Dr - Based on SimTraffic. EBL: 71' Use 75' Use 50' WBL: 48' NBL: 110' Use 125' SBL: 62' Use 75' US 301 and Morningside Dr. - Based on SimTraffic EBL: 94' Use 100' EBR: 51' Use 50' NBL: 120' Use 125' SBL: 124' Use 125' SBR: 30' Use 25'



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### Section 5.0 SUMMARY AND CONCLUSIONS

Level of Service and capacity analysis were conducted for the following intersections and segments:

Intersections

- Morningside/Adair Road and SR 52
- Morningside Drive and Fort King Road
- Morningside Drive and US 301

Segments

- Morningside Drive/Adair Road from SR 52 to Fort King Road
- Morningside Drive from Fort King Road to US 301
- Morningside Drive from US 301 to Old Lakeland Highway

The following is the summary of the results and conclusions:

### Intersections

### Morningside Drive/Adair Road and SR 52

Unsignalized (Option A)

- Operates below the Level of Service standard during the AM and PM peak hours with the existing geometry and existing peak season traffic.
- Operates below the Level of Service standard during the AM and PM peak hours with the existing geometry and 2045 design traffic.

### Signalized (Option B)

• Operates at or above the Level of Service standard with the existing geometry and with 2045 design traffic with the assumption that a signal will be warranted.

Morningside Drive and Fort King Road

Unsignalized (Option A)

• Operates below the Level of Service standard during the AM peak hour with the existing geometry and existing peak season traffic.



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- Operates below the Level of Service standard during the AM and PM peak hours with the existing geometry and with the 2045 design traffic.
- Operates below the Level of Service standard during the AM and PM peak hours with improved geometry and with the 2045 design traffic.

### Signalized (Option B)

• Operates at or above the Level of Service standard during the AM and PM peak hours with improved geometry and with the 2045 design traffic with the assumption that a signal will be warranted.

### Roundabout (Option C)

• Operates at or above Level of Service standard during the AM and PM peak hours with one lane roundabout and with the 2045 design traffic.

### Morningside Drive and US 301

Signalized (Option B)

- Operates at or above the Level of Service standard during the AM and PM peak hours with existing geometry and with the existing peak season traffic.
- Operates at or above the Level of Service standard during the AM and PM peak hours with existing geometry and with the 2045 design traffic.

### Segments

### Morningside Drive/Adair Road from SR 52 to Fort King Road

Capacity analysis indicates that this segment should operate at an acceptable Level of Service during the AM and PM peak hours through the design year (2045) as a two (2) lane undivided roadway.

### Morningside Drive from Fort King Road to US 301

Capacity analysis indicates that this segment should operate at an acceptable Level of Service during the AM and PM peak hours through the design year (2045) as a two (2) lane undivided roadway.

### Morningside Drive from US 301 to Old Lakeland Highway

Capacity analysis indicates that this segment should operate at an acceptable Level of Service during the AM and PM peak hours through the design year (2045) as a two (2) lane undivided roadway.



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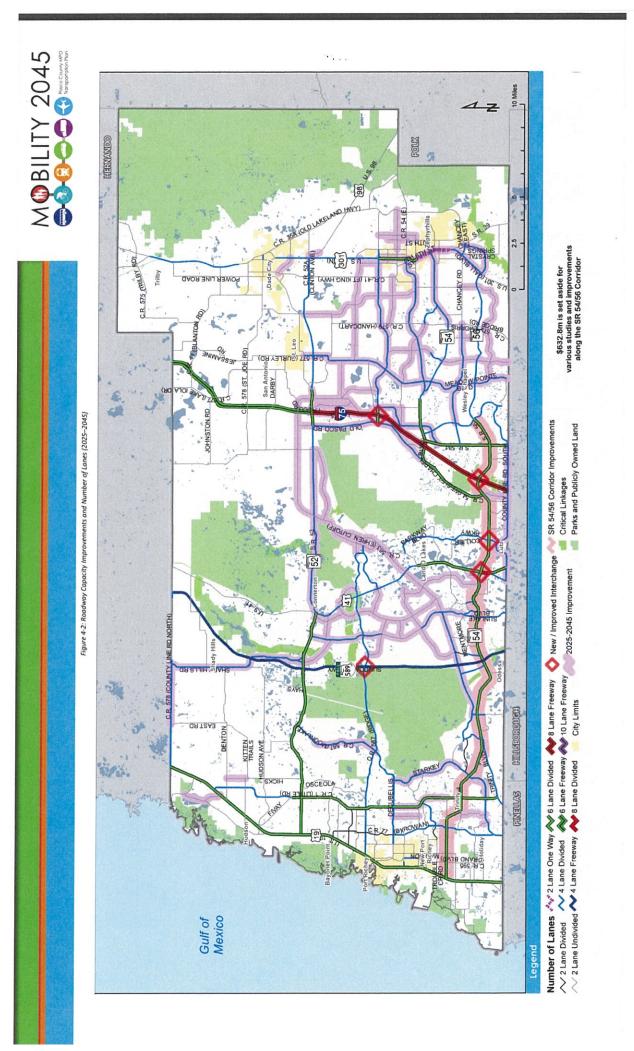
APPENDIX - A

/



2045 COST AFFORDABLE TRANSPORTATION PLAN

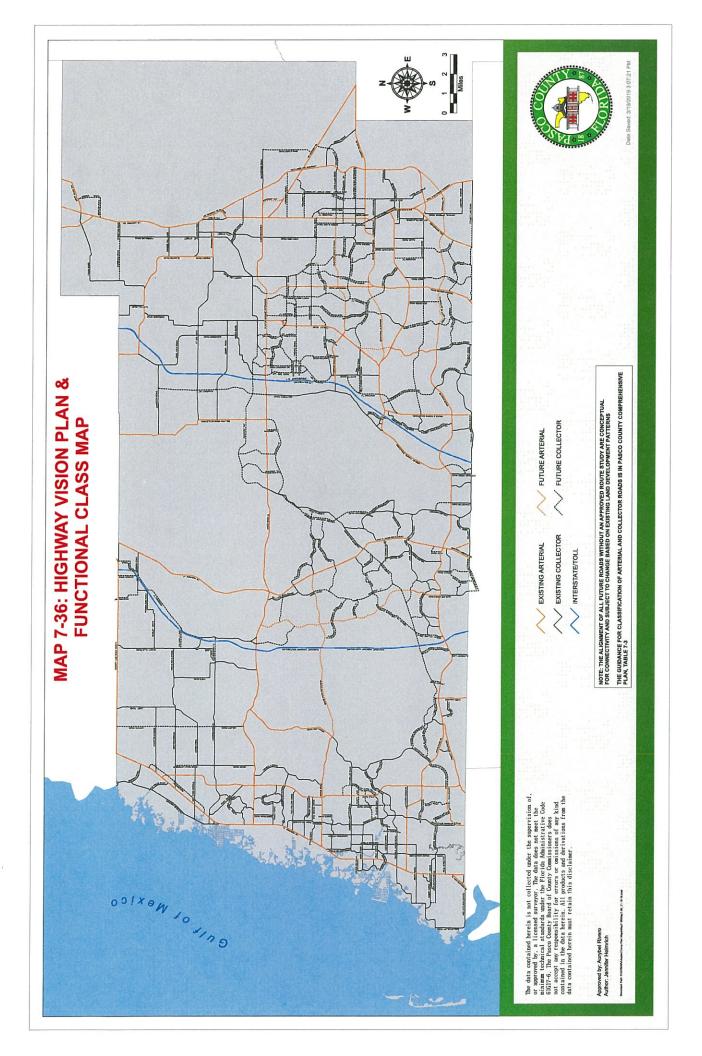




HIGHWAY VISION PLAN

1





APPENDIX - B



# **48 HOUR TRAFFIC COUNTS**



# Prepared by National Data & Surveying Services **VOLUME** SR 52 N/O Morningside Dr

Day: Tuesday Date: 9/22/2020 City: Dade City Project #: FL20\_120203\_005

	D	AILY	TOT	ALS		NB	SB	EB		WB				Т	otal
		AILT	101/	413		5,355	5,352	0		0				1(	),707
AM Period	NB		SB	S. Date	EB	WB	TOTAL	PM Period	NB		SB	EB	WB		OTAL
00:00	9		8				17	12:00	78		83			161	
00:15 00:30	3		1 2				4 8	12:15 12:30	80 80		86 85			166 165	
00:45	5	23	6	17			11 40	12:45	95	333	84	338		179	671
01:00	0	20	5	17			5	13:00	59		82	550		141	07.
01:15	4		4				8	13:15	83		79			162	
01:30	2		2				4	13:30	78		70			148	
01:45	3	9	3	14			6 23	13:45	98	318	55	286		153	604
02:00	4		6				10	14:00	96		77			173	
02:15 02:30	4		4 1				8 3	14:15 14:30	128 94		112 109			240 203	
02:30	4	14	3	14			7 28	14:45	103	421	93	391		196	81
03:00	5	14	5	14			10	15:00	102	421	117	551		219	011
03:15	2		12				14	15:15	101		96			197	
03:30	3		4				7	15:30	85		127			212	
03:45	3	13	9	30			12 43	15:45	92	380	98	438		190	81
04:00	4		11				15	16:00	97		107			204	
04:15	4		16				20	16:15	134		84			218	
04:30 04:45	76	21	14 19	60			21 25 81	16:30 16:45	110 102	443	107 102	400		217 204	0.4
04:45	6	21	35	60			41	17:00	102	443	152	400		204	843
05:15	8		41				49	17:15	113		131			244	
05:30	22		50				72	17:30	116		93			209	
05:45	34	70	80	206			114 276	17:45	112	468	129	505		241	973
06:00	28		99				127	18:00	81		84			165	-
06:15	39		83				122	18:15	72		77			· 149	
06:30	68		70	007			138	18:30	77		58			135	
06:45	87 137	222	75	327			162 549 244	18:45 19:00	59 74	289	59 58	278		118	567
07:15	122		133				255	19:15	54		38			92	
07:30	86		92				178	19:30	69		50			119	
07:45	95	440	63	395			158 835	19:45	53	250	58	204		111	454
08:00	84		64				148	20:00	65		47			112	
08:15	96		81				177	20:15	92		34			126	
08:30	85		75				160	20:30	50		34			84	
08:45	79	344	84	304			163 648	20:45	32	239	26	141		58	380
09:00	66		59				125	21:00	31		30			61	
09:15 09:30	67 61		64 76				131 137	21:15 21:30	24 24		31 13			55 37	
09:45	78	272	57	256			135 528	21:45	17	96	14	88		31	184
10:00	86		70				156	22:00	25	55	18			43	104
10:15	65		75				140	22:15	17		13			30	
10:30	70		78				148	22:30	11		9			20	
10:45	72	293	67	290			139 583	22:45	15	68	14	54		29	122
11:00	66		77				143	23:00	7		19			26	
11:15	63		57				120	23:15	11		6			17	
11:30	79 87	205	72 71	277			151	23:30 23:45	9 7	24	6	20		15	70
11:45 TOTALS	8/	295 2016	/1	277 2190			158 572 4206	TOTALS	/	34 3339	8	39 3162		15	73 650
SPLIT %		47.9%		52.1%			39.3%	SPLIT %		51.4%		48.6%			60.7
		AILY T	OTA	10		NB	SB	EB		WB				T	otal
	D,	AILY I	UTA	LS		5,355	5,352	0		0				10	,707
								the second s			-				

AM Peak Hour	07:00	06:45	- Contraction of the	Rev and	06:45	PM Peak Hour	16:15	17:00			17:00
AM Pk Volume	440	407			839	PM Pk Volume	473	505			973
Pk Hr Factor	0.803	0.765			0.823	Pk Hr Factor	0.882	0.831			0.872
7 - 9 Volume	784	699	0	0	1483	4 - 6 Volume	911	905	0	0	1816
7 - 9 Peak Hour	07:00	07:00			07:00	4 - 6 Peak Hour	16:15	17:00			17:00
7 - 9 Pk Volume	440	395			835	4 - 6 Pk Volume	473	505			973
Pk Hr Factor	0.803	0.742	0.000	0.000	0.819	Pk Hr Factor	0.882	0.831	0.000	0.000	0.872

A water

# Prepared by National Data & Surveying Services VOLUME

SR 52 N/O Morningside Dr

Day: Wednesday Date: 9/23/2020

City: Dade City Project #: FL20\_120203\_005

	D	AILY	TOL		Stra Barris	NB	SB	and the second	EB		WB						Fotal
A DEPOSIDE	U	AILT	101/	41.5		5,480	5,44	7	0		0			Harris-		10	0,927
AM Period	NB	ale kojek	SB	1204295	EB	WB	T	OTAL	PM Period	NB	Martin	SB	EE	3	WB	T	OTAL
00:00	11		5				16	AL SUR	12:00 12:15	85		69				154	
00:15 00:30	3 9		8 4				11 13		12:15	78 74		83 84				161 158	
00:45	5	28	6	23			11	51	12:45	84	321	90	326			174	647
01:00	1		5				6	S. C. S.	13:00	91		92				183	
01:15	4		3				7		13:15	88		94				182	
01:30	4	12	2 6	16			6 10	29	13:30 13:45	80 100	359	67 79	222			147 179	691
01:45	4	13	1	16			5	29	14:00	89	339	101	332			1/9	691
02:15	4		3				7		14:15	118		106				224	
02:30	5		0				5		14:30	91		92				183	
02:45	2	15	0	4			2	19	14:45	111	409	97	396			208	805
03:00 03:15	4		1 7				5 9		15:00 15:15	100 97		117 104				217	
03:15	2		8				10		15:30	108		104				201 213	
03:45	3	11	8	24			11	35	15:45	75	380	95	421			170	801
04:00	3		6				9		16:00	117		78				195	
04:15	5		14				19		16:15	120		102				222	
04:30	6	21	16	50			22	72	16:30 16:45	114 120	471	112	201			226	050
04:45	7	21	16 38	52			23 45	73	17:00	120	471	89 161	381			209 289	852
05:15	10		43				53		17:15	122		122				244	
05:30	15		53				68		17:30	100		109				209	
05:45	18	50	87	221			105	271	17:45	117	467	99	491			216	958
06:00	32		90				122		18:00 18:15	114		103				217	
06:15 06:30	42 71		92 80				134 151		18:15	81 91		94 73				175 164	
06:45	77	222	70	332			147	554	18:45	81	367	66	336			147	703
07:00	116		86				202	100000	19:00	57		50				107	
07:15	132		132				264		19:15	40		59				99	
07:30	80	420	94	276			174	004	19:30	68	220	53	202			121	124
07:45 08:00	100 94	428	64 71	376			164 165	804	19:45 20:00	64 84	229	40	202			104	431
08:15	97		48				145	The second	20:15	68		35				103	
08:30	78		65				143	States 2	20:30	41		32				73	
08:45	84	353	75	259			159	612	20:45	44	237	49	163			93	400
09:00	56		84				140		21:00	32		30				62	
09:15 09:30	82 62		65 68				147		21:15 21:30	39 27		32 22				71 49	
09:30	71	271	68 79	296			130 150	567	21:30	27	126	18	102			49	228
10:00	72	2/1	75	250			147	507	22:00	21	120	15	102			36	220
10:15	67		85				152	3.1.1.1	22:15	21		20				41	
10:30	73	0.00	60				133		22:30	18		12				30	
10:45 11:00	66 70	278	71 88	291			137 158	569	22:45 23:00	14	74	<u>12</u> 9	59			26 23	133
11:00	69		88 71				158		23:15	14		8				19	
11:30	88		75				163		23:30	11		12				23	
11:45	79	306	75	309			154	615	23:45	8	44	6	35			14	79
TOTALS	-	1996		2203				4199	TOTALS		3484		3244				6728
SPLIT %		47.5%		52.5%				38.4%	SPLIT %		51.8%	all mark	48.2%				61.6%
and the second second	and the second			10		NB	SB		EB		WB					T	otal
	DA	AILY T	OTA	LS		5,480	5.447	FILS AND	0		0					10	.927
Cherry Ball Brent Mark			Contra a		and and the second second	3,400	3,447	A DESCRIPTION OF	U		0				Destanting the state	1 10	15121

					111 1 1	Arrest a					
AM Peak Hour	07:00	06:45			07:00	PM Peak Hour	16:30	17:00			16:30
AM Pk Volume	428	382			804	PM Pk Volume	484	491			968
Pk Hr Factor	0.811	0.723			0.761	Pk Hr Factor	0.945	0.762			0.837
7 - 9 Volume	781	635	0	0	1416	4 - 6 Volume	938	872	0	0	1810
7 - 9 Peak Hour	07:00	07:00			07:00	4 - 6 Peak Hour	16:30	17:00			16:30
7 - 9 Pk Volume	428	376			804	4 - 6 Pk Volume	484	491			968
Pk Hr Factor	0.811	0.712			0.761	Pk Hr Factor	0.945	0.762		0.000	0.837





					SI	FD0 r5z	1		6 M	orniz	بالألحد
County Statio Descri Start Start	n: ption: Date:	14 5121 SR 52, 02/11/ 1200		- CR579	/HAPPY H	HILL RD./	PROSPEC	T RD.			
		Dir	ection:	E			Dir	ection:	W		
Combin Time Total	ed 1st	2nd	3rd	4th	Total	1st	2nd	3rd	4th	Total	
 0000	13	8	16	6	43	4	2	4	5	15	
58 0100	5	8	2	4	19	4	1	3	0	8	1
27 0200	3	7	2	1	13	2	2	1	4	9	I
22 0300	2	4	2	8	16	8	11	5	4	28	1
44 0400	5	4	9	15	33	11	8	19	26	64	[
97 0500	6	12	28	27	73		43	77	104	256	
329											
0600 680	22	41	77	123	263	104	114	89	110	417	I
0700 1071	138	98	117	134	487	117	188	147	132	584	
0800	114	117	106	90	427	130	99	82	82	393	!
820 0900	79	84	121	94	378	96	91	79	69	335	
713 1000	86	107	87	86	366	95	77	78	74	324	1
690 1100	80	84	106	106	376	97	91	86	86	360	
736										308	-
1200 670	82	88	98	94	362		87	71	68		-
1300 778	114	82	100	117	413	84	111	66	104	365	l
1400 921	86	92	101	117	396	131	125	144	125	525	]
1500	94	91	119	118	422	116	128	149	108	501	I
923 1600	114	124	120	149	507	116	112	144	121	493	I
1000 1700	112	150	116	118	496	155	159	95	104	513	1
1009 1800	104	109	89	72	374		59	57	75	271	
T000	704	103	5	12		00	60			<u> </u>	1

645											
1900	62	55	63	37	217	70	56	79	48	253	
470											
2000	38	40	33	37	148	39	22	30	22	113	
261									~~		
2100	24	30	26	33	113	25	20	19	22	86	
199	20	23	29	20	101	16	12	6	9	43	
2200 144	29	23	29	20	101 ]	10	12	0	9	45	
2300	17	17	15	11	60	11	9	9	6	35	
95	,ш, г	-/	10		00 1		-	-	Ū		
											-
24-Hour	Totals:				6103					6299	
12402											
											-
					-1						
			_	Pe	ak Volume		ation			<b>_</b> • • •	
		tion:				tion: W				Directions	
	Hour	Vo.	Lume		Hour	Volum		ŀ	lour	Volume	
А.М.	700		487		715	59	97		700	1071	
Р.М.	1630		531		1630	57	79	1	L630	1110	
Daily	1630		531		715	59	97	1	L630	1110	
-											

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Generated by SPS 5.0.54P

County Statio Descri Start Start	n: ption: Date:	14 5121 SR 52, 02/12/2 1200		F CR579	)/НАРРҮ НІ	LL RD./I	PROSPEC	Γ RD.			
		Dir	ection:	E			Dire	ection:	W		
Combin Time Total	ed 1st	2nd	3rd	4th	Total	1st	2nd	3rd	4th	Total	
 0000 64	11	17	15	5	48	2	4	6	4	16	
0100 39	6	4	3	5	18	8	3	6	4	21	
0200	3	4	6	3	16	4	4	3	5	16	[
32 0300	0	4	2	0	6	4	6	5	8	23	
29 0400	3	2	9	7	21	17	8	11	25	61	1
82 0500	7	9	15	31	62	35	46	80	97	258	I
320									106	404	
0600 657	23	46	73	111	253	101	102	95	100		•
0700 1052	136	98	107	128	469	121	190	156	116	583	
0800	114	105	86	88	393	101	106	80	71	358	]
751 0900	69	81	116	104	370	97	85	71	79	332	
702 1000	70	84	91	85	330	96	59	74	78	307	1
637 1100	93	102	68	64	327	90	120	80	77	367	1
694					·						-
1200 823	92	92	108	100	392	137	99	95	100	431	
1300 743	84	102	90	95	371	94	105	79	94	372	
1400	97	91	108	128	424	121	100	107	117	445	
869 1500	104	107	103	107	421	128	142	119	124	513	I
934 1600	120	119	107	122	468	105	135	125	105	470	
938 1700	125	130	114	117	486	136	149	105	98	488	
974											
1800	89	99	80	76	344	72	73	69	53	267	1

611											
1900	68	69	40	55	232	50	51	53	38	192	
424											
2000	41	48	34	49	172	36	27	31	47	141 ]	
313											
2100	37	32	32	34	135	39	32	21	18	110	
245	27	26	22	10	102	10	47	7	9	F1	
2200 154	37	26	22	18	103	18	17	/	9	51	
2300	8	14	16	7	45	11	11	11	4	37	
82	U	74	10	,	ן כד	**		بالوجالو	-	57	
											_
24-Hour	Totals:				5906					6263	
12169											
											-
						_					
				Pe	ak Volume		ation	_			
		tion:				tion: W				Directions	
	Hour	Vo.	lume		Hour	Volum		ŀ	lour	Volume	
Α.Μ.	700		469		700	58			700	1052	
Ρ.Μ.	1645		491		1630	51		1	L630	999	
Daily	1645		491		700	58	33		700	1052	

Generated by SPS 5.0.54P

Prepared by National Data & Surveying Services

## VOLUME

US 301 N/O Morningside Dr

Day: Tuesday Date: 9/22/2020

7 - 9 Peak Hour

7 - 9 Pk Volume

**Pk Hr Factor** 

07:45

661

0.955

08:00

682

0.902

City: Dade City Project #: FL20\_120203\_006

	DA	шν-	τοτμ	NIC		NB	SB		EB		WB						Т	otal
	DA	ILT	1017	ALS		12,615	11,77	0	0	THE	0						24	,385
AM Period	NB		SB	Magar.	EB	WB		DTAL	PM Period	NB		SB		EB	WE	3		TAL
00:00	17 14		23				40		12:00 12:15	225 249		236 222					461 471	
00:15 00:30	14		17 8				31 23		12:30	249		275					545	
00:45	13	59	7	55			20	114	12:45	277	1021	223	956				500	1977
01:00	8		11				19	Sec. 2	13:00	243		213					456	
01:15	12		7				19		13:15	224		223					447	
01:30 01:45	10 12	42	5 11	34			15 23	76	13:30 13:45	234 223	924	230 224	890				464 447	1814
02:00	8	42	6	54			14	10	14:00	219	524	211	050				430	1014
02:15	8		1				9		14:15	229		215					444	
02:30	9		9				18		14:30	227		226					453	
02:45	10 18	35	7	23			17	58	14:45 15:00	266	941	216	868				482	1809
03:15	14		9				23		15:15	261		234					442	
03:30	9		15				24		15:30	225		292					517	
03:45	10	51	12	39			22	90	15:45	229	943	231	971				460	1914
04:00	14		13				27		16:00	312		217					529	
04:15 04:30	9		21				30 35		16:15 16:30	250 263		184 224					434 487	
04:45	12 19	54	23 25	82			44	136	16:45	203	1104	224	849				503	1953
05:00	11	54	27	02			38	100	17:00	302	1104	250	0-15				552	1555
05:15	24		39				63		17:15	315		228					543	
05:30	25	0.000	56				81		17:30	256		186					442	
05:45		99	63	185			102	284	17:45 18:00	232	1105	182	846				414	1951
06:00 06:15	46 50		72 94				118 144		18:00	207 213		205 158					412 371	
06:30	81		98				179		18:30	162		153					315	
06:45		281	123	387			227	668	18:45	191	773	146	662				337	1435
07:00	87		121				208		19:00	156		137					293	
07:15	139		144				283		19:15	156		111					267	
07:30 07:45	162 173 5	561	185 174	624			347 347	1185	19:30 19:45	137 165	614	127 134	509				264 299	1123
07:45	157	501	159	024			316	1105	20:00	141	014	91	509				232	1125
08:15	165		149				314		20:15	111		111					222	
08:30	166		189				355		20:30	101		67					168	
08:45		644	185	682			341	1326	20:45	100	453	51	320				151	773
09:00 09:15	145 163		186 175				331 338		21:00 21:15	102 83		68 61					170 144	
09:30	188		175				363		21:30	71		41					112	
09:45		690	195	731			389	1421	21:45	42	298	39	209				81	507
10:00	196		172				368		22:00	58		50					108	
10:15	162		196				358		22:15	46		34					80	
10:30 10:45	190 214 7	762	198 198	764			388 412	1526	22:30 22:45	40 36	180	34 22	140				74 58	320
10:45	185	/02	237	704			412	1520	23:00	45	100	17	140				62	520
11:15	220		216				436		23:15	17		19					36	
11:30	226		218				444		23:30	33		17					50	
11:45		368	210	881			447	1749	23:45	18	113	10	63	/ Children and			28	176
TOTALS		146	1	4487				8633	TOTALS		8469		7283					15752
SPLIT %	48	8.0%		52.0%				35.4%	SPLIT %		53.8%		46.2%					64.6%
	DAI	LΥ Τ	ота	LS		NB	SB		EB		WB				and the second		То	
	Carlos and	1				12,615	11,770		0	- And a fam	0						24,	385
AM Peak Hour	1	1:45		11:45				11:45	PM Peak Hour		16:30		15:15				12.55	16:30
AM Pk Volume		981		943				1924	PM Pk Volume		1159		974					2085
Pk Hr Factor	A CONTRACTOR OF A CONTRACTOR OFTA CONT	.908	-	0.857	1.4			0.883	Pk Hr Factor	102530	0.920		0.834				C. S. P. S.	0.944
7 - 9 Volume	1	205		1306				2511	4 - 6 Volume		2209		1695					3904

07:45 4 - 6 Peak Hour

4 - 6 Pk Volume

Pk Hr Factor

1332

0.938

16:30

1159

0.920

16:30

926

0.926

16:30

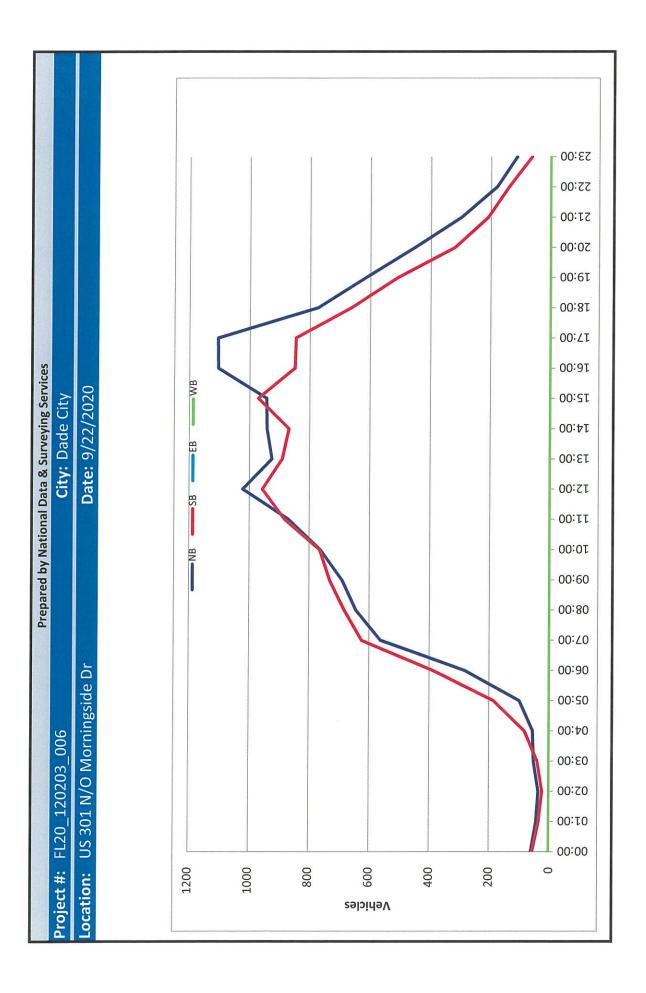
2085

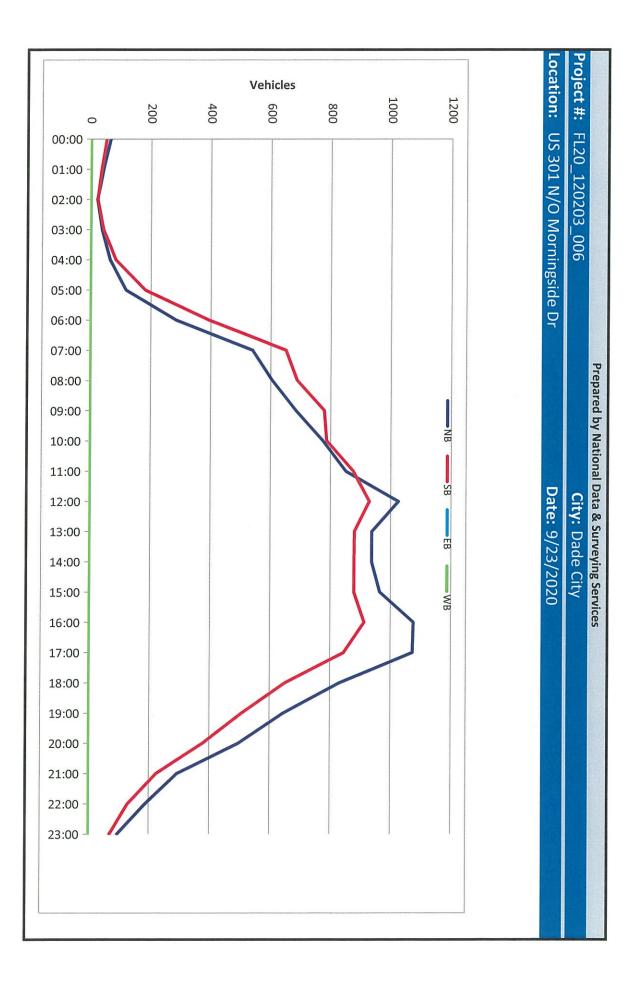
## Prepared by National Data & Surveying Services VOLUME US 301 N/O Morningside Dr

Day: Wednesday Date: 9/23/2020

City: Dade City Project #: FL20\_120203\_006

2011 Internation	159			Anne		NB	17 Carrie	SB	(SYNM)	EB		WB							т	otal
	D	AILY	τοτ	ALS		12,642	2	11,87	1	0		<u>vvв</u> 0							-	1,513
AM Period	NB		SB		EB	WB			- DTAL	PM Period	NB		SB		EB		WB		-	OTAL
00:00	21		11				1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	32		12:00	247		234		20				481	
00:15	14		20					34		12:15	264		238						502	
00:30	17	64	10	<b>F</b> 4				27	445	12:30	258	1025	238	000					496	1054
00:45	12 11	64	10 11	51				22	115	12:45 13:00	256 243	1025	219 235	929					475	1954
01:15	11		8					19		13:15	243		188						4/8	
01:30	8		8					16		13:30	218		242						460	
01:45	11	41	8	35				19	76	13:45	224	937	215	880					439	1817
02:00	2		7					9		14:00	231		216						447	
02:15	8		0					8		14:15 14:30	204		214						418	
02:30 02:45	9	22	11 5	23				20 8	45	14:30	245 257	937	227 222	879					472 479	1816
03:00	5	22	6	25				11	45	15:00	240	557	196	075					436	1810
03:15	11		10					21		15:15	237		212						449	
03:30	1		14					15		15:30	260		250						510	
03:45	20	37	12	42				32	79	15:45	227	964	221	879					448	1843
04:00	13		18					31		16:00	276		214						490	
04:15 04:30	21 11		13 27					34 38		16:15 16:30	258 259		246 219						504 478	
04:45	19	64	25	83				44	147	16:45	283	1076	234	913					517	1989
05:00	23		36					59		17:00	273	10/0	243	510					516	1909
05:15	25		27					52		17:15	283		230						513	
05:30	25		69					94		17:30	259		170						429	
05:45	44	117	49	181				93	298	17:45	258	1073	202	845					460	1918
06:00 06:15	48 63		68 101					116 164		18:00 18:15	236 235		184 148						420 383	
06:30	77		96					173		18:30	184		171						355	
06:45	96	284	128	393				224	677	18:45	176	831	147	650					323	1481
07:00	109		140					249		19:00	183		134						317	
07:15	122		155					277		19:15	150		112						262	
07:30	141	520	176	650				317	1100	19:30 19:45	157	CAE	145	507					302	1150
07:45 08:00	167 131	539	179 163	650				346 294	1189	20:00	<u>155</u> 148	645	116 110	507					271 258	1152
08:15	170		165					335		20:15	130		92						222	
08:30	165		183					348		20:30	114		73						187	
08:45	139	605	177	688				316	1293	20:45	104	496	103	378					207	874
09:00	152		182					334		21:00	79		80						159	
09:15	160		180					340		21:15 21:30	65		43						108	
09:30 09:45	181 191	684	218 198	778				399 389	1462	21:30	80 69	293	51 50	224					131 119	517
10:00	199	004	187	//0				386	1402	22:00	58	235	40	224					98	517
10:15	175		188					363		22:15	53		40						93	
10:30	208		208					416		22:30	44		30						74	
10:45	192	774	203	786				395	1560	22:45	33	188	21	131					54	319
11:00	215		219					434		23:00 23:15	26		18						44	
11:15 11:30	216 195		198 236					414 431		23:30	26 24		17 16						43 40	
11:45	224	850	222	875				446	1725	23:45	20	96	20	71					40	167
TOTALS		4081		4585					8666	TOTALS		8561		7286						15847
SPLIT %		47.1%		52.9%					35.4%	SPLIT %		54.0%		46.0%			(inclusion)		See.	64.6%
	D	AILY T	OTA	15		NB		SB		EB		WB							To	otal
			OTA	25		12,642		11,871		0		0							24,	,513
AM Peak Hour		11:45		11:45					11:45	PM Peak Hour	S-19-345	16:30	affice but he	16:15						16:30
AM Pk Volume		993		932					1925	PM Pk Volume		1098		942						2024
Pk Hr Factor		0.940		0.979					0.959	Pk Hr Factor		0.970		0.957						0.979
7 - 9 Volume		1144		1338	0	-	0		2482	4 - 6 Volume	1.4.410	2149		1758	Contraction of	0		0	90, 301	3907
		07:45		07:45					07:45	4 - 6 Peak Hour		16:30		16:15						16:30
7 - 9 Peak Hour									Contraction of the local division of the loc											
7 - 9 Peak Hour 7 - 9 Pk Volume		633		690					1323	4 - 6 Pk Volume		1098		942						2024





# Prepared by National Data & Surveying Services **VOLUME** Fort King Rd N/O Morningside Dr

Day: Tuesday Date: 9/22/2020

DAILY TOTALS         2,839         2,869         0         0         5,708           AM Period 00:15         1         2         12         12:00         39         30         30         30         30         30         30         30         30         30         30         1         31         31445         65         50         55         52         247         117         460         30         30	and the second	TO COM H				the state of the s	ND	SB		EB		IA/D	LU HORA				2 80 T	otal
AM Period         NB         SB         EB         WB         TOTAL         PM Period         NB         SB         EB         WB         TOTAL           00:00         6         6         6         12         12         12:00         39         39         39         96         96           00:30         4         2         6         27         12:30         41         176         32         166         87         34           00:30         1         0         2         13:30         44         13:46         46         97         115         115         105         36         97         113         105         31:44         33         34         14:39         54         99         113         105         36         113         105         36         113         113:30         44         13:400         50         50         53         113         14:39         54         22:0         53         113         14:39         54         99         113         113:0         14:39         56         113         116:00         30         36         57         30         38         57         50         50         56 <th></th> <th>D</th> <th>AILY</th> <th>τοτ</th> <th>ALS</th> <th></th> <th>NB 2.839</th> <th></th> <th>9</th> <th>Construction of the second sec</th> <th></th> <th><u>WB</u></th> <th></th> <th></th> <th></th> <th></th> <th>and the second second</th> <th></th>		D	AILY	τοτ	ALS		NB 2.839		9	Construction of the second sec		<u>WB</u>					and the second second	
	AM Period	NB		SB		FR					NB		SR		FR	WB		
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07:00         88         49         137         19:00         30         29         50           07:15         89         101         190         19:15         35         27         62           07:30         58         60         118         19:30         28         18         46           07:45         53         288         44         254         97         542         19:45         31         124         31         105         62         229           08:00         44         42         86         20:00         27         23         50         50           08:15         67         36         103         20:15         20         11         31         27           08:30         42         51         93         20:30         10         17         83         141           09:00         35         37         72         21:00         15         15         30         25         27         93         20:30         10         17         29         29         29         29         29         29         29         29         20         21:00         15         15         10 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>States -</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									States -									
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09:00 09:15 29       35       37       72       21:00 71       15       15       15       30         09:15 09:30       44       38       70       84       309       12       17       8       25         09:30       44       38       82       21:30       12       17       29       29         09:45       31       139       53       170       84       309       21:45       16       60       8       48       24       108         10:00       32       48       70       22:00       9       6       15       15       13       108       13       108       13       14       15       1			112122		1000							100						
09:15       29       42       71       21:15       17       8       25         09:30       44       38       82       21:30       12       17       29       29         09:45       31       139       53       170       84       309       21:45       16       60       8       48       24       108         10:00       32       48       80       80       22:00       9       6       15       15       15         10:15       26       44       70       22:15       12       11       23       15       15       15       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16       16       17       15       16       16       16       16       16       16       16       16       16       16       16       17       16       1			197		170				367			79		62				141
09:30       44       38       82       21:30       12       17       29         09:45       31       139       53       170       84       309       21:45       16       60       8       48       24       108         10:00       32       48       309       21:45       16       60       8       48       24       108         10:15       26       44       70       22:15       12       11       23       15         10:30       40       47       70       22:15       12       11       23       23         10:35       30       128       36       175       66       303       22:45       6       36       9       30       13       33         11:30       31       35       66       23:00       8       10       18         11:30       23       46       31       37       31       18       30       <	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1																	
09:45       31       139       53       170       84       309       21:45       16       60       8       48       24       108         10:00       32       48       80       22:00       9       6       15       15       15       15       15       15       15       15       15       15       15       15       15       15       15       15       15       15       16       60       8       48       15       15       15       15       15       15       15       15       15       15       16       10:30       40       47       70       22:30       9       4       13										22 WY (MODELS 1 ) TO 22								
10:00       32       48       80       22:00       9       6       15       12         10:15       26       44       70       87       22:15       12       11       23         10:30       40       47       87       22:30       9       4       13         10:45       30       128       36       175       66       303       22:45       6       36       9       30       15       66         11:00       31       35       66       23:00       8       10       18       18         11:15       44       55       99       23:15       7       11       18       12         11:30       23       46       69       23:30       6       6       12       12         11:45       45       143       43       179       88       322       23:45       6       27       3       30       9       57         TOTALS       1113       1166       2279       TOTALS       1703       3422       34       349       51.2%       39.9%       SPLIT %       50.3%       49.7%       60.1         DAULY TOTALS       <			139		170				309	21:45		60		48				108
10:30       40       47       87       22:30       9       4       13         10:45       30       128       36       175       66       303       22:45       6       36       9       30       15       66         11:00       31       35       66       303       22:45       6       36       9       30       15       66         11:00       31       35       66       23:00       8       10       18       18       18       18       18       18       18       12       18       12       13       12       12       12       12       12       12       12       12       12       12       12       12       13       14       14       15       16       1726											-							atte series
10:45       30       128       36       175       66       303       22:45       6       36       9       30       15       66         11:00       31       35       66       23:00       8       10       18       12       13       143       116       124       143       143 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>																		
11:00       31       35       66       23:00       8       10       18         11:15       44       55       99       23:15       7       11       18         11:30       23       46       69       23:30       6       6       12         11:45       45       143       43       179       88       322       23:45       6       27       3       30       9       57         TOTALS       1113       1166       2279       TOTALS       1726       1703       3429         SPLIT %       48.8%       51.2%       39.9%       SPLIT %       50.3%       49.7%       60.1%			170		175			Contraction of the	202			26		20			and the second se	66
11:15       44       55       99       23:15       7       11       18         11:30       23       46       69       23:30       6       6       12         11:45       45       143       43       179       88       322       23:45       6       6       27       3       30       9       57         TOTALS       1113       1166       2279       TOTALS       1726       1703       3429         SPLIT %       48.8%       51.2%       39.9%       SPLIT %       50.3%       49.7%       60.1%			128		1/5				503			30		50				00
11:30       23       46       69       23:30       6       6       7       7       7       12       9       57         11:45       45       143       43       179       88       322       23:45       6       27       3       30       9       57         TOTALS       1113       1166       2279       TOTALS       1726       1703       3425         SPLIT %       48.8%       51.2%       39.9%       SPLIT %       50.3%       49.7%       60.1	Transport Processory	1000000																
TOTALS         1113         1166         2279         TOTALS         1726         1703         3429           SPLIT %         48.8%         51.2%         39.9%         SPLIT %         50.3%         49.7%         60.1%           DAULY TOTALS         NB         SB         EB         WB         Total		23		46				and a second			6		6				12	Self The se
SPLIT %         48.8%         51.2%         39.9%         SPLIT %         50.3%         49.7%         60.1           DAILY TOTALS         NB         SB         EB         WB         Total	11:45	45	143	43	179			88	322	23:45	6	27	3	30			9	57
DAILY TOTALS NB SB EB WB Total	TOTALS		1113		1166				2279	TOTALS		1726		1703				3429
	SPLIT %		48.8%		51.2%				39.9%	SPLIT %		50.3%		49.7%				60.1%
2,839 2,869 0 0 5,708		D		OTA	15		NB	SB		EB		WB					Т	otal
		U	AILT	UTA	125		2,839	2,869		0		0					5,	708

	at most that the second second		<b>-</b> )	000	,005	U	U				5,700
AM Peak Hour	07:00	07:00			07:00	PM Peak Hour	13:30	16:30			16:30
AM Pk Volume	288	254			542	PM Pk Volume	230	281			505
Pk Hr Factor	0.809	0.629			0.713	Pk Hr Factor	0.799	0.826			0.902
7 - 9 Volume	485	424	0	0	909	4 - 6 Volume	435	473	0	0	908
7 - 9 Peak Hour	07:00	07:00			07:00	4 - 6 Peak Hour	17:00	16:30			16:30
7 - 9 Pk Volume	288	254			542	4 - 6 Pk Volume	230	281			505
Pk Hr Factor	0.809	0.629			0.713	Pk Hr Factor	0.885	0.826	0.000	0.000	0.902

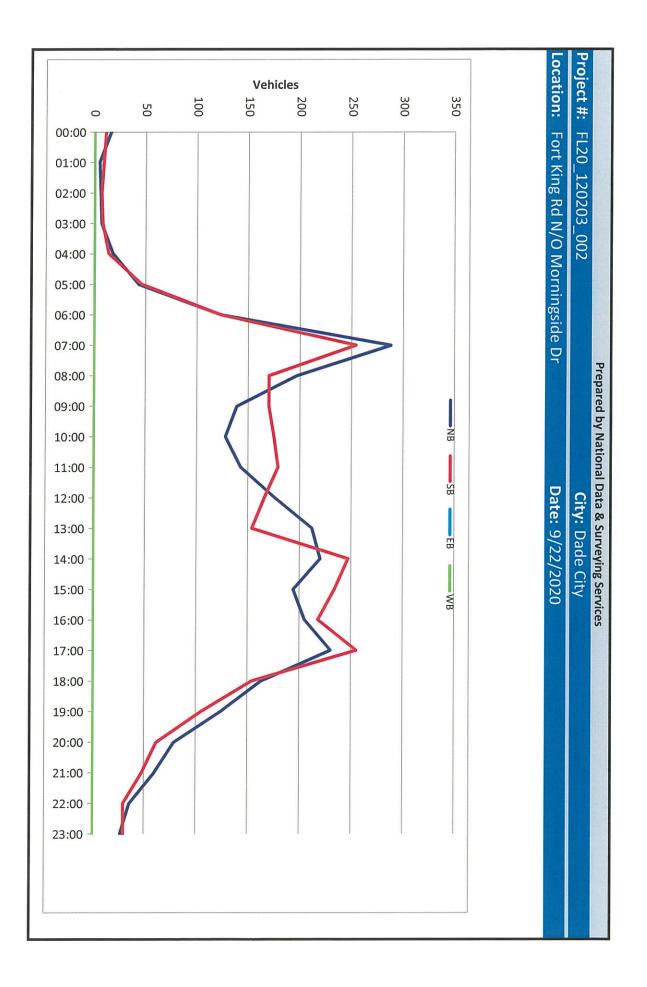
# Prepared by National Data & Surveying Services VOLUME

# Fort King Rd N/O Morningside Dr

Day: Wednesday Date: 9/23/2020

City: Dade City Project #: FL20\_120203\_002

and the second						NB		SB		EB		WB	i chi se		1015622			L T	otal
	D	AILY -	ΤΟΤ	ALS		2,905		2,937	7	0		0						-	,842
AM Period	NB		SB		EB	WB			DTAL	PM Period	NB		SB		EB	W	'B	ТС	DTAL
00:00	10		4					14		12:00	40		47					87	
00:15	3		2				5	5		12:15	39		51					90	
00:30	8	22	4	10				12 2	22	12:30 12:45	48 41	169	39 44	101				87	349
00:45 01:00	2	23	0	10				5	33	13:00	61	168	39	181				85 100	349
01:15	4		4					8		13:15	61		42					103	
01:30	3		1					4		13:30	47		38					85	
01:45	2	11	5	13				7	24	13:45	76	245	36	155				112	400
02:00	1		2					3		14:00	58		54					112	
02:15	1		2					3		14:15 14:30	55 60		92 71					147 131	
02:30 02:45	3 2	7	3	8				3	15	14:45	44	217	58	275				102	492
03:00	0	/	2	0				2	15	15:00	38	21/	48	215				86	452
03:15	3		3					6		15:15	48		64					112	
03:30	1		3					4		15:30	45		52					97	
03:45	3	7	0	8				3	15	15:45	40	171	42	206				82	377
04:00	4		1					5		16:00	48		47					95	
04:15 04:30	4 3		1 8					5 11		16:15 16:30 r	47 67		40 51					87 118	
04:30	6	17	8 5	15				11	32	16:45 <i>f</i>	46	208	87	225				133	433
05:00	3	1/	7	15				10	52	17:00 +	55	200	71	225				126	433
05:15	5		7					12		17:15 🔶	44		63					107	
05:30	14		17					31		17:30	48		53					101	
05:45	23	45	22	53				45	98	17:45	68	215	41	228				109	443
06:00	23		13					36		18:00	41		46					87	
06:15	24		25					49		18:15 18:30	55		52					107	
06:30 06:45	24 50	121	46 48	132				70 98	253	18:45	35 43	174	52 43	193				87 86	367
07:00	83	121	68	152				151	233	19:00	39	1/4	29	195				68	307
07:15	84		101					185		19:15	41		26					67	
07:30	54		57					111		19:30	44		34					78	
07:45	53	274	46	272				99	546	19:45	38	162	30	119				68	281
08:00	50		38					88		20:00	37		30					67	
08:15	60		51					111		20:15 20:30	32		18					50	
08:30 08:45	40 36	186	48 43	180				88 79	366	20:30	12 16	97	15 16	79				27 32	176
09:00	43	100	30	180				73	500	21:00	15	57	23	15				38	170
09:15	37		25					62		21:15	14		16					30	
09:30	33		40					73		21:30	15		7					22	
09:45	45	158	43	138				88	296	21:45	12	56	14	60				26	116
10:00	29		52					81		22:00	17		7					24	
10:15	30		46					76		22:15	13		18					31	
10:30	36 32	127	48 26	172				84 58	299	22:30 22:45	16 10	56	9 9	43				25 19	99
10:45 11:00	32	127	34	1/2				72	235	23:00	4	50	6	45				10	35
11:15	33		46					79		23:15	6		12					18	
11:30	36		30					66		23:30	4		7					11	
11:45	37	144	31	141				68	285	23:45	2	16	6	31				8	47
TOTALS		1120		1142					2262	TOTALS		1785		1795			S. S.		3580
SPLIT %		49.5%		50.5%					38.7%	SPLIT %		49.9%		50.1%	.a				61.3%
		AILY T	OTA	15		NB	Uper P	SB		EB		WB		Sugar					otal
	UF	alet 1	UTA	123		2,905		2,937		0		0						5,8	842
AM Peak Hour		07:00	17000	06:45					07:00	PM Peak Hour		13:45		14:00				1	13:45
AM Pk Volume		274		274					546	PM Pk Volume		249		275					502
Pk Hr Factor		0.815		0.678				a manual	0.738	Pk Hr Factor		0.819		0.747				1900	0.854
7 - 9 Volume		460	1000	452	0	N. Contraction	0	12.4.315	912	4 - 6 Volume		423		453	C	)	0		876
7 - 9 Peak Hour		07:00		07:00					07:00	4 - 6 Peak Hour		16:15		16:45					16:30
									and the second second second										
7 - 9 Pk Volume		274		272					546	4 - 6 Pk Volume		215		274					484





# Prepared by National Data & Surveying Services VOLUME Fort King Rd S/O Morningside Dr

Day: Tuesday Date: 9/22/2020

299

0.662

329

0.709

7 - 9 Pk Volume

Pk Hr Factor

City: Dade City
Project #: FL20\_120203\_003

618

0.954

	SIL LES					NB		SB	EB		WB		State				Т	otal
	C	DAILY	тот	ALS		3,258		3,500	0	Profile S	0						a second second second	758
AM Period	NB		SB	R SANGE	EB	WB	(usile	TOTAL	PM Period	NB		SB		EB	W	В	TC	DTAL
00:00	5		7					12	12:00	40		52					92	
00:15	3		3					6	12:15 12:30	52		53					105	
00:30 00:45	1 4	13	2	14				3 6 27	12:30	40	190	55 44	204				95 102	394
01:00	1	15	6	14				7	13:00	49	150	47	204				96	334
01:15	2		3					5	13:15	58		49					107	
01:30	1		1	4.0				2	13:30	57		48	100				105	
01:45	2	6	2	12				4 18 4	13:45	56	220	<u>39</u> 50	183				95 121	403
02:15	1		3					4	14:15	69		89					158	
02:30	3		1					4	14:30	61		78					139	
02:45	3	7	2	10				5 17	14:45	56	257	52	269				108	526
03:00	0		4					4	15:00	56		75					131	
03:15 03:30	3		1 0					4	15:15 15:30	60 44		79 91					139 135	
03:45	3	7	3	8				6 15	15:45	62	222	63	308				125	530
04:00	3		1	0				4	16:00	51		60	000				111	550
04:15	2		1					3	16:15	56		57					113	
04:30	6		6	10				12	16:30 🖈	62		92					154	
04:45	4	15	5 10	13				<u>9 28</u> 13	16:45 Ø	67 67	236	78 95	287				145	523
05:15	11		6					15	17:15 4	82		75					157	
05:30	17		15					32	17:30	71		62					133	
05:45	17	48	27	58				44 106		61	281	73	305				134	586
06:00	30		15					45	18:00	56		52					108	
06:15 06:30	30 32		27 37					57 69	18:15 18:30	71 60		53					124	
06:45	64	156	37	116				101 272		43	230	51 50	206				111 93	436
07:00	116	150	58	110				174	19:00	31	250	45	200				76	430
07:15	98		113					211	19:15	37		37					74	
07:30	56		74					130	19:30	38		34					72	
07:45	59	329	<u>54</u> 48	299				113 628	19:45 20:00	30	136	35	151				65	287
08:00 08:15	45 66		48					93 108	20:15	27 19		37 31					64 50	
08:30	46		65					111	20:30	17		21					38	
08:45	48	205	51	206				99 411	20:45	19	82	19	108				38	190
09:00	46		43					89	21:00	13		19					32	
09:15	38		55					93	21:15	23		16					39	
09:30 09:45	42 29	155	46 56	200				88 85 355	21:30 21:45	13 14	63	16 8	59				29 22	122
10:00	56	100	55	200				111	22:00	8	05	6	39				14	122
10:15	28		42					70	22:15	14		17					31	
10:30	44		54					98	22:30	11		10					21	
10:45	31	159	45	196				76 355	22:45	7	40	11	44				18	84
11:00 11:15	37 47		48 57					85 104	23:00 23:15	4 10		14 13					18 23	
11:15	37		49					86	23:30	4		13 5					9	
11:45	55	176	54	208				109 384	23:45	7	25	4	36				11	61
TOTALS		1276	AVE S	1340	A States and			2616	TOTALS		1982		2160					4142
SPLIT %		48.8%		51.2%				38.79	6 SPLIT %		47.9%		52.1%					61.3%
	D	AILY -	τοτα	IS		NB		SB	EB		WB						and the second se	otal
	0					3,258		3,500	0		0						6,	758
AM Peak Hour		06:45		07:00				07:00	The second s		16:45		16:30	1240340				16:30
AM Pk Volume		334		299				628	PM Pk Volume		287		340					618
Pk Hr Factor		0.720		0.662				0.744	and the second se		0.875	A Marine	0.895					0.954
7 - 9 Volume		534		505				1039	4 - 6 Volume		517		592		D	0		1109
7 - 9 Peak Hour		07:00		07:00				07:00			16:45		16:30					16:30
7 - 9 Pk Volume		329		299				628	4 - 6 Pk Volume		287		340					618

4 - 6 Pk Volume

Pk Hr Factor

340

0.895

287

0.875

628

Prepared by National Data & Surveying Services

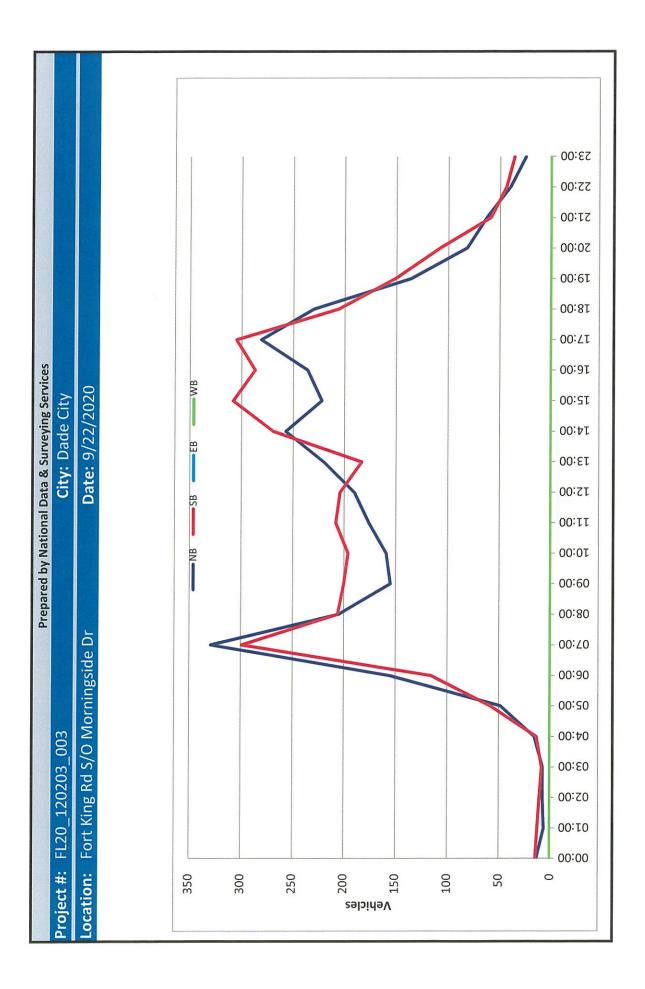
### VOLUME

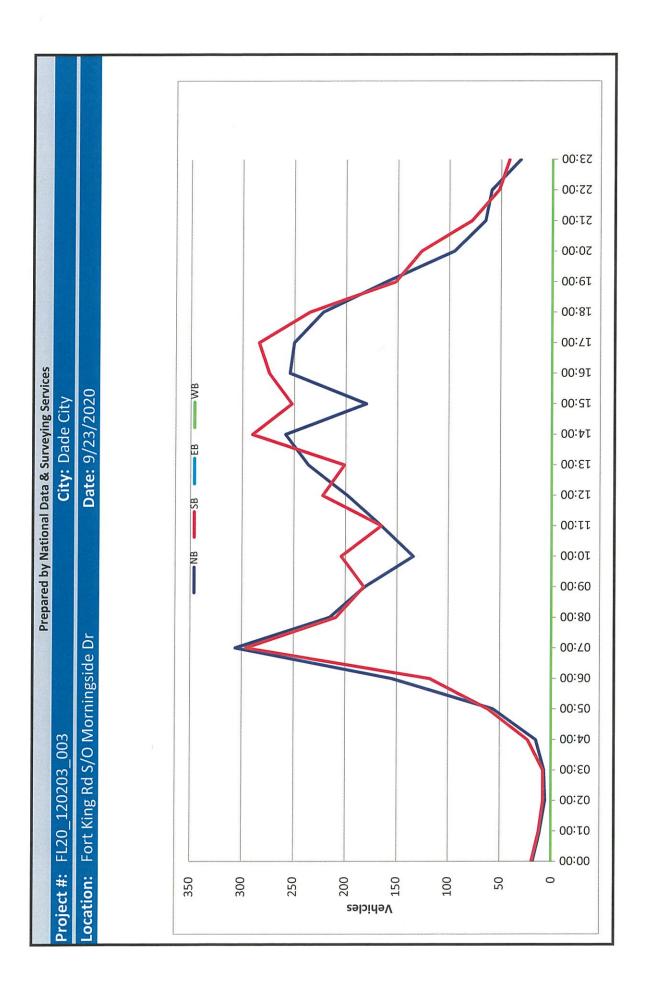
Fort King Rd S/O Morningside Dr

Day: Wednesday Date: 9/23/2020

City: Dade City Project #: FL20\_120203\_003

	D	AILY	τοτ	ALS		NB 3,278		SB	4	EB 0	1	WB 0								otal 792
AB4 Deviced	NID		CD		EB		•	3,51	4 DTAL	PM Period	NID	0	CD		EB		14/D			DTAL
AM Period 00:00	NB 8		<b>SB</b> 9		ED	WB		17	JTAL	12:00	<b>NB</b> 40		<b>SB</b> 55		ED		WB	291.1995	95	TAL
00:15	2		4					6		12:15	50		67						117	
00:30	6		5					11		12:30	54		53						107	
00:45	2	18	1	19				3	37	12:45	54	198	47	222					101	420
01:00	6		3					9		13:00	56		48						104	
01:15 01:30	2		5 1					7 2		13:15 13:30	66 59		58 52						124	
01:45	2	11	3	12				5	23	13:45	55	236	43	201					98	437
02:00	2		2					4		14:00	63		48						111	
02:15	3		3					6		14:15	72		91						163	
02:30	1	6	3	0				4		14:30	72	250	91	200					163	
02:45	0	6	0	8				0	14	14:45 15:00	51 37	258	60 66	290					111 103	548
03:15	3		3					6		15:15	48		72						120	
03:30	1		1					2		15:30	47		64						111	
03:45	3	7	2	8				5	15	15:45	48	180	50	252					98	432
04:00	5		4					9		16:00	59		59						118	
04:15 04:30	4 3		4 9					8 12		16:15 16:30 て	58 78		56 68						114 146	
04:30	3	15	6	23				9	38	16:45 -	59	254	91	274					140	528
04:45	5	10	8	23				13	50	17:00 -	53	2.54	90	2/4					143	520
05:15	11		10					21		17:15 -	55		77						132	
05:30	16		19					35		17:30	75		66						141	
05:45	24	56	24	61				48	117	17:45	67	250	51	284					118	534
06:00 06:15	29 26		11 22					40 48		18:00 18:15	57 66		62 68						119 134	
06:30	42		40					82		18:30	54		58						112	
06:45	58	155	45	118				103	273	18:45	45	222	47	235					92	457
07:00	93		68					161		19:00	37		34						71	
07:15	95		97					192		19:15	38		30						68	ALC: NO
07:30	57 61	306	69 62	296				126 123	602	19:30 19:45	38 48	161	49 39	152					87 87	313
07:45 08:00	66	300	43	290				109	602	20:00	32	161	48	152					80	313
08:15	61		61					122		20:15	24		33						57	
08:30	48		49					97		20:30	14		24						38	
08:45	40	215	56	209				96	424	20:45	25	95	22	127					47	222
09:00	45		46					91		21:00 21:15	17		32 19						49 37	
09:15 09:30	44 38		34 54					78 92		21:30	18 18		19						29	
09:45	54	181	48	182				102	363	21:45	12	65	16	78					28	143
10:00	34		54					88		22:00	19		9						28	
10:15	35		57					92		22:15	15		20						35	
10:30	26	124	58	204				84	220	22:30	12	50	9	50					21	111
10:45 11:00	39 42	134	35 42	204				74 84	338	22:45 23:00	<u>13</u> 10	59	14 11	52					27	111
11:15	47		42					89		23:15	7		14						21	
11:30	42		39					81		23:30	7		11						18	
11:45	34	165	42	165				76	330	23:45	7	31	6	42					13	73
TOTALS		1269		1305					2574	TOTALS		2009		2209						4218
SPLIT %		49.3%		50.7%					37.9%	SPLIT %		47.6%		52.4%			State of			62.1%
	D	AILY T	OTA	15		NB		SB		EB		WB							То	otal
			OTA	20		3,278		3,514		0	and a	0							6,7	792
AM Peak Hour		07:00		07:00		C. C. C. D. C.	CHINE IS	11111	07:00	PM Peak Hour	1996	17:30	24	16:30	102197		1 4513		1	16:30
AM Pk Volume		306		296					602	PM Pk Volume		265		326						571
Pk Hr Factor		0.805		0.763					0.784	Pk Hr Factor		0.883		0.896	-			and the		0.952
7 - 9 Volume	(august)	521	1	505	0	15-30-24-2	0		1026	4 - 6 Volume		504	Bah	558		0		0		1062
7 - 9 Peak Hour		07:00		07:00					07:00	4 - 6 Peak Hour		16:00		16:30						16:30
7 - 9 Pk Volume		306		296					602	4 - 6 Pk Volume		254		326						571
Pk Hr Factor	1200	0.805	Lake .	0.763	0.00	0	0.000		0.784	Pk Hr Factor	Call Call	0.814	Contraction of the	0.896	The second	0.000	210125	0.000		0.952





# Prepared by National Data & Surveying Services **VOLUME** Morningside Dr E/O SR 52

Day: Tuesday Date: 9/22/2020

00:00         6         6         12         12:00         18         1           00:15         0         2         2         12:15         24         22           00:30         0         0         0         12:30         21         1           00:45         1         7         0         8         1         15         12:45         30         93         2           01:00         3         0         3         13:00         22         2         2         1         1           01:15         2         1         3         13:15         19         3         19         2         1         3         13:15         19         3         19         2         2         1         3         13:15         19         3         19         2         1         3         19         2         1         3         19         2         1         3         19         2         1         3         16         76         2         1         3         16         76         2         1         3         3         12         1         3         14:30         41         2         1	1 4 0 71 3 1 7 7 4 105 6 4 4 5 5 8 133 3 4	45 50 46 40 1 57 98 66	164 181
00:00         6         6         12         12:00         18         1           00:15         0         2         2         12:15         24         2           00:30         0         0         0         12:30         21         1           00:45         1         7         0         8         1         15         12:45         30         93         2           01:00         3         0         3         13:00         22         2         2         1 <td< th=""><th>6 1 4 0 71 3 1 7 7 4 105 6 4 5 5 8 133 3 4</th><th>34 45 35 50 45 50 46 40 1 57 98 66 37 2</th><th><u>164</u> <u>181</u></th></td<>	6 1 4 0 71 3 1 7 7 4 105 6 4 5 5 8 133 3 4	34 45 35 50 45 50 46 40 1 57 98 66 37 2	<u>164</u> <u>181</u>
00:15         0         2         2         12:15         24         2           00:30         0         0         0         0         12:30         21         1           00:45         1         7         0         8         1         15         12:30         21         1           00:45         1         7         0         8         1         15         12:45         30         93         2           01:00         3         0         3         13:00         22         2         2           01:15         2         1         3         13:00         19         3           01:30         1         0         1         0         7         13:45         16         76         2           01:45         0         6         0         1         0         7         13:45         16         76         2           02:00         0         0         0         14:00         21         3           02:15         1         1         2         14:15         44         5           02:30         0         0         0         14:30         4	1 4 0 71 3 1 7 7 4 105 6 4 4 5 5 8 133 3 4	45 35 50 1 45 50 46 40 1 57 98 66 37 2	181
00:30         0         0         0         12:30         21         1           00:45         1         7         0         8         1         15         12:45         30         93         2           01:00         3         0         3         1         15         12:45         30         93         2           01:00         3         0         3         13:10         22         2         2           01:15         2         1         3         13:15         19         3           01:30         1         0         1         13:30         19         2           01:45         0         6         0         1         0         7         13:45         16         76         2           02:00         0         0         0         14:00         21         3	4 0 71 3 1 7 7 4 105 6 4 4 5 5 8 133 3 4	35 50 1 45 50 46 40 1 57 98 66 37 2	181
00:45         1         7         0         8         1         15         12:45         30         93         2           01:00         3         0         3         0         3         13:00         22         2         2           01:15         2         1         3         13:00         22         2         2           01:30         1         0         1         13:30         19         2           01:45         0         6         1         0         7         13:45         16         76         2           02:00         0         0         0         14:00         21         33           02:15         1         1         2         14:15         44         5           02:30         0         0         0         14:30         41         2           02:45         0         1         2         3         2         4         14:45         19         125         1           03:00         1         0         1         15:00         19         2         19         2	0 71 3 1 7 4 105 6 4 5 8 133 3 4	50         1           45         50           46         40           40         1           57         98           66         37	181
01:00         3         0         3         13:00         22         2         2         2         1         3         13:00         22         2         2         2         1         3         13:00         13:15         19         3         19         3         10         11         13:30         19         2         10         11         13:30         19         2         10         7         13:45         16         76         2         10         7         13:45         16         76         2         10         11         1         2         14:10         21         3         3         02:10         11         11         2         14:15         14         14         5         14         12         2         14:15         14         14         2         14         12         2         14         12         2         14         12         2         14         12         12         12         12         12         14         15         14         12         12         12         12         12         12         12         12         12         12         12         12         12         12	3 1 7 4 105 6 4 5 8 133 3 4	45 50 46 40 1 57 98 66 37 2	181
01:15         2         1         3         13:15         19         3           01:30         1         0         1         13:30         19         2           01:45         0         6         0         1         0         7         13:45         16         76         2           02:00         0         0         0         7         13:45         16         76         2           02:00         0         0         0         1         2         14:10         21         3           02:15         1         1         2         14:15         44         55           02:30         0         0         0         14:30         41         22           02:45         0         1         2         3         2         4         14:45         19         125         1           03:00         1         0         1         15:00         19         22	1 7 4 105 6 4 5 8 133 3 4	50 46 40 1 57 98 66 37 2	
01:30 01:45         1         0         1         13:30 0         19         2           01:45         0         6         0         1         0         7         13:45         16         76         2           02:00         0         0         0         0         14:00         21         3           02:15         1         1         2         14:15         44         5           02:30         0         0         0         14:30         41         2           02:45         0         1         2         3         2         4         14:45         19         125         1           03:00         1         0         1         15:00         19         2	7 4 105 6 4 5 8 133 3 4	46 40 1 57 98 66 37 2	
01:45         0         6         0         1         0         7         13:45         16         76         2           02:00         0         0         0         14:00         21         3           02:15         1         1         2         14:15         44         5           02:30         0         0         0         14:30         41         2           02:45         0         1         2         3         2         4         14:45         19         125         1           03:00         1         0         1         15:00         19         2	4 105 6 4 5 8 133 3 4	40 1 57 98 66 37 2	
02:15       1       1       2       14:15       44       5         02:30       0       0       0       14:30       41       2         02:45       0       1       2       3       2       4       14:45       19       125       1         03:00       1       0       1       15:00       19       22       2       2       19       125       1	4 5 <u>8 133</u> 3 4	98 66 37 2	25.0
02:30         0         0         14:30         41         2           02:45         0         1         2         3         2         4         14:45         19         125         1           03:00         1         0         1         15:00         19         22	5 <u>8 133</u> 3 4	66 37 2	25.0
02:45         0         1         2         3         2         4         14:45         19         125         1.           03:00         1         0         1         15:00         19         22         3         2         4         14:45         19         125         1.	8 133 3 4	37 2	250
<b>03:00</b> 1 0 1 <b>15:00</b> 19 2	3 4		
	4		258
<b>03:15</b> 1 1 2 <b>15:15</b> 24 2.		42	
<b>O3:30</b> 2 0 2 <b>15:30</b> 28 1	4	47	
<b>03:45</b> 1 5 0 1 1 6 <b>15:45</b> 16 87 2		and the second se	177
<b>04:00</b> 2 0 2 <b>16:00</b> 19 22		42	
<b>04:15</b> 1 0 1 <b>16:15</b> 20 20	J	40	
<b>04:30</b> 2 3 5 <b>16:30</b> 40 2		69	
04:45 5 10 3 6 8 16 <b>16:45</b> 22 101 23			201
<b>05:00</b> 2 2 4 <b>17:00</b> 29 29		58	
05:15         6         7         13         17:15         16         24           05:30         9         3         12         17:30         25         21		44	
05:30         9         3         12         17:30         25         27           05:45         14         31         10         22         24         53         17:45         38         108         24		52 66 2	220
<b>6:00</b> 9 11 20 <b>18:00</b> 16 22		36	220
<b>06:15</b> 14 16 30 <b>18:15</b> 25 33		56	
<b>06:30</b> 27 19 46 <b>18:30</b> 24 24		48	
<b>06:45</b> 22 72 18 64 40 136 <b>18:45</b> 22 87 13		34 1	174
<b>07:00</b> 36 51 87 <b>19:00</b> 24 16		40	
<b>07:15</b> 53 47 100 <b>19:15</b> 10 17		27	
<b>07:30</b> 20 35 55 <b>19:30</b> 18 17		35	105
07:45         39         148         21         154         60         302         19:45         11         63         12           08:00         15         6         21         20:00         16         10		23 1 26	125
<b>08:15</b> 26 10 36 <b>20:15</b> 21 6		20	
<b>08:30</b> 22 13 35 <b>20:30</b> 8 10		18	
<b>08:45</b> 15 78 16 45 31 123 <b>20:45</b> 12 57 7			90
<b>09:00</b> 15 11 26 <b>21:00</b> 8 8		16	
<b>09:15</b> 19 13 32 <b>21:15</b> 7 9		16	
<b>09:30</b> 26 9 35 <b>21:30</b> 4 6		10	
09:45         34         94         16         49         50         143         21:45         3         22         3           10:00         13         19         32         22:00         8         1	26		48
10:00         13         19         32         22:00         8         1           10:15         11         17         28         22:15         5         4		9 9	
<b>10:10</b> 11 17 28 22.15 5 4 <b>10:30</b> 15 16 31 <b>22:30</b> 5 3		8	
<b>10:30</b> 19 58 13 65 32 123 <b>22:45</b> 2 20 3	11		31
<b>11:00</b> 19 14 33 <b>23:00</b> 5 1		6	
<b>11:15</b> 16 14 30 <b>23:15</b> 4 2		6	
<b>11:30</b> 10 22 32 <b>23:30</b> 0 3		3	
<b>11:45</b> 22 67 18 68 40 135 <b>23:45</b> 0 9 1	7	1 1	16
TOTALS         577         486         1063         TOTALS         848	837	16	1685
SPLIT %         54.3%         45.7%         38.7%         SPLIT %         50.3%	49.7%	61	51.3%
DAUX TOTALS NB SB EB WB		Total	al
DAILY TOTALS 0 0 1,425 1,323		2,748	18

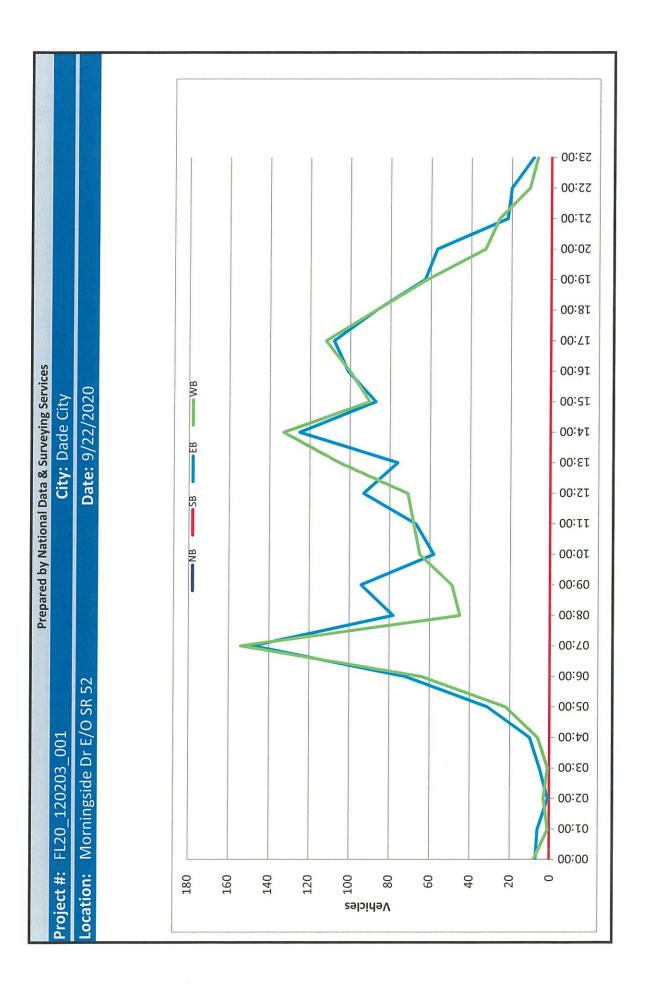
				0 (	Mins. Constant	1,425	1,323				2,748
AM Peak Hour			07:00	07:00	07:00	PM Peak Hour			14:00	13:30	13:45
AM Pk Volume			148	154	302	PM Pk Volume			125	141	261
Pk Hr Factor			0.698	0.755	0.755	Pk Hr Factor			0.710	0.653	0.666
7 - 9 Volume	0	0	226	199	425	4 - 6 Volume	0	0	209	212	421
7 - 9 Peak Hour			07:00	07:00	07:00	4 - 6 Peak Hour			16:15	16:30	16:30
7 - 9 Pk Volume			148	154	302	4 - 6 Pk Volume			111	114	221
Pk Hr Factor			0.698	0.755	0.755	Pk Hr Factor			0.694	0.983	0.801

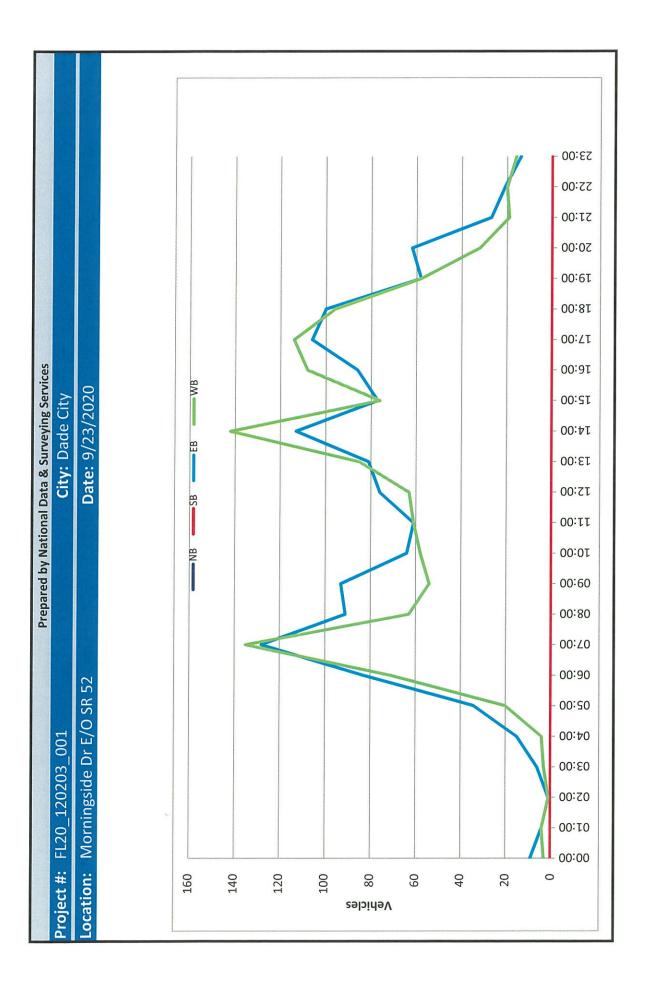
# Prepared by National Data & Surveying Services VOLUME Morningside Dr E/O SR 52

Day: Wednesday Date: 9/23/2020

				NB		SB		EB		WB	and the second sec			No.	- Store sales		Total
	DAILY TOTALS			0		0	a provent	1,410		1,306						2	2,716
AM Period	NB SB	EB		WB		Т	OTAL	PM Period	NB	S	В	EB		WB		Т	OTAL
00:00		4		2		6		12:00				19		13		32	
00:15		2		0		2		12:15				20		20		40	
00:30		2		1		3		12:30				21		14		35	
00:45		1	9	0	3	1	12	12:45				16	76	16	63	32	139
01:00		0		3		3		13:00				24		17		41	
01:15		3		0		3		13:15				23		22		45	
01:30		1		0		1		13:30				16	1000	28	03000	44	
01:45		0	4	1	4	1	8	13:45				18	81	18	85	36	166
02:00		0		0		0		14:00				23		39		62	
02:15		1		1		2		14:15				41		48		89	
02:30		0	4	0	4	0		14:30				34	440	31		65	
02:45		0	1	0	1	0	2	14:45 15:00				15	113	24	142	39	255
03:15		0		0		2		15:15				21 17		21		42	
03:30		1		1		2		15:30				21		16 22		33	
03:45		4	6	1	3	5	9	15:45				18	77	17	76	43 35	150
04:00		2	0	0	5	2	9	16:00				18	11	28	76	46	153
04:15		4		1		5		16:15				19		25		40	
04:30		3		2		5		16:30				26		30		56	
04:45		6	15	1	4	7	19	16:45				23	86	25	108	48	194
05:00		2	15	3	4	5	15	17:00				38	00	19	100	57	194
05:15		5		3		8		17:15				19		29		48	
05:30		9		4		13		17:30				27		36		63	
05:45		18	34	10	20	28	54	17:45				22	106	30	114	52	220
06:00		10		15		25		18:00				26	100	25		51	
06:15		22		15		37		18:15				28		26		54	
06:30		28		22		50		18:30				27		27		54	
06:45		23	83	19	71	42	154	18:45				19	100	18	96	37	196
07:00		30		38		68		19:00				11		14		25	
07:15		42		57		99		19:15				13		13		26	
07:30		28		25		53		19:30				20		15		35	
07:45		28	128	15	135	43	263	19:45				14	58	16	58	30	116
08:00		19		18		37	New Ser	20:00				22		8		30	
08:15		29		11		40		20:15				21		6		27	
08:30		23		18		41		20:30				11		7		18	
08:45		20	91	16	63	36	154	20:45				8	62	11	32	19	94
09:00		18		11		29		21:00				8		7		15	
09:15		12		10		22		21:15				10		6		16	
09:30		35		17		52		21:30				3		2		5	EN SEGY
09:45		28	93	16	54	44	147	21:45				6	27	4	19	10	46
10:00		19		12		31		22:00				4		3		7	
10:15		20		16		36	And And	22:15				9		8		17	
10:30		13	CA.	16 14	F 0	29	122	22:30 22:45				3	24	5	20	8	
10:45 11:00		<u>12</u> 17	64	14	58	26 31	122	22:45				5	21	4	20	9	41
11:00		17		24		31	1122	23:00				2		2 5		9	
11:15		13		13		27		23:15				2		5		7	
11:30		14	61	13	61	27	122	23:30				2	14	4 5	16	6 8	30
TOTALS		1/	589	10	477	21	1066	TOTALS		- AVELS		3	821	5	829	0	1650
SPLIT %			55.3%		44.7%		39.2%	SPLIT %					49.8%	14-14-14 14-14-14	50.2%		60.8%
JFLIT /0			55.570		-1-1.7 70		33.2/0						45.0%		30.276		
	DAILY TOTALS			NB		SB		EB		WB							otal
		C E O IF SE		0		0		1,410		1,306			14.42.50			2,	,716

				U	U	1,410	1,306			an a	2,710
AM Peak Hour			07:00	06:45	07:00	PM Peak Hour		The set	13:45	14:00	14:00
AM Pk Volume			128	139	263	PM Pk Volume			116	142	255
Pk Hr Factor			0.762	0.610	0.664	Pk Hr Factor			0.707	0.740	0.716
7 - 9 Volume	0	0	219	198	417	4 - 6 Volume	0	0	192	222	414
7 - 9 Peak Hour			07:00	07:00	07:00	4 - 6 Peak Hour			16:45	17:00	17:00
7 - 9 Pk Volume			128	135	263	4 - 6 Pk Volume			107	114	220
Pk Hr Factor			0.762	0.592	0.664	Pk Hr Factor			0.704	0.792	0.873





# Prepared by National Data & Surveying Services **VOLUME** Morningside Dr E/O US 301

Day: Tuesday Date: 9/22/2020

							100.000									Colored Arrest		
	DAILY	TOTALS			NB		SB		EB		WB							otal
			9.62		0		0		1,296	1918-18	1,641	materia					2,	,937
AM Period	NB	SB	EB		WB		T	OTAL	PM Period	NB	States and	SB	EB		WB		то	DTAL
00:00			2		1		3		12:00				28		35		63	
00:15			2		1		3		12:15				35		45		80	
00:30			0		3		3		12:30				30		27		57	
00:45			1	5	1	6	2	11	12:45				25	118	43	150	68	268
01:00			1		2		3		13:00				23		39		62	
01:15			2		0		2		13:15				31		38		69	
01:30			1 2	c	0	c	1	12	13:30 13:45				24 29	107	32 32	1.41	56	240
01:45			0	6	2	6	6	12	14:00				30	107	32	141	61 64	248
02:00			0		0		0		14:15				24		29		53	
02:30			0		0		0		14:30				24		29		57	
02:45			0		0	2	0	2	14:45				22	104	37	129	59	233
03:00			0		0	2	0	4	15:00				22	104	30	125	52	235
03:15			1		õ		1		15:15				26		29		55	
03:30			ō		1		1		15:30				31		27		58	
03:45			1	2	Ō	1	1	3	15:45				30	109	37	123	67	232
04:00			1		0		1		16:00				23		29		52	
04:15			0		0		0		16:15				4 26		39		65	
04:30			0		0		0	- States	16:30				¥ 28		36		64	
04:45			3	4	2	2	5	6	16:45				7 27	104	37	141	64	245
05:00			1		0		1		17:00				$\neq$ 34		36		70	A PERSON
05:15			1		3		4	CALL STATE	17:15				29		31		60	
05:30			4		5		9		17:30				28		32		60	
05:45			4	10	4	12	8	22	17:45				31	122	26	125	57	247
06:00			2		6		8		18:00				24		31		55	
06:15			4		6		10	T. M. BR	18:15				26		19	3	45	
06:30			3		4		7		18:30				20		27		47	
06:45			5	14	12	28	17	42	18:45				22	92	23	100	45	192
07:00			5		8		13	SUSA I	19:00				13		32		45	
07:15			10		17		27	a fuera da	19:15				12		18		30	
07:30			- 7	24	6	10	13	00	19:30				20	60	27	0.5	47	100
07:45			- 12	34	15	46	27	80	19:45 20:00				23	68	18	95	41	163
08:00			- 8		12		20		20:00				10		22		32	
08:15 08:30			- 10 17		15 21		25 38		20:15				19 13		15 20		34 33	
08:30			16	51	18	66	34	117	20:45				7	49	13	70	20	119
09:00			18	51	14	00	32	11/	21:00				8	49	12	10	20	119
09:15			13		23		36	1	21:15				9		9		18	
09:30			13		22		35		21:30				7		12		19	
09:45			14	58	31	90	45	148	21:45				1	25	5	38	6	63
10:00			19		35		54	110	22:00				1		6		7	00
10:15			22		26		48		22:15				3		6		9	
10:30			22		27		49		22:30				3		3		6	
10:45			21	84	27	115	48	199	22:45				0	7	4	19	4	26
11:00			25		32		57	Neter States	23:00				5		3		8	1
11:15			34		24	1	58		23:15				2		0		2	
11:30			34		39		73	STATE I	23:30				3		1		4	
11:45			19	112	35	130	54	242	23:45				1	11	2	6	3	17
TOTALS				380		504		884	TOTALS					916		1137		2053
SPLIT %				43.0%		57.0%		30.1%	SPLIT %					44.6%		55.4%		69.9%

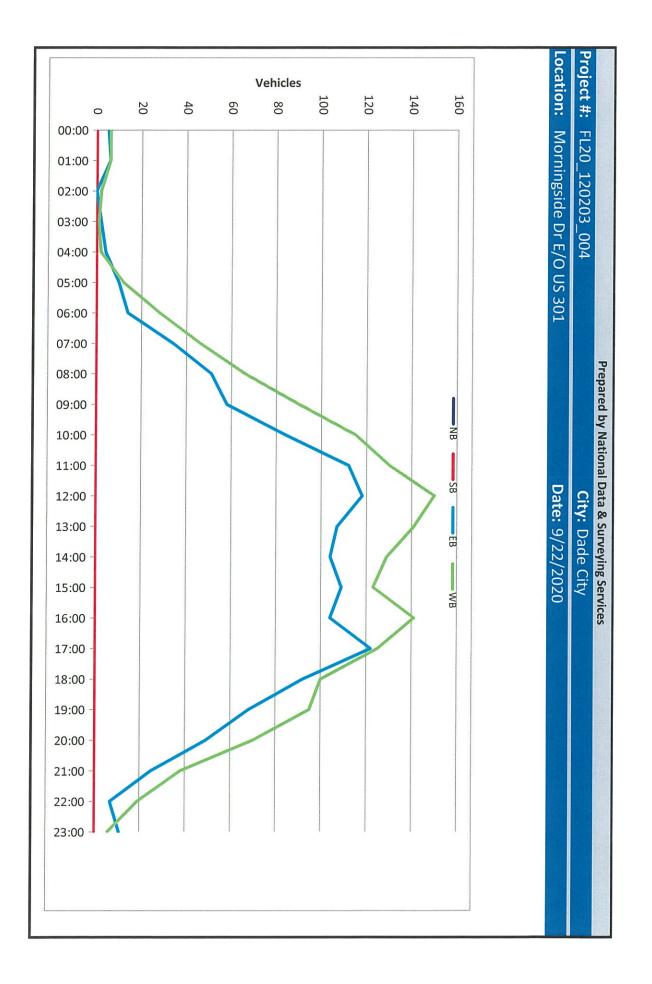
	DAILY TO	TAIS		NB	SB	EB	WB	South Board			Total
	DAILTTO	TALS		0	0	1,296	1,641	1930			2,937
AM Peak Hour			11:30	11:30	11:30	PM Peak Hour			17:00	12:15	12:00
AM Pk Volume			116	154	270	PM Pk Volume			122	154	268
Pk Hr Factor			0.829	0.856	0.844	Pk Hr Factor			0.897	0.856	0.838
7 - 9 Volume	0	0	85	112	197	4 - 6 Volume	0	0	226	266	492
7 - 9 Peak Hour			08:00	08:00	08:00	4 - 6 Peak Hour			17:00	16:15	16:15
7 - 9 Pk Volume			51	66	117	4 - 6 Pk Volume			122	148	263
Pk Hr Factor	0.000	0.000	0.750	0.786	0.770	Pk Hr Factor	0.000	0.000	0.897	0.949	0.939

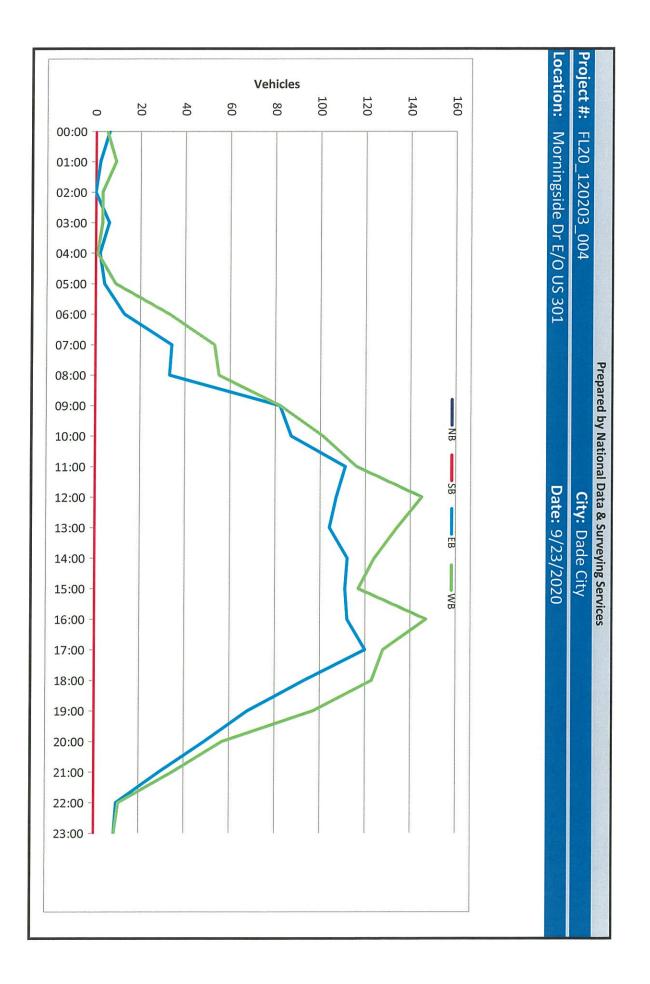
Prepared by National Data & Surveying Services VOLUME Morningside Dr E/O US 301

Day: Wednesday Date: 9/23/2020

The second	DAILY TOTALS			NB		SB		EB	WB		Store St				Т	otal
	DAILT TOTALS			0		0	203 38	1,304	1,597	7			alle a		2,	,901
AM Period	NB SB	EB		WB	aller of	T	OTAL	PM Period	NB	SB	EB		WB		тс	DTAL
00:00		0		1		1		12:00			35		36		71	
00:15		3		2		5		12:15			19		33		52	
00:30		2	8.80	1		3		12:30			24		39		63	
00:45		1	6	1	5	2	11	12:45			29	107	37	145	66	252
01:00		0		3		3		13:00			31		35		66	
01:15		1		3		4		13:15			29		37		66	
01:30		0		2		2		13:30			21		28		49	
01:45		1	2	1	9	2	11	13:45			23	104	34	134	57	238
02:00 02:15		0		2		2		14:00 14:15			22		31		53	
A CONTRACTOR OF A CONTRACTOR O		0		0		0		14:15			28		35		63	
02:30 02:45		0		1	2	0	2	14:30			26	110	31	124	57	220
02:45		1		1	3	1 2	3	15:00			<u>36</u> 22	112	27	124	63 48	236
03:15		0		0		0		15:15			31		30		61	
03:30		0		1		1		15:30			39		35		74	
03:45		5	6	1	3	6	9	15:45			19	111	26	117	45	228
04:00		0	0	0	5	0		16:00			18	111	40	11/	58	220
04:15		0		1		1		16:15			34		38		72	
04:30		0		ō		Ō		16:30			32		28		60	
04:45		2	2	0	1	2	3	16:45			28	112	41	147	69	259
05:00		0	-	0	-	0		17:00			30	114	32	147	62	233
05:15		1		2		3		17:15			32		35		67	
05:30		2		2		4		17:30			22		24		46	
05:45		1	4	5	9	6	13	17:45			36	120	37	128	73	248
06:00		5		3		8		18:00			24		37		61	
06:15		1		5		6		18:15			25		37		62	REAL STREET
06:30		2		5		7		18:30			27		25	6	52	11221
06:45		5	13	20	33	25	46	18:45			17	93	24	123	41	216
07:00		4		12		16		19:00			21		29		50	Ser and
07:15		7 13		18		31	Standard State	19:15			16		21		37	11223
07:30		9		8		17		19:30			19		27		46	
07:45		8	34	15	53	23	87	19:45			12	68	20	97	32	165
08:00		9		8		17		20:00			15		13		28	STATISTICS.
08:15		8		17		25		20:15			11		15		26	1112375
08:30		10		12		22	1.1.1	20:30			11		13		24	Nº AN
08:45		6	33	18	55	24	88	20:45			12	49	16	57	28	106
09:00		16		17		33		21:00			11		10		21	and the second
09:15		19		19		38	S CASE	21:15			8		6		14	09933
09:30		20	00	20	00	40	104	21:30			6	20	12	25	18	
09:45		27	82	26	82	53 44	164	21:45 22:00			4	29	7	35	11	64
10:00 10:15		15 15		29 27		44		22:00			1 3		4 5		5 8	
10:15		25		16		42		22:15			3		2		8 5	Charles a
10:30		32	87	29	101	61	188	22:45			3	10	0	11	3	21
11:00		30	07	29	101	51	100	23:00			2	10	4	11	6	- 21
11:15		30		30	1	60		23:15			1		4		5	1999
11:30		24		35		59		23:30			2		1		3	2.53
11:45		27	111	30	116	57	227	23:45			4	9	Ō	9	4	18
TOTALS			380		470		850	TOTALS				924		1127		2051
SPLIT %			44.7%		55.3%		29.3%	SPLIT %				45.1%		54.9%		70.7%
																-

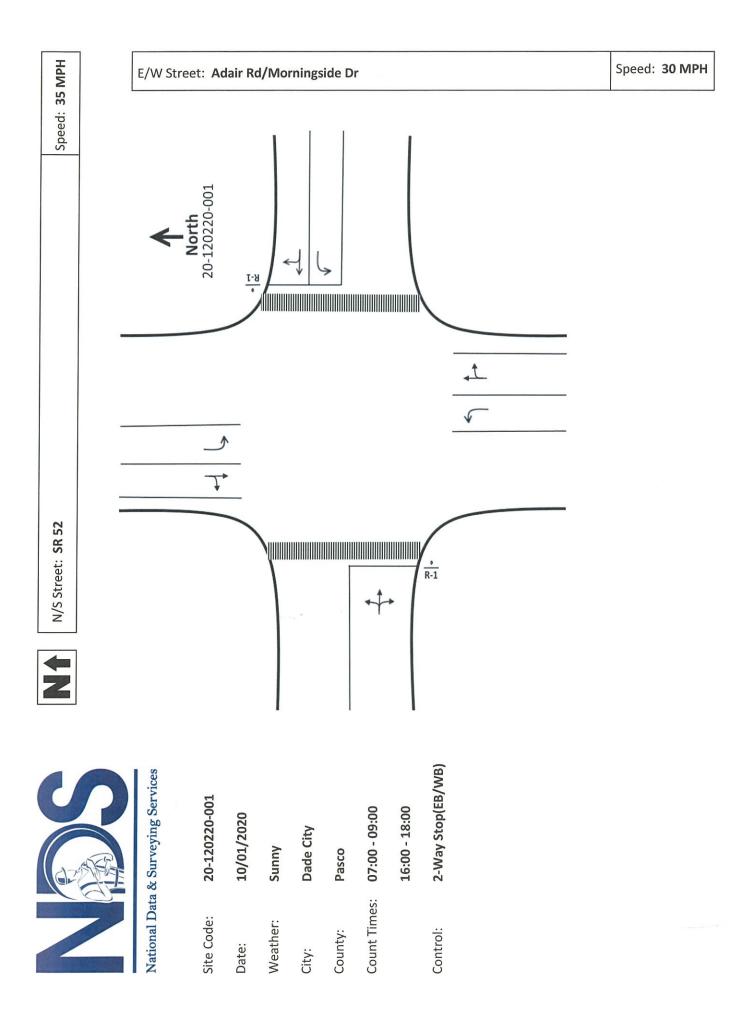
	DAILY TO	TAIS		NB	SB	EB	WB				Total
	DAILTTO	TALS		0	0	1,304	1,597	Brith and State	Ma Balliona		2,901
AM Peak Hour			10:30	11:45	11:15	PM Peak Hour			14:45	12:30	16:15
AM Pk Volume			117	138	247	PM Pk Volume			128	148	263
Pk Hr Factor			0.914	0.885	0.870	Pk Hr Factor		S. S	0.821	0.949	0.913
7 - 9 Volume	0	0	67	108	175	4 - 6 Volume	0	0	232	275	507
7 - 9 Peak Hour			07:15	08:00	07:15	4 - 6 Peak Hour			16:15	16:00	16:15
7 - 9 Pk Volume			39	55	88	4 - 6 Pk Volume			124	147	263
Pk Hr Factor		0.000	0.750	0.764	0.710	Pk Hr Factor			0.912	0.896	0.913





INTERSECTION TRAFFIC COUNTS





# Location: SR 52 & Adair Rd/Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-001 Date: 10/1/2020

L								Total	la					חמובי	המובי זען געבט		
NS/EW Streets:		SR 52	52			SR 52	22		Ac	Adair Rd/Morningside Dr	ningside Dr		Ad	air Rd/Mon	Adair Rd/Morningside Dr		
		NORTH	NORTHBOUND			SOUTHBOUND	<b>BOUND</b>			EASTBOUND	DUND			WESTBOUND	SOUND		
AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	Ш	Ш	ER	EU	ML	TW	WR	MII	TOTAL
7:00 AM	4	82	22	0	9	87	1	0	13	6	6	0	10	3	50	0	775
7:15 AM	9	73	16	0	16	115	6	0	5	8	14	0	23	5	35	0 0	377
7:30 AM	8	75	9	0	12	75	2	0	m	9	IJ	0	19		6 00	0 0	222
7:45 AM	3	81	8	0	10	76	4	0	00	6	12	0	00	, <del>.</del>	) <b>(</b>	0 0	225
8:00 AM	1	85	11	0	9	64	e	0	5	m	4	0	4	-	) m	0	190
8:15 AM	1	73	10	0	S	64	5	0	8	9	7	0	- 10			0 0	194
8:30 AM	4	75	9	0	m	54	5	0	10	m	L)	0	000	4	9 10	0 0	183
8:45 AM	4	99	4	0	S	50	2	0	9	m	m	0	, m	4	2	0	152
	NL	NT	NR	NN	SL	ST	SR	SU	E	Ш	ER	B	M	MT	WR	MI	TOTAL
TOTAL VOLUMES :	31	610	83	0	63	585	31	0	58	47	59	0	80	23	56	2 0	1763
APPROACH %'s :	4.28%	84.25%	11.46%	0.00%	9.28%	86.16%	4.57%	0.00%	35.37%	28.66%	35.98%	0.00%	40.82%	11.73%	47.45%	0.00%	
PEAK HR :		07:00 AM - 08:00 AM	- 08:00 AM	Sector States		の時間になるの		Series and		のないのないである	SALA LINE AND	Second Second	いたななのの記				TOTAL
PEAK HR VOL :	21	311	52	0	4	353	16	0	29	32	40	0	60	6	11	0	1044
<b>PEAK HR FACTOR :</b>	0.656	0.948	0.591	0.000	0.688	0.767	0.444	0.000	0.558	0.889	0.714	0.000	0.652	0.750	0.550	0.000	
		0.889	889			0.738	38			0.815	15			0.608	98		0.811
		NORTH	NORTHBOUND			SOUTHBOUND	SOUND			EASTBOUND	OUND			WESTBOUND	SOUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	Ц	Ш	ER	EU	ML	TW	WR	MII	TOTAL
																	:

		NORTHBOUND	BOUND			SOUTHBOUNE	BOUND			EASTBOUND	<b>DNUC</b>			WESTE	30UND		Γ
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	Ы	ER	E	WL	TW	WR	MU	TOTAL
4:00 PM	2	135	22	0	13	106	7	0	S	e	6	0	16	5	10	0	338
4:15 PM	2	126	17	0	7	105	9	0	9	2	11	0	25	8	11	0	331
4:30 PM	2	117	24	0	12	107	11	0	7	ы	12	0	15	6	8	0	334
4:45 PM	5	116	19	0	8	67	5	0	80	2	18	0	16	6	6	0	317
5:00 PM	11	129	26	0	16	145	12	0	4	ъ	19	0	18	8	16	0	409
5:15 PM		122	14	0	11	112	10	0	9	8	10	0	23	7	13	0	344
5:30 PM	9	133	15	0	10	06	14	0	8	7	10	0	15	10	m	0	321
5:45 PM	11	132	19	0	16	06	12	0	4	10	11	0	22	2	7	0	336
	NL	NT	NR	NN	SL	ST	SR	SU	Ц		R	B	ML	TW	WR	NM	TOTAL
TOTAL VOLUMES :	62	1010	156	0	93	852	77	0	48		100	0	150	58	17	C	730
APPROACH %'s :	5.05%	82.25%	12.70%	0.00%	9.10%	83.37%	7.53%	0.00%	24.62%	24.10%	51.28%	0.00%	52.63%	20.35%	27.02%	0.00%	
PEAK HR :		05:00 PM - 06:00 PM	M4 00:90				N. C. S. C.	Sec. Sec.			Station 14	1.1.22	Adding	1. 1. 1. 1. 1.			TOTAL
PEAK HR VOL :	36	516	74	0	53	437	48	0	22	30	50	0	78	27	39	0	1410
PEAK HR FACTOR :	0.818	0.970	0.712	0.000	0.828	0.753	0.857	0.000	0.688	0.750	0.658	0.000	0.848	0.675	0.609	0,000	
		0.943	43			0.77	17	ALC: NO		0.911				0.8	37		0.862

National Data & Surveying Services

## Intersection Turning Movement Count

Location: SR 52 & Adair Rd/Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-001 Date: 10/1/2020

NS/EW Strends         St 23         St 23         St 23         Addir Rol/Montingside Dr.         Addir Rol/Montingside Dr.           All         0         NOTTBOUID         0         Souther         Not         Not </th <th></th>																		
N         NORTHBOLNO         SOTTHBOLNO         NORTHBOLNO         WESTBOLNO         WESTBOLNO           N <th>NS/EW Streets:</th> <th></th> <th>SR 5</th> <th>22</th> <th></th> <th></th> <th>SR</th> <th>22</th> <th></th> <th>Ac</th> <th>dair Rd/Mor</th> <th>ningside Dr</th> <th></th> <th>A</th> <th>dair Rd/Mo</th> <th>orningside D</th> <th></th> <th></th>	NS/EW Streets:		SR 5	22			SR	22		Ac	dair Rd/Mor	ningside Dr		A	dair Rd/Mo	orningside D		
N         N			NORTH	BOUND			SOUTH	BOUND		3	EASTB	dNNO			WEST	BOUND		
4         78         19         0         6         97         1         9         0         10         11         5         0         11         5         0         11         5         0         11         5         0         12         13         8         0         11         0         11         6         7         1         6         7         0         3         5         1         0         13         3         3         0         1         1         0         11         1         11         12         0         13         3	AIVI	D N	0 IN	0 NR	0 NIN		<mark>کا 0</mark>	<mark>0</mark> 85	0	<mark>0</mark> II	0	0	0	0	0	0	0	TOT
6         69         16         11         8         14         0         20         23         5         3         4         0         1         7         0         1         7         0         1         7         0         1         7         0         1         7         0         1         1         64         1         0         4         1         1         1         7         0         1         1         7         0         1         1         7         0         1         1         7         0         1         1         7         0         1         1         7         0         1         1         7         0         1<	7:00 AM		78	19	0		87	1	30	13	6	50	20	10	M (C)	29 29	0	268
8         74         5         0         12         71         2         0         3         5         5         0         18         3         7         0         1         0         11         0         1         0         11         0         4         1         1         0         1         0         4         1         1         0         3         5         4         5         0         3         5         4         1         0         4         1         1         0         4         1         1         0         3         5         5         0         3         5         5         0         3         5         5         0         3         5         5         0         3         5         5         0         3         5         0         3         5         0         3         5         0         3         5         0         3         5         0         3         5         0         3         5         0         3         5         1         1         0         0         0         0         0         0         0         0         0         0 </td <td>7:15 AM</td> <td></td> <td>69</td> <td>16</td> <td>0</td> <td></td> <td>113</td> <td>8</td> <td>0</td> <td>S</td> <td>8</td> <td>14</td> <td>0</td> <td>20</td> <td>2</td> <td>35</td> <td>0 0</td> <td>312</td>	7:15 AM		69	16	0		113	8	0	S	8	14	0	20	2	35	0 0	312
3         81         8         0         9         72         4         0         8         9         12         0         4         1         5         0           1         64         7         0         4         61         3         5         0         3         4         1         1         5         0         4         1         1         1         1         1         1         1         1         1         1         1         1         0         3         4         1         1         0         3         4         1         1         0         1 <td>7:30 AM</td> <td>8</td> <td>74</td> <td>S</td> <td>0</td> <td></td> <td>71</td> <td>2</td> <td>0</td> <td>3</td> <td>S</td> <td>5</td> <td>0</td> <td>18</td> <td>m</td> <td>2</td> <td>0</td> <td>213</td>	7:30 AM	8	74	S	0		71	2	0	3	S	5	0	18	m	2	0	213
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	7:45 AM	m	81	œ	0		72	4	0	8	6	12	0	80	1	2	0	220
1         64         7         0         3         5         0         3         5         4         0           4         64         3         0         4         65         5         0         8         6         7         0         3         5         4         1         0           1         NT         NT         NU         SL         553         SS         0         3         5         4         1         0         0           31         SN         NN         NT         NU         SL         SS         SS         SS         0         3         3         1         0         0           1         SN         NN         NN         SS         SS <td>8:00 AM</td> <td></td> <td>80</td> <td>11</td> <td>0</td> <td></td> <td>62</td> <td>ю</td> <td>0</td> <td>2</td> <td>3</td> <td>4</td> <td>0</td> <td>4</td> <td></td> <td></td> <td>0</td> <td>181</td>	8:00 AM		80	11	0		62	ю	0	2	3	4	0	4			0	181
4         68         6         0         3         51         5         0         10         3         4         1         7         4         5         0         3         51         5         0         1         4         5         0         3         4         1         1         0           NL         NT         NR         NU         55         55         56         57%         67.9%         0.00%         35.8%         35.5%         35.5%         37.2%         37         23         87         0         0           21         302         48         0         0.558         0.661         0.558         0.661         0.700         35.5%         47         1         0           21         302         48         15         0         0.558         0.661         0.700         35.49%         12.57%         47.54%         0.00%           21         302         48         1         0         0         0         0.558         0.661         0.700         0.796         0.79%         0.00%         0.00%         0.756         0.759%         0.00%         0.00%         0.756         0.00%         0.00%	8:15 AM		64	2	0		60	2	0	8	9	7	0	m	5	4	0	174
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8:30 AM		68	9	0		51	S	0	10	e	S	0	7	4	5	0	171
NIL         State         State <t< td=""><td>8:45 AM</td><td>4</td><td>64</td><td>m</td><td>0</td><td></td><td>43</td><td>2</td><td>0</td><td>9</td><td>e</td><td>e</td><td>0</td><td>e</td><td>4</td><td>1</td><td>0</td><td>140</td></t<>	8:45 AM	4	64	m	0		43	2	0	9	e	e	0	e	4	1	0	140
313         573         0         60         559         30         0         538         46         53         70         7		N	NT	NR	NN	SL	ST	SR	SU	Ш	E	H	EU	M	ΜT	WR	MIT	
4.53%         8.50%         0.00%         9.24%         86.13%         4.62%         0.00%         35.58%         28.22%         36.20%         0.00%         39.99%         12.57%         47.54%         0.00%           21         302         0.650         0.00%         39.39%         12.57%         47.54%         0.00%           21         302         0.653         0.00%         39.39%         12.57%         47.54%         0.00%           21         302         0.632         0.00%         39.39%         12.57%         47.54%         0.00%           0.518         0.322         0.632         0.632         0.630         0.70%         39.9%         12.57%         47.54%         0.00%           0.918         0.322         0.632         0.630         0.675         0.54%         0.00%         39.9%         12.57%         47.54%         0.00%           0         0         0         0         0         0         0         0         0.618         0.00%         59.9%         12.54%         100         0         56.6%         0.00%         59.9%         12.54%         0         0         0         0         0         0         0         0	TOTAL VOLUMES :	31	578	75	0	60	559	30	0	58	46	29	0	73	23	87	0	1679
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	APPROACH %'s :		84.50%	10.96%	0.00%	9.24%	86.13%	4.62%	0.00%	35.58%	28.22%	36.20%	0.00%	39.89%	12.57%		0.00%	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	PEAK HR :		- MA 00:70	08:00 AM								A COLEMAN						1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	PEAK HR VOL :		302	48	0	43	343	15	0	29	31	40	0	56	6	76	0	1013
NORTHBOUND         SOUTHBOUND         EASTBOUND         EASTBOUND           0         NL         NR         NO         SOUTHBOUND         WESTBOUND           7         112         NR         NO         SOUTHBOUND         MESTBOUND         WESTBOUND           7         112         10         7         SOUTHBOUND         SOUTHBOUND         WESTBOUND           7         112         12         0         13         100         7         0         5         3         9         0         15         W <td>PEAK HR FACTOR :</td> <td></td> <td>0.932 0.91</td> <td>0.632</td> <td>0.000</td> <td>0.672</td> <td>0.759 0.73</td> <td>0.469 32</td> <td>0.000</td> <td>0.558</td> <td>0.861 0.80</td> <td>0.714</td> <td>0.000</td> <td>0.700</td> <td>0.750</td> <td>0.543 518</td> <td>0.000</td> <td>0.812</td>	PEAK HR FACTOR :		0.932 0.91	0.632	0.000	0.672	0.759 0.73	0.469 32	0.000	0.558	0.861 0.80	0.714	0.000	0.700	0.750	0.543 518	0.000	0.812
0         0			NORTHE	SOUND			SOUTH	SOLIND			FASTR	ON IO			WEST	CINI OR		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	PM	C	C	C	C		0		c	C			c	C			c	
	-	NL	LN	NR	NN		2	2			> L			MI	D TW	N/D	0	TOTAL
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4:00 PM	9	132	20	0		100	7	0	5	m	6	20	:	ſ	10		375
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4:15 PM		122	16	0		103	9	0	9	2	00	0	24	000	10	0 0	317
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4:30 PM		112	18	0		105	11	0	7	S	12	0	15	6	00	0	318
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4:45 PM		115	17	0		95	5	0	8	7	18	0	16	6	6	0	312
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5:00 PM		125	21	0		144	12	0	4	S	19	0	18	8	15	0	397
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5:15 PM	_	122	14	0		112	10	0	9	8	6	0	23	7	13	0	343
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5:30 PM		131	15	0		89	14	0	8	9	10	0	15	10	m	0	316
NL         NT         NR         NU         St         ST         SR         SU         EL         ET         ER         EU         WL         WT         WR         WU         NU         NU         NU         NL         MT         WR         WU         NU         NU         St         St<	5:45 PM		132	19	0		06	12	0	4	10	10	0	22	2	9	0	333
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		NL	NT	NR	NN	SL	ST	SR	SU	EL	Ш	ß	EU	ML		WR	MU	TOTAL
05:00 PM - 06:00 PM         51         435         48         0         22         29         48         0         78         27         37         0           35         510         69         0         51         435         48         0         22         29         48         0         78         27         37         0           0.80         0.966         0.821         0.000         0.555         0.617         0.000         0.648         0.617         0.000	APPROACH %'s :		991 83.21%	140 11.75%	0.00%	86 8.59%	838 83.72%	77 7.69%	0.00%	48 25.40%	46 24 34%	95 50 26%	0 00%	148 57 86%			0 000	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	PEAK HR :	The Allinear		MG 00:90	Source	No. 1 No. 1	- Alexandre	Part Part	South States		der and and			200000			0.00.0	
0.80 0.966 0.821 0.000 0.797 0.755 0.857 0.000 0.688 0.725 0.632 0.000 0.848 0.675 0.617 0.000	PEAK HR VOL :	200	510	69	0	51	435	48	0	22	29	48	0	78	27	37	0	1389
	PEAK HR FACTOR :		0.966	0.821	0.000	0.797	0.755	0.857	0.000	0.688	0.725	0.632	0.000	0.848	0.675	0.617	0.000	0.875

# Location: SR 52 & Adair Rd/Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-001 Date: 10/1/2020

								HT	F					nate: 1	Date: 10/1/2020		
NS/EW Streets:		SR 52	52			SR 52	22		Ac	Adair Rd/Morningside Dr	ningside Dr		Ac	air Rd/Mori	Adair Rd/Morningside Dr		
		NORTH	NORTHBOUND			SOUTHBOUND	GUND			EASTBOUND	DUND			WESTBOUND	GUND		
AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	Ы	ER	EU	M	TW	WR	MII	TOTAL
7:00 AM	0	4	e	0	0	0	0	0	0	0	0	0	0	0	0	0	1
7:15 AM	0	4	0	0	0	2	1	0	0	0	0	0		0 0			10
7:30 AM	0	1	1	0	0	4	0	0	0	-	0	0		0 0	, <del>-</del>		ç o
7:45 AM	0	0	0	0	1	4	0	0	0	0	0	0	10	0	4 0		י ר <u>ר</u>
8:00 AM		5	0	0	0	2	0	0	0	0	0	0	0	0	0	0	σ
8:15 AM		6	e	0	1	4	0	0	0	0	0	0	~	0	I	0 0	00
8:30 AM		7	0	0	0	m	0	0	0	0	0	0	-	0	· -	0 0	1
8:45 AM	0	2	1	0	1	7	0	0	0	0	0	0	0	0		0	12
	IN	ΔT	NR	IIN	0	۲ ا	9	U		Ŀ	E	-	11/1	WT	UM.	AA11	TOTAL
TOTAL VOLUMES	2	55	0	2	; r	90	ś.	3 0	; <		5 0	2 0		1 ^ ~	NN	n v	INIAL
APPROACH %'s :	0.00%	80.00%	2(	0.00%	10.00%	86.67%	1 3.33%	0.00%	0.00%	100.00%	0.00%	0.00%	73 85%	0 00%	6 46 15%	0 00%	84
PEAK HR :		07:00 AM - 08:00 AM	MK 00:80	見たいでのない	No. of the other		and a second sec	10000000	A COM THE							2000	TOTAI
PEAK HR VOL :	0	6	4	0	1	10	1	0	0	1	0	0	4	0	5 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0	31
PEAK HR FACTOR :	0.000	0.563	0.333	0.000	0.250	0.625	0.250	0.000	0.000	0.250	0.000	0.000	0.333	0.000	0.250	0.000	144 0
		0.464	64	Sector Sector		0.600	0		E QUE TANK	0.250	0	100 M 100 M		0.417	17		c//.0
		NORTH	NORTHBOUND			SOUTHBOUND	BOUND			EASTBOUND	DUND			WESTBOUND	BOUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	TN	NR	NU	SL	ST	SR	SU	E	Ы	R	B	ML	ΤW	WR	MU	TOTAL
4:00 PM	1	m	2	0	0	9	0	0	0	0	0	0	1	0	0	0	13
4:15 PM	0	4	1	0	2	2	0	0	0	0	c	0	+	C	-	C	14

		NORTHBOUND	BOUND			SOUTHBOUN	BOUND			EASTBOUN	OUND			WESTBOUND	BOUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	Ц	Ш	ER	EU	WL	M	WR	MU	TOTAL
4:00 PM	1	m	2	0	0	9	0	0	0	0	0	0	1	0	0	0	13
4:15 PM	0	4	1	0	2	2	0	0	0	0	б	0	1	0	1	0	14
4:30 PM	0	S	9	0	m	2	0	0	0	0	0	0	0	0	0	0	16
4:45 PM	0	1	2	0	0	2	0	0	0	0	0	0	0	0	0	0	ъ
5:00 PM	0	4	2 2	0	1	1	0	0	0	0	0	0	0	0	1	0	12
5:15 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	-
5:30 PM	0	2	0	0	1	1	0	0	0	1	0	0	0	0	0	0	i LO
5:45 PM	1	0	0	0	0	0	0	0	0	0	1	0	0	0	1	0	ŝ
																	•
	NL	NT	NR	NU	SL	ST	SR	SU	E	Ш	щ	EU	ML	MT	WR	MM	TOTAL
TOTAL VOLUMES :	2	19	16	0	7	14	0	0	0	Ч	Ŋ	0	2	0	с	0	69
APPROACH %'s :	5.41%	51.35%	43.24%	0.00%	33.33%	66.67%	0.00%	0.00%	0.00%	16.67%	83.33%	0.00%	40.00%	0.00%	60.00%	0.00%	;
PEAK HR :		05:00 PM - 06:00 PM	MG 00:90	- TENE							いたのの	11 1 1 1	A CANADA U	10 - 10 - 10	Sec. 10. 192	1	TOTAL
PEAK HR VOL :	1	9	5	0	2	2	0	0	0	1	2	0	0	0	2	0	21
PEAK HR FACTOR :	0.25	0.375	0.250	0.000	0.500	0.500	0.000	0.000	0.000	0.250	0.500	0.000	0.000	0.000	0.500	0.000	
		0.333	33			0.500	00			0.75	20			0.50	00		0.438

# Location: SR 52 & Adair Rd/Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-001 Date: 10/1/2020

								Bik	Bikes					Date:	<b>Jate:</b> 10/1/2020		
NS/EW Streets:		SR 52	52			SR 52	52			Adair Rd/Morningside Dr	irningside D		A	dair Rd/Mo	Adair Rd/Morningside Dr	c.	
		NORTH	NORTHBOUND			SOUTH	SOUTHBOUND			EASTI	EASTBOUND			WEST	BOUND		
AM	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	
	NL	N	NK	NU	SL	ST	SR	SU	ᆸ	Ц	ER	EU	1	WT	WR	MU	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	C
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0		0			
7:30 AM	0	0	0	0	0	0	0	0	0	0							
7:45 AM	0	0	0	0	0	0	0	0	0	0	0 0						
8:00 AM	0	0	0	0	0	0	0	0	0	C	0	0		0		0 0	
8:15 AM	0	0	0	0	0	0	0	0	0	C							
8:30 AM	0	0	0	0	0	0	0	0	C	0 0							
8:45 AM	0	0	0	0	0	0	0	0	00	00	00	0	00	00	00	00	00
	NL	NT	NR	NU	SL	ST	SR	SU	Ш	Ш	ER	EU		TW	WR	MII	TOTAI
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR :		- MA 00:70	07:00 AM - 08:00 AM	all and a set				ALC: NOT	a state of the	語語があるというという	A State of the sta	Contract and	R.C. S. Category		- The second second	からいないない	TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0	0	0	0	0	0	c	c	
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	<b>b</b>
2		NORTH	NORTHBOUND		2	SOUTH	BOUND			EAST	EASTBOUND			WEST	BOUND		L
N N	N 0	0 L	NR NR	0 N	<mark>0</mark> 7	0 کل دہ	0 8	0	<mark>0</mark> 1	<u> </u>	<mark>0</mark> 1	0	0	0	0 0 The	0	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
4:15 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0 0	
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	. 0
4:45 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
5:00 PM	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0	0	2

		NORTHBOUND	BOUND			SOUTH	BOUND			EASTBC	<b>DUND</b>			WEST	BOUND		
Md	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	Ц	Ш	ER	EU	ML	TW	WR	MIN	TOTAI
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10
4:45 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	00	
5:00 PM	0	0	0	0	0	1	Ţ	0	0	0	0	0	0	0	0	0	1
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	I C
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
												5					
	NL	NT	NR	NU	SL	ST	SR	SU	Ш	Ш	ER	B	ML	MT	WR	MU	TOTAL
TOTAL VOLUMES :	0	1	0	0	0	2	1	0	0	0	0	0	0	0	C	c	4
APPROACH %'s :	0.00%	0.00% 100.00%	0.00%	0.00%	0.00%	66.67%	33.33%	0.00%					L.		,	)	
PEAK HR :		05:00 PM - 06:00 PM	Mq 00:90	Station of			「おおいたい」の		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1	1. 19 1. 19	1.11.12	Strain and a	State State	14 10 11 11 11 11 11 11 11 11 11 11 11 11	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TOTAL
PEAK HR VOL :	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0	0	~
PEAK HR FACTOR :	0.00	0.000	0.000	0.000	0.000	0.250	0.250	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1
						0.21	20										0.250

## Intersection Turning Movement Count

Location: SR 52 & Adair Rd/Morningside Dr City: Dade City

Project ID: 20-120220-001 Date: 10/1/2020

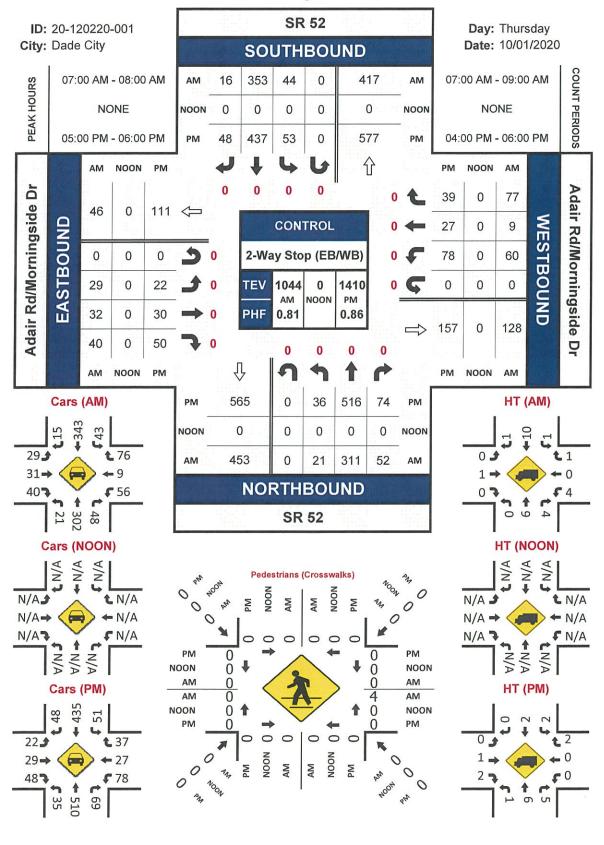
		Pedestrians	Pedestrians (Crosswalks)		
NS/EW Streets:	SR 52	SR 52	Adair Rd/Morningside Dr	Adair Rd/Morningside Dr	
AM	NORTH LEG	SOUTH LEG	EAST LEG	WEST LEG	
	EB WB	EB WB	NB SB	NB SB	TOTAI
7:00 AM	0	0 0	1 0	0	
7:15 AM	0	0	1 0	0	
7:30 AM	0	0	2 0	0	
7:45 AM	0 0	0	0	0	10
8:00 AM	0	0	0	1 0	(
8:15 AM	0	0	0	0	
8:30 AM	0 0	0	0	0	
8:45 AM	0	0	0	0	00
	EB WB	EB WB	NB SB	NB SB	TOTAL
TOTAL VOLUMES :	0	0	4 0	1 0	ц
APPROACH %'s :			100.00% 0.00%	100.00% 0.00%	)
PEAK HR :	07:00 AM - 08:00 AM				TOTAI
PEAK HR VOL :	0 0	0 0	4 0	0	4
<b>PEAK HR FACTOR :</b>			0.500		
			0.500		0.500
				AN ADDRESS ADDRESS AND ADDRESS AND ADDRESS	

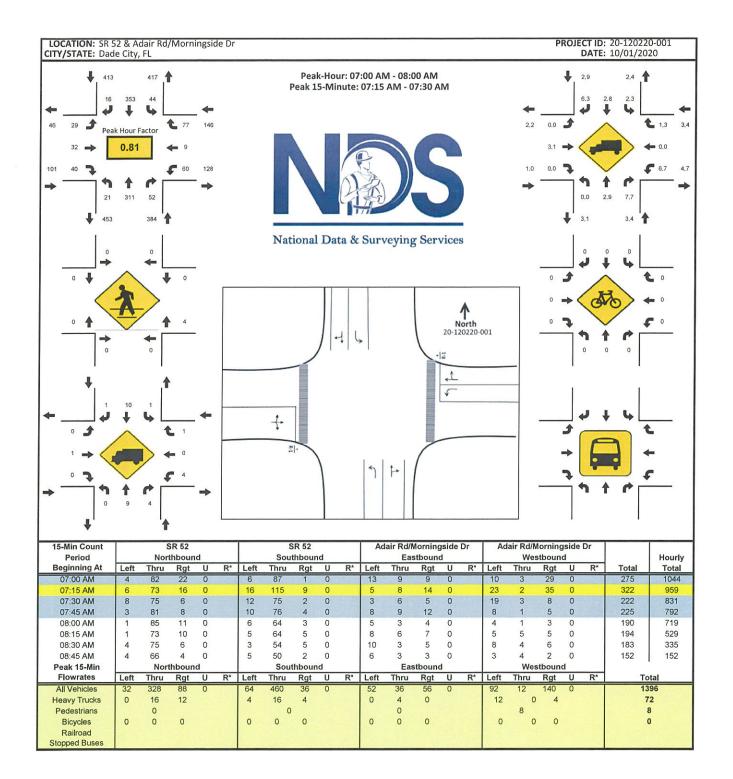
	TOTAL	0	0	0	0	0	0	0	0	 TOTAL	0		TOTAL	0	,	
WEST LEG	SB	0	0	0	0	0	0	0	0	ß	0			0		
WE	NB	0	0	0	0	0	0	0	0	NB	0			0		
EAST LEG	SB	0	0	0	0	0	0	0	0	SB	0		の設計になか	0		
EAST	NB	0	0	0	0	0	0	0	0	NB	0			0		
SOUTH LEG	WB	0	0	0	0	0	0	0	0	WB	0		No Constanting	0		
SOUT	EB	0	0	0	0	0	0	0	0	B	0			0		
H LEG	WB	0	0	0	0	0	0	0	0	WB	0		06:00 PM	0		
NORTH LEG	EB	0	0	0	0	0	0	0	0	B	0		05:00 PM - 06:00 PM	0		
PM		4:00 PM	4:15 PM	4:30 PM	4:45 PM	5:00 PM	5:15 PM	5:30 PM	5:45 PM		TOTAL VOLUMES :	APPROACH %'s :	PEAK HR :	PEAK HR VOL :	PEAK HR FACTOR :	
											TOT	AP			PEAP	

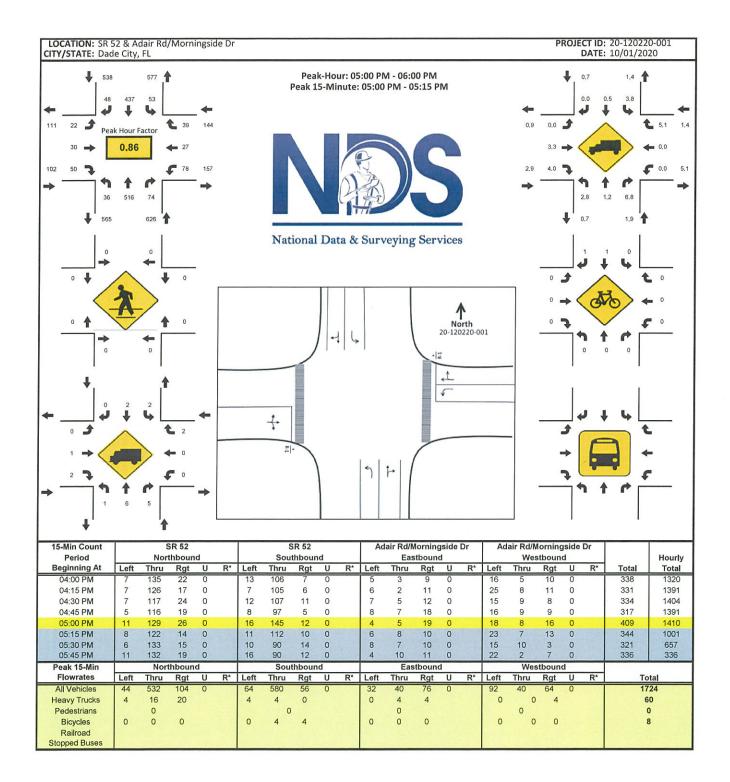
Prepared by National Data & Surveying Services

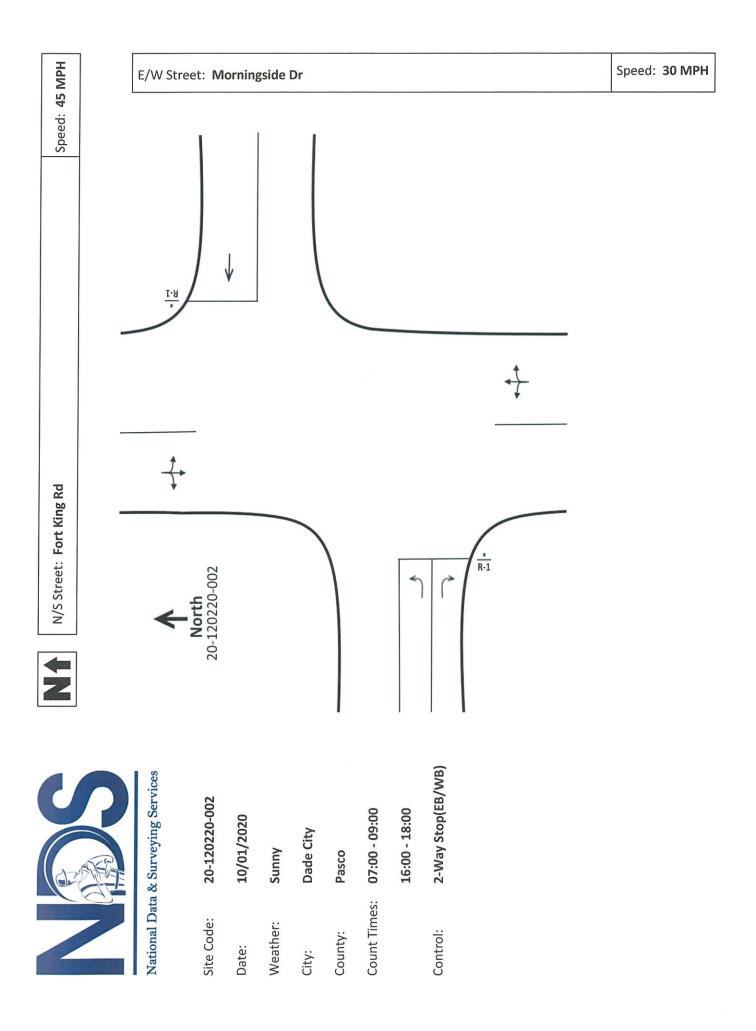
### SR 52 & Adair Rd/Morningside Dr

### Peak Hour Turning Movement Count









## Intersection Turning Movement Count

Location: Fort King Rd & Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-002 Date: 10/1/2020

NS/EW Streets:																	
		Fort King Rd	ng Rd			Fort King Rd	ng Rd			Morningside Dr	side Dr			Morningside Dr	side Dr		
		NORTH	NORTHBOUND	0		SOUTHBOUNE	BOUND			EASTBOUND	DUND			WESTBOUND	SOUND		
AIM	NL 0	0 LN	NR 0	0 NN	<mark>0</mark>	0 ST	0 8	0	<mark>0</mark> īī	<u> </u>	<mark>0</mark> 8	0	0	0	0	0	TOTAL
7:00 AM	28	52	S	0	7	33	12	30	10	4	10	2 0		1	L L		177
7:15 AM	37	73	e	0	S	67	23	0	20	- 4	3 2		o (c	4	1		51
7:30 AM	18	43	4	0	2	48	2	0	10	. 0	3 2		n (		- ~		162
7:45 AM	12	41	2	0	4	34	e co	0	4	000	11		, <del>,</del> ,	1	0 4		131
8:00 AM	5 2	43	e	0	7	46	2	0	2	2	15	00	-	- 0	- ~		100
8:15 AM	10	53	8	0	m	35	4	C	ισ	10	1 =		10		10		120
8:30 AM	13	44	e	0	4	43	- LO	0		I	0		4		4		act
8:45 AM	7	31	ю	0	e	34	ę	0	2	0	10	0	2	0	4 <del>- 1</del>	0	96
	NL	NT	NR	NU	SL	ST	SR	SU	Ш	Ы	Я	EU	ML	WT	WR	MU	TOTAL
TOTAL VOLUMES :	130	380	31	0	35	340	59	0	62	21	126	0	16	6	21	0	
APPROACH %'s :	24.03%	70.24%	5.73%	0.00%	8.06%	78.34%	13.59%	0.00%	29.67%	10.05%	60.29%	0.00%	34.78%	19.57%	45.65%	0.00%	
PEAK HK :		U/:UU AM - U8:UU AM	U8:00 AM														TOTAL
DEAK HE VOL :	547 CFA10	209	14 0.700	0000	18	182	45	0000	44	16	82	0	10	6	15	0	739
	710.0	0.704	04	0000	cto:n	0.645	15	000-0	ncc.u	0.755	0.891	0.000	0.41/	0.563 (0.500)	0.536 00	0.000	0.679
		NODTH															
DM	C	0		C	C			c	c			c	c	WESIBUUND		•	
	N	, Lu	NB		ס ס	5	0		> 1	> [			0			0	101
4:00 PM	20	33	-	0	2	48	2	2	1		22		A L		YN C	OM C	IOI AI
4:15 PM	32	31	ı <del>.</del>		0	31	ά		1 1	<b>-</b>	50		t r	+ +	7	0 0	ACT 1
4:30 PM	29	42		0		4	9 4	0 0	4		22		11	-1 (Y			140
4:45 PM	22	41	S	0	-	54	. 0	0	10	0 0	24		:		4 40		175
5:00 PM	31	49	0	0	2	67	7	0	7	0	35	0	2	4	~	0	211
5:15 PM	29	39	1	0	1	46	11	0	9	0	31	0	9	9	4	C	180
5:30 PM	21	30	e	0	1	49	e	0	9	1	23	0	0	0	. ~	0 0	141
5:45 PM	27	42	1	0	2	55	6	0	9	0	36	0	) <del> </del>	0	2	00	181
	NL	NT	NR	NN	SL	ST	SR	SU	Н	Б	ß	EU	ML	ΜT	WR	MU	TOTAL
TOTAL VOLUMES :	211	307		0	15	394	58	0	48	2	228	0	39	20	24	0	
APPKUACH % S	59./4%	- MG 02.10	0,05.20 Md 02.30	0.00%	3.21%	84.37%	12.42%	0.00%	17.27%	0.72%	82.01%	0.00%	46.99%	24.10%	28.92%	0.00%	
DEAV UD VOL -	111	171	HI DC'CD	-	U	•••	5		ŗ	c	1		-				TOTAL
PEAK HR FACTOR :	111	1/1	0.350	0000	5090	2111 0 787	31 0 705	0 000	21 0.675	0000	115	0000	27	13	14	0	732
	2000	0.903	03		770-0	0.813	50/-0	00000	C10.0	0.000	120.0	0.000	4T0'0	24C.U	20C.U	0.000	0.867

# Location: Fot King Rd & Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-002 Date: 10/1/2020

Fort King Rd           NORTHBOUND           0         0           0         NT           17         NR           17         5           14         5           12         3           13         3           13         3           13         3           13         3           13         3           13         3           13         3           13         3           13         3           13         3           13         3           13         3           14         3           14         3           14         3           14         3           15         3           16         0.500           0.690         0.00           0         0           1         1		Co	Cars							
NORTHBOUND           0         0         0           NL         NT         NR           28         47         5           37         72         3           17         43         4           12         39         2           5         41         3           12         31         3           12         41         3           12         41         3           12         41         3           12         41         3           12         41         3           24.32%         69.88%         5.79%           0.64         0.698%         5.79%           0.64         0.698%         5.79%           0.690         0.0700         0           0.690         0.690         0           0.690         0.690         0           0.690         0         0           1         1         1	For	Fort King Rd		Morningside Dr	۲.		Morningside Dr	side Dr		
0         0         0         0           NL         NT         NR         5           28         47         5         3           17         43         4         4           17         43         4         7           12         39         2         3           12         41         3         7           12         41         3         7           12         41         3         7           12         41         3         7           12         41         3         7           12         31         3         7           126         5.79%         5.79%         7           24.32%         69.88%         5.79%         0           0.64         0.698         0.700         0           0.64         0.698         0.700         0           0.690         0         0.690         0           1         1         1         1	SOI	SOUTHBOUND		EASTBOUND	0		WESTBOUND	GNID		
NL         NT         NR           28         47         5           37         72         3         3           17         43         4         4           12         39         2         3           12         39         2         3           12         41         3         7           12         41         3         7           12         41         3         7           12         41         3         7           12         41         3         7           12         41         3         7           NL         NT         NR         7           126         5.38%         5.79%         6           24.32%         69.88%         5.79%         0           0.64         0.69.8%         5.79%         0           0.64         0.69.8%         5.79%         0           0.690         0.0760         0         0           0.690         0         0         0           18         31         1         1			0		0	0	0	0	C	
28 47 5 37 72 3 17 34 4 5 41 3 8 48 7 12 41 3 7 31 3 7 31 3 7 31 3 7 24.32% 69.88% 5.79% 0.64 0.698 0.700 0 0.64 0.698 0.700 0 0.64 0.698 0.700 0 0.69 0.700 0 0.69 0.700 0 0.69 0.691 14 0.690 0 0.691 0.700 0 0.690 0 0.600 0 0 0.600 0 0 0.600 0 0 0.600 0 0 0.600 0 0 0.600 0 0 0.600 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL	SR SU	E	Ē	ER FU	MI	TW	WB	MII	TOTAL
37     72     3       17     43     4       12     39     2       5     41     3       8     48     7       12     41     3       7     31     3       12     41     3       12     41     3       NL     NT     NR       126     308%     5.79%       24.32%     69.88%     5.79%       0.64     0.698%     5.79%       0.64     0.698%     0.700       0.64     0.698     0.700       0.64     0.698     0.700       0.690     0     0       0     0     0       18     31     1			6			0	0	1		161
17     43     4       12     39     2       5     41     3       8     48     7       12     41     3       8     48     7       12     41     3       12     41     3       12     41     3       12     41     3       23     31     3       126     362     30       24     201     14       0.64     0.698     0.700       0.64     0.698     0.700       0     0     0       0     0     0       18     31     1			19				14			TOT
12         39         2           5         41         3           8         48         7           8         48         7           12         41         3           12         41         3           12         41         3           12         41         3           12         41         3           7         31         3           12         41         3           12         41         3           24         201         14           0.64         0.698         0.700           0.690         0.660         0           0.690         0.690         0           1         1         1		7 0	4			n (		~ ~		150
5         41         3           8         48         7           8         48         7           12         41         3           7         31         3           NL         NT         NR           126         362         30           24.32%         69.88%         5.79%           94         201         14           0.64         0.698         0.700         0           0.64         0.698         0.700         0           0.690         0.0700         0         0           1         NORTHBOUND         0         0           0         0         0         0         0           1         NT         NR         1         1	0 4 34	3	1	0 00	16 0	) <del></del> (	4	0 4		175
8         48         7           12         41         3           7         31         3           NL         NT         NR           126         30         30           24.32%         69.88%         5.79%           94         201         14           94         201         14           0.64         0.698         0.700         0           0.64         0.698         0.700         0           0.690         0.0700         0         0           18         31         1         1			1			-	0			177
12 41 3 7 31 3 NL NT NR 126 362 30 24.32% 69.88% 5.79% 0.64 0.698 0.700 0 0.64 0.698 0.700 0 0.690 0.690 0.700 0 0.690 0.690 0.701 14 0.690 0.700 0 0.690 14 0.691 16 0.691 14 0.691 14 0.690 17 0.690 17 0.691 14 0.690 17 0.690 17 0.600 17 0.000 17 0.0000 17 0.0000 17 0.0000 17 0.0000 17 0.0000 17 0.0000 17 0.0000 17 0	0 3 35	3	9	10		10		10		177
7 31 3 NL NT NR 126 362 30 24.32% 69.88% 5.79% 0.64 0.698 0.700 0 0.64 0.698 0.700 0 0.69 0.700 0 0.690 0 0.690 0 0.690 1 0.690 1 0.690 1 0.690 1 0.690 1 0.691 1 0.690 1 0.691 1 0.69	0 4 42		S			-	0 0	1		173
NL NT NR 126 362 30 24.32% 69.88% 5.79% 07.00 AM - 08:00 AM 94 201 14 0.64 0.698 0.700 0 0.690 0.690 0 0.690 0 0.690 0 0 0 0 0 NL NT NR 18 31 1	0 3 34	3		10	0	7	00		00	5 7 8
NL NT NR 126 362 30 24.329, 69.88% 5.79% 07.00 AN - 08:00 AM 94 201 14 0.64 0.698 0.700 0 0.690 0.690 0.690 0 0.690 0 NL NT NR 18 31 1										
126 362 30 24.32% 69.88% 5.79% 0.64 0.698 0.700 0 0.64 0.698 0.700 0 0.690 0.690 0.700 0 0.690 0 0.690 0 0.690 0 0.690 14 0.690 0 0.690 14 0.690 0 0.690 14 0.690 0 0.690 0 0.690 0 0.640 0.638 0.700 0 0.640 0.638 0.700 0 0.640 0.638 0.700 0 0.650 0 0.640 0.638 0.700 0 0.650 0.700 0 0.650 0.700 0 0.650 0.638 0.700 0 0.650 0 0.550 0 0.550 0 0.550 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		SR	Ц			M	TW	WR	MI	TOTAI
24.32% 69.88% 5.79% 07:00 AM - 08:00 AM 94 201 14 0.64 0.698 0.700 0 0.690 0.690 0.690 0 0.690 0 0.690 14 0.690 0 0.691 14 0.691 14 14 14 14 14 14 14 14 14 14	35	56 0	46	21 1	116 0	16	σ	51	2	1166
07:00 AM - 08:00 AM 94 201 14 0.64 0.698 0.700 0.690 0.690 NORTHBOUND 0 0 NL NT NR 18 31 1	0.00% 8.35%	13.37%	~	%8	%	3	19.57%	45.65%	0.00%	0011
94 201 14 0.64 0.698 0.700 0.690 0.690 0.690 NORTHBOUND 0 0 0 NL NT NR 18 31 1	W		Constant of the second	12		10				TOTAL
0.64 0.698 0.700 0.690 NORTHBOUND 0 0 0 NL NT NR 18 31 1	18	43				9	0	15	c	002
0.690 0 NORTHBOUND 0 0 0 NL NT NR 4:00 PM 18 31 1	0.000 0.643 0.690	0.489 0.000	0.434	0.500 0.830	30 0.000	0.417	0.563	0.536	0.000	2
0 0 0 0 0 NI NT NR 4:00 PM 18 31 1		0.653		.67			0.500	00		0.663
NORTHBOUND 0 0 0 NL NT NR 4:00 PM 18 31 1										
0 0 0 0 NL NT NR 4:00 PM 18 31 1	SOI	SOUTHBOUND		EASTBOUND	٥	_	WESTBOUND	GNIND		
NL NT NR 18 31 1	0	0	0		0 0	0	0	0	0	
18 31 1	SL	SR SU	EL	Ш	ER EU	ML	WT	WR	MN	TOTAL
1	0 3 47	7 0	2	0	2 0	4	4	1	0	150
4:15 PM 31 30 1 0	2	7 0	7	1 2	0 0	2	-	4		141

		NORTH	NORTHBOUND			SOUTHBOUND	BOUND			EASTBOUNE	DUND			WESTBOUN	BOUND		Γ
Md	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	Ц	Ш	ER	EU	WL	TW	WR	MN	TOTAI
4:00 PM	18	31	1	0	m	47	7	0	2	0	32	0	4	4	-	0	150
4:15 PM	31	30	1	0	2	30	7	0	7	1	20	0	7		4	0 0	141
4:30 PM	28	39	1	0	1	43	4	0	4	0	25	0	11	ŝ	2		161
4:45 PM		39	5	0	1	54	6	0	9	0	24	0	m	0	9	0	169
5:00 PM	28	47	0	0	2	62	5	0	9	0	34	0	7	4	2	0	197
5:15 PM		39	1	0	1	46	11	0	Ŋ	0	31	0	S	9	4	0	178
5:30 PM	in the second	29	m	0	1	49	ę	0	5	Ħ	22	0	0	2	2	0	138
5:45 PM	Sante	40	1	0	2	54	6	0	9	0	36	0	1	0	2	0	177
																	•
	NL	NT	NR	NN	SL	ST	SR	SU	E	Ш	æ	B	ML	MT	WR	MM	TOTAL
TOTAL VOLUMES :	203	294	13	0	13	385	55	0	41	2	224	0	38	20	23	0	1311
APPROACH %'s :	39.80%	57.65%	2.55%	0.00%	2.87%	84.99%	12.14%	0.00%	15.36%	0.75%	83.90%	0.00%	46.91%	24.69%	28.40%	0.00%	
PEAK HR :		04:30 PM - 05:30 PN	05:30 PM						たいないの			のないではない		NUCLAS OF			TOTAI
PEAK HR VOL :	107	164	7	0	2	205	29	0	21	0	114	0	26	13	14	0	705
PEAK HR FACTOR :	0.92	0.872	0.350	0.000	0.625	0.827	0.659	0.000	0.875	0.000	0.838	0.000	0.591	0.542	0.583	0.000	:
		0.927	27			0.80	56			0.84	4			0 0	00	2000	0.895

## Intersection Turning Movement Count

Location: Fort King Rd & Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-002 Date: 10/1/2020

NORTHEOUND         SOUTHEOUND         SOUTHEOUND         EASTBOUND         EASTBOUND           0 <th>NS/EW Streets:</th> <th></th> <th>Fort King Rd</th> <th>g Rd</th> <th></th> <th></th> <th>Fort King Rd</th> <th>g Rd</th> <th></th> <th></th> <th>Morningside Dr</th> <th>side Dr</th> <th></th> <th></th> <th>Morning</th> <th>Morninaside Dr</th> <th></th> <th>_</th>	NS/EW Streets:		Fort King Rd	g Rd			Fort King Rd	g Rd			Morningside Dr	side Dr			Morning	Morninaside Dr		_
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			NORTHE	DNND		A CONTRACTOR OF A CONTRACTOR	SOUTHB	GNND			EASTB	DNDO		Sala and and and	WEST	FROLIND	Situation	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0	0	0	0		0	0	0	0	0	0	0	0	0	0	C	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		NL	NT	NR	NU	321	ST	SR	SU	旧	Ы	ER	Ð	M	WT	WR	M	TOTAI
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	00 AM	0	2 L	0	0		e S	1	0	1	0	2	0	0	0	0	0	17
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15 AM	0	1	0	0		4	1	0	1	0	1	0	0	C		0 0	~
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	30 AM	1	0	0	0		1	0	0	9	0		0 0		0 0			o ç
0         2         0         0         3         0         0         1         0	45 AM	0	2	0	0		0	0	0		0	, <del></del>	0 0		0 0			C v
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	00 AM	0	2	0	0		e	0	0		0	0	0	0	0			2
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	15 AM	2	5	1	0		0	1	0	m	0	C	C	C	C			5
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	8:30 AM	1	S	0	0		1	0	0	0	0	0	0 0		0 0			7 v
NL         NT         NL         NL<	45 AM	0	0	0	0		0	0	0	-	0	-	0	0	00	00	00	5 0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	T	NL	NT	NR	NN	SL	ST	SR	SII	ш	Ŀ	ΕŖ	II	IVI	MT	M/D	11/11	TOTAL
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	UMES :	4	18	-	C	C	1	5	30	14	; c		3 <					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	: s,% H	17.39%	78.26%	4.35%	0.00%	0.00%	80.00%	20.00%	0.00%	61.54%	0.00%	38.46%	0.00%		5	D	5	5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	AK HR :	0	7:00 AM - (	NR 00:80		のないのであった。	ANY TON	No. Sector							ALCONTRACT.	100000000000000000000000000000000000000	Constant and a constant	TOTAL
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R VOL :	1	8	0	0		8	2	0	11	0	6	C	C	0	c	C	30
0.450       0.450       0.450       0.450         0       0       0       0       0       0         N       N       N       N       N       N         N       N       N       N       N       N         N       N       N       N       N       N         N       N       N       N       N       N         N       N       N       N       N       N         N       N       N       N       N       N         N       N       N       N       N       N         N       N       N       N       N       N         1       1       1       0       0       0       0         1       1       1       0       0       0       0       0         1       1       1       0       0       0       0       0       0         1       1       1       0       0       0       0       0       0       0       0         1       1       1       0       0       0       0       0       0 <td< td=""><td>CTOR :</td><td>0.250</td><td>0.400</td><td>0.000</td><td>0.000</td><td></td><td>0.500</td><td>0.500</td><td>0.000</td><td>0.458</td><td>0.000</td><td>0.450</td><td>0.000</td><td>0.000</td><td>0.000</td><td>0000</td><td>0000</td><td>3</td></td<>	CTOR :	0.250	0.400	0.000	0.000		0.500	0.500	0.000	0.458	0.000	0.450	0.000	0.000	0.000	0000	0000	3
NORTHBOUND         SOUTHBOUND           0         0         0         0           NL         NT         NR         VORTBOUND           SOUTHBOUND         SOUTHBOUND         SOUTHBOUND           NL         NT         NR           NL         N         SCOTHBOUND           NL         NR         NU           SOUTHBOUND         SCOTHBOUND           NL         NR           NL         NR           NU         SL           S         SL           S         SL           N         NU           S         SL           S         SL           S         SL           S         SL           N         NU           S         SL           S         SL      S			0.45	0			0.50	0			0.45	55			2000	0000	0000	0.750
NORTHBOUND         SOUTHBOUND           0	and the second se																	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	and the second se	2	NORTHE	NUND			SOUTHB	SOUND			EASTB	OUND			WEST	TBOUND		
NI         NR         NU         SI         SI         SI         NI         NR         NU         SI         SI<		0	0	0	0		0	0	0	0	0	0	0	0	0	0	0	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Stand The	NL	NT	NR	NU		ST	SR	SU	E	山	ER	EU	ML	TW	WR	MU	TOTAL
	MG 00:	2	2	0	0		1	0	0	0	0	1	0	0	0	1	0	6
	1:15 PM	1	1	0	0		1	1	0	0	0	1	0	0	0	C	C	С
	::30 PM	1	m	0	0		1	0	0	0	0	0	0	0	0	0 0	0 0	о го
	:45 PM		2	0	0		0	0	0	4	0	0	0	0	0	0	00	9 9
	MG 00:0		2	0	0		S	2	0	1	0	1	0	0	0	0	0	14
	:15 PM		0	0	0		0	0	0	1	0	0	0		0	) C	) C	- ^
	::30 PM		H	0	0		0	0	0	. +	0	•	) C		) C		) C	1 1
	:45 PM	H	2	0	0		1	0	0	0	00				0 0			7 4

FOTAL 48

WU 0 0.00%

WT 0 0.00%

WR

ML

EU 0 0.00%

ER 4 36.36%

ET 0 0.00%

Ч E

SU 0 0.00%

SR 3 21.43%

ST 9 64.29%

SL 2 14.29%

NU 0 0.00%

NR 0 0.00%

NT 13 61.90%

NL 8 38.10% 4:30 PM - 05:30 PI

63.64%

50.00%

50.00%

TOTAL 27 0.482

00000

0.000

0.000

1 0.250

0.000

1 0.250

0.000

6 0.375

0.000

2 0.250

60.300

0.000

0.000

0.000

0.583

0.33

4

TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR :

0.550

0.286

0.438

0.250

## Intersection Turning Movement Count

Location: Fort King Rd & Morningside Dr City: Dade City Control: 2-Way Stop (EB/WB)

Project ID: 20-120220-002 Date: 10/1/2020

								Bil	Bikes					Date:	<b>Date:</b> 10/1/2020		
NS/EW Streets:		Fort King Rd	ng Rd			Fort King Rd	ng Rd			Morning	Morningside Dr			Morningside Dr	jside Dr		
AM	N 0	NORTH 0 NT	NORTHBOUND 0 0 NT NR	0 NN	<mark>ତ</mark> ଅ	SOUTHBOUND 0 0 ST SR	BOUND 0 SR	s o	<mark>0</mark> 급	EASTI 0 ET	EASTBOUND 0 0 1T ER	E o	0	WEST 0 WT	WESTBOUND 0 0 0T WR	0	TOTAI
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:20 MM	0 0	0 0	0 0	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM		0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0	0	0	0	0	0
MA 00.8			00					0 0	0	0	0	0 0	0	0	0	0	0
8:15 AM	0	0 0	00	0 0	0 0	00	00	0 0					0 0		0 0	0 0	0 0
8:30 AM 8:45 AM	00	00	00	00	00	00	00	00	000	000	000	000	000	000	000	000	000
	Z	NT	an	IIN	υ	L L	G	CL	ū	t	6	Ē	14.1	5	-		, <u>-</u>
TOTAL VOLUMES : APPROACH %'s :	0	0	0	0	0	0	50	30	0	0	40	20	0	0	20	0	0
PEAK HR :	and the second second	07:00 AM - 08:00 AM	08:00 AM							Contraction of the second	Statistical Statistics			State States	ACCURATE ACCURATE	and second	TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	C	0	C	c	c	c	c	C	
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	<b>b</b>
PM	0	NORTH 0	NORTHBOUND 0 0	C	C	SOUTH	BOUND	C	C	EAST	EASTBOUND	c	c	WEST	WESTBOUND	c	
	NL	NT	NR	NU	SL	ST	SR	SU	, II	, E	<b>,</b> 出	, UI	ML	M	WR	MN	TOTAI
4:00 PM	00	<del>, 1</del> 0	0 0	0 0	0 0	0 0	00	0 0	0 0	0 0	0	0	0	0	0	0	
4:30 PM		00											0 0	0 0	0 0	0 0	0 0
4:45 PM	0	0 0	0	0 0	0	00	00	00	00	00	00	0 0	00	0 0			
5:00 PM		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM 5:45 PM	00	0 0	00	00	00	00	00	00	00	00	00	0 0	00	00	00	00	00
T	z	NT	NR	IIN	U	٦ ل	cD	CII	Ξ	Ŀ	8	ī	14/1	TAT.		14/11	*TOT
TOTAL VOLUMES :	0	H H	0	0	0	50	60	20	10	] 0	50	20	0	0	0	0	101AL
APPROACH %'s :	0.00%	100.00%	%00.0	0.00%													
PEAK HR :		04:30 PM - 05:30 PM	05:30 PM	Ellister an	States and			States and		French - State	N.N.K. NAM		The last of the last		A STATE AND A STAT	A COLORADO	TOTA
PEAK HR VOL :	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
PEAK HR FACTOR :	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	>
A NOT AND A DATE OF A DATE	Service and Constraints			Contraction of the second					CALCULATION CONTRACTOR			AND DESCRIPTION OF TAXABLE PARTY OF TAXA				The second se	

## Intersection Turning Movement Count Location: Fort King Rd & Morningside Dr City: Dade City Date: 10/1/2020

### Project ID: 20-120220-002 Date: 10/1/2020

### Pedestrians (Crosswalks)

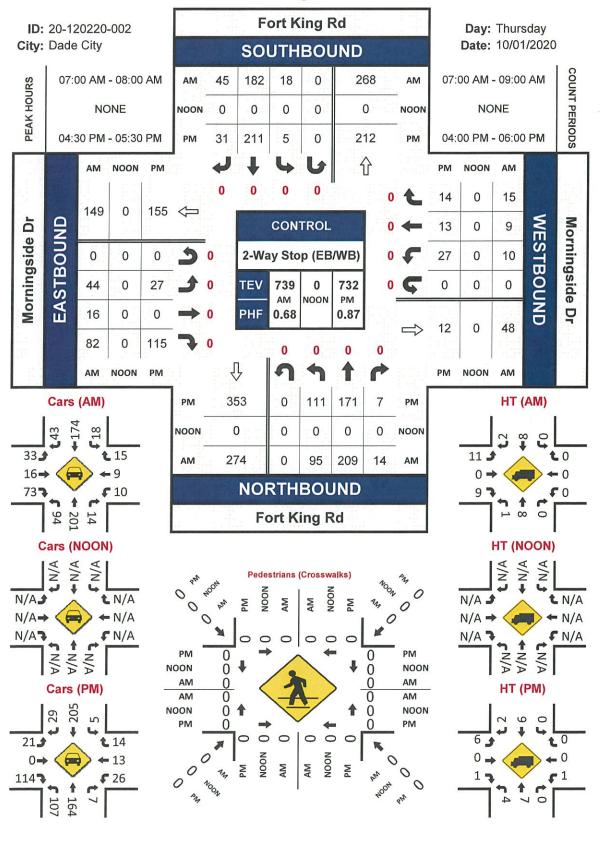
						-			
NS/EW Streets:	Fort King Rd	ng Rd	Fort K	Fort King Rd	Morningside Dr	side Dr	Morningside Dr	side Dr	
MM	NORTH LEG	I LEG	SOUT	SOUTH LEG	EAST	EAST LEG	WEST LEG	LEG	
	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
7:00 AM	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0
	B	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0
APPROACH %'s :									
PEAK HR :	07:00 AM - 08:00 AM	08:00 AM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
<b>PEAK HR FACTOR :</b>						State State			
	-								
	ITOON	(L -		0111					

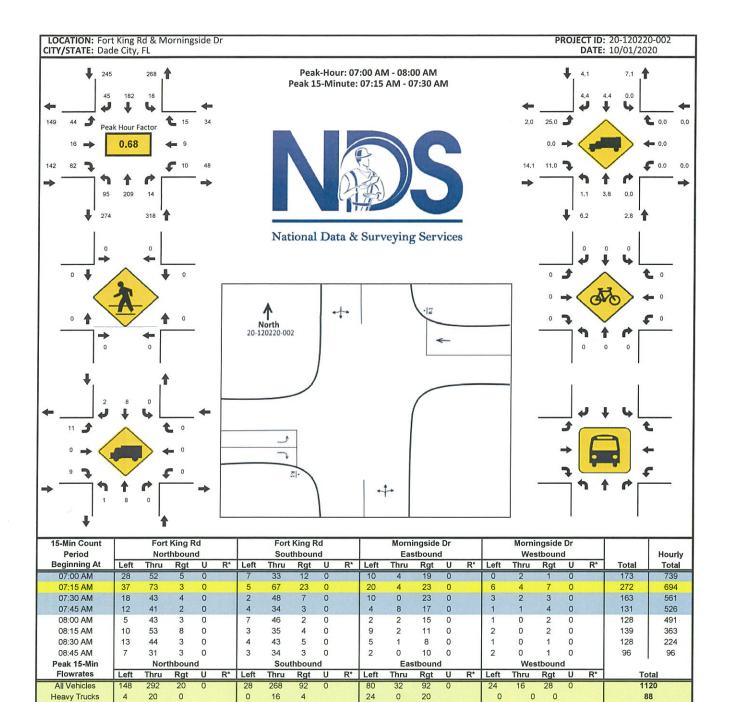
DNA	NORTH LEG	LEG	SOUTH LEG	H LEG	EAST LEG	LEG	WEST	WEST LEG	
LIM	EB	WB	EB	WB	NB	SB	NB	SB	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0
	B	WB	EB	WB	NB	SB	NB	SB	TOTAL
TOTAL VOLUMES :	0	0	0	0	0	0	0	0	0
APPROACH %'s :									
PEAK HR :	04:30 PM - 05:30 PM	05:30 PM							TOTAL
PEAK HR VOL :	0	0	0	0	0	0	0	0	0
<b>PEAK HR FACTOR :</b>									
									ななないの

Prepared by National Data & Surveying Services

### Fort King Rd & Morningside Dr

### Peak Hour Turning Movement Count

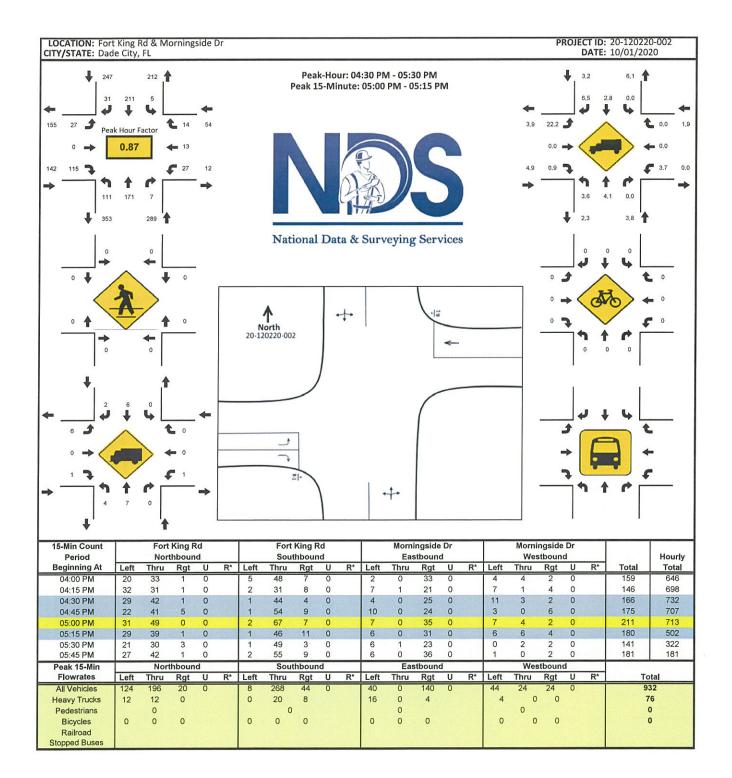




0 0

Pedestrians

Bicycles

Railroad Stopped Buses 

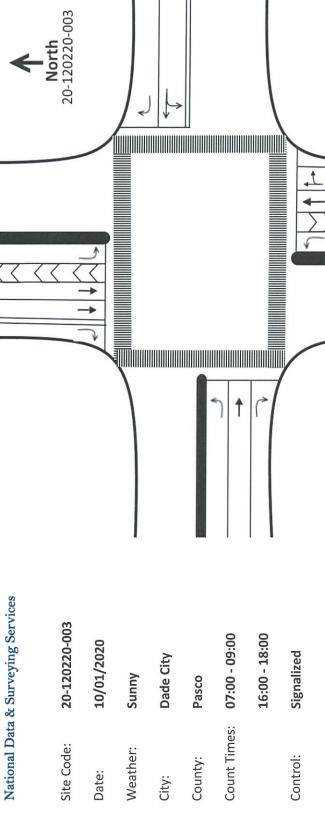


N/S Street: US 301

Ż

Speed: 50 MPH

E/W Street: Morningside Dr



### SIGNAL TIMING

PHASES	1	2	m
SL/ST	00:22	00:31	00:36
NT/ST	01:21	01:23	01:22
ET/WT	00:26	00:22	00:37

## Intersection Turning Movement Count

Location: US 301 & Morningside Dr City: Dade City

								2	Inno								
NS/EW Streets:		US 301	301			US 301	01			Morningside Dr	iide Dr			Morningside Dr	side Dr		
	0	NORTH	NORTHBOUND		0	SOUTHI	BOUND			EASTBOUND	<b>DNUC</b>			WESTBOUND	GUND		
AIVI	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	รา	ST	SR	SU	EL	E	ER	B	WL	WT	WR	MN	TOTAL
7:00 AM	1	91	4	0	9	96	2	0	3	1	0	0	4	0	4	0	212
7:15 AM	4	137	4	0	7	138	e	0	2	2	1	0	9	1	15	0	320
7:30 AM	2	152	S	m	5	172	9	0	1	0	-	C	ſ	C	10		367
7:45 AM	1	181	9	1	6	165	4	0	2	)	+ C			- c	2 1		202
8:00 AM	2	148	2	2	4	142	m	0	-	. 0			. ப	1 C	no		roc vec
8:15 AM	7	169	2	2	8	159	9	0	m	00	4 (r~		10	4 +	nα		378
8:30 AM	12	141	S	2	13	135	2	,	9 4	)	10		ζα		0 <sup>cc</sup>		344
8:45 AM	7	162	4	4	15	159 8	8	0	6	ŝ	14	0	13	50	6	00	399
	N	NT	NR	NN	SL	ST	SR	SU	H	Б	ER	EU	M	WT	WR	MI	TOTAL
TOTAL VOLUMES :	36	1181	35	14	67	1166	39	1	25	8	12	0	58	7	73	0	2722
APPROACH %'s :	2.84%	93.29%	2.76%	1.11%	5.26%	91.59%	3.06%	0.08%	55.56%	17.78%	26.67%	0.00%	42.03%	5.07%	52.90%	0.00%	
PEAK HR :		07:30 AM - 08:30 AM	- 08:30 AM	C. S.C.							144 A	10 × 10					TOTAL
PEAK HR VOL :		650	18	8	26	638	19	0	7	1	5	0	27	4	32	0	1447
PEAK HR FACTOR :	0.429	0.898	0.750	0.667	0.722	0.927	0.792	0.000	0.583	0.250	0.417	0.000	0.675	0.500	0.800	0.000	0.045
		0.910	10			0.933	33	1000		0.542	12			0.829	67		C+FC-U
		THOM															
DAA	c	NUKIH		c		South	SOUND			EASTBOUND	OUND			WESTBOUND	<b>ONND</b>		
<b>FIM</b>		D LV	O N		<b>&gt;</b> 7	- t	<mark>-</mark> 5	- <del>.</del>	<b>0</b> i	0	0 {	0	0	0	0	0	
4-00 DM	1	100	11	C C		10	YC CC	n o	러		Υ Υ	D o	ML	M	WK	NN	TOTAL
A-15 DM	10	ULC TOT	1	n r		100	5	0 0	17	4 (	χ,	0 0	23	-	15	0	563
MG UE-V	9 0	210		vr		06T	77	0 0	51	n u	1	0 0	23	2	19	0	619
	n u	000	TO	V C		7/1	14	0 0	61	n u	D I	0 0	18	m I	21	0	564
Md UU-3		100	10	7 0		077	70	0	19	7	י ה	0	1/	m	24	0	577
5.15 PM	βα	107	10			107		0 0	15	2	Ω.	0 0	25	4 (	17	0 0	623
PM 05:30 PM		222	17	- C		174	18		11	+ <	0 -		07	o r	D1C		252
5-45 DM		108	10	4 +		261	01		11	t (		0 0	71	<b>n</b> ,	2	0	212
	TO	1 70	'n	T		/01	11	D	77	D	10	0	24	4	23	0	466
	NL	NT	NR	NN	SL	ST	SR	SU	Е	E	ER	EU	ML	WT	WR	NN	TOTAL
TOTAL VOLUMES :		1880	86	14	161	1519	146	0	145	22	54	0	162	34	164	0	4476
APPROACH %'s :	4.30%	90.8/%	4.16%	0.68%	8.82%	83.19%	8.00%	0.00%	65.61%	9.95%	24.43%	%00.0	45.00%	9.44%	45.56%	0.00%	
PEAK HK :			M4 61:60 -														TOTAL
PEAK HR VOL :	_	103/	4/	9	83	807	72	0	72	10	27	0	83	12	81	0	2383
PEAK HK FACIUK :	160.0	150 0	0./83	0./.0	0.669	0.91/	0.818	0.000	0.947	0.833	0.614	0.000	0.830	0.750	0.844	0.000	

### Intersection Turning Movement Count

Location: US 301 & Morningside Dr City: Dade City Control: Signalized

Project ID: 20-120220-003 Date: 10/1/2020

I								Cars	LS						11 10 10 10 10 10 10 10 10 10 10 10 10 1		
NS/EW Streets:		US 301	01			10E 301	01			Morningside Dr	side Dr			Morningside Dr	side Dr		
		NORTHBOUND	BOUND			SOUTHBOUND	BOUND			EASTBOUND	OUND.			WESTBOUND	BOUND	Γ	
AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	Е	Б	ER	EU	MI	TW	WR	MIN	TOTAL
7:00 AM	1	06	4	0	9	92	2	0	1	0	0	0	4	0	4	0	204
7:15 AM	4	131	2	0	7	136	m	0	2	2	-	C	9		. Ļ		310
7:30 AM	2	144	2	e	5	164	9	0	. +1	0	0		) (r	+ 0	10		247
7:45 AM	1	174	5	1	6	157	4	0	2		0	0 0	9		4	0 0	365
8:00 AM	2	144	S	2	4	134	m	0	1	0	1	0	5	2	6	0	312
8:15 AM	7	164	2	2	8	152	9	0	e	0	m	0	8	1	8	0	364
8:30 AM	11	137	4	2	12	133	7	1	4	1	2	0	8	0	13	0	335
8:45 AM	2	155	4	4	14	153	8	0	6	m	4	0	10		6	0	381
	NL	IN	NR	NN	SL	ST	SR	SU	Ц	占	R	EU	ML	WT	WR	MN	TOTAL
TOTAL VOLUMES :	35	1139	28	14	65	1121	39	1	23	7	11	0	52	9	72	0	2613
APPROACH %'s :	2.88%	93.67%	2.30%	1.15%	5.30%	91.44%	3.18%	0.08%	56.10%	17.07%	26.83%	0.00%	40.00%	4.62%	55.38%	0.00%	
PEAK HR :		07:30 AM - 08:30 AM	08:30 AM	The states of the	The state of the s												TOTAL
PEAK HR VOL :	12	626	14	8	26	607	19	0	7	-	4	0	24	4	31	0	1383
<b>PEAK HR FACTOR :</b>	0.43	0.899	0.700	0.667	0.722	0.925	0.792	0.000	0.583	0.250	0.333	0.000	0.750	0.500	0.775	0.000	
		0.912	12	Alter Land		0.931	11			0.500	00			0.868	68		0.947
		NORTHBOUND	BOUND			SOUTHBOUND	GUND			EASTBOUND	<b>ONND</b>		1	WESTE	WESTBOUND		
PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	TN	NR	N	SL	ST	SR	SU	EL	ET	ER	EU	ML	TW	WR	MN	TOTAL
4:00 PM	15	196	11	m	18	203	23	0	21	4	8	0	23	7	15	0	547

		NORTHBOUND	30UND			SOUTHB	THBOUND			EASTBOUND	DNUC			WESTBOUNI	DUND		
MY	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	NL	TN	NR	NU	SL	ST	SR	SU	EL	ET	H	B	WL	MT	WR	MU	TOTAL
4:00 PM	15	196	11	m	18	203	23	0	21	4	8	0	23	7	15	0	547
4:15 PM	18	261	15	2	17	194	22	0	19	m	10	0	23	2	19	0	605
4:30 PM	6	253	6	2	31	169	14	0	19	m	9	0	17	m	21	0	556
4:45 PM	9	226	12	2	17	214	20	0	18	2	2	0	17	m	24	0	566
5:00 PM	10	277	10	m	18	215	16	0	15	2	5	0	25	4	17	0	617
5:15 PM	8	218	7	0	26	181	22	0	20	4	8	0	20	80	20	0	542
5:30 PM	13	218	12	1	16	172	17	0	11	4	-	0	12	m	25	0	505
5:45 PM	10	195	6	1	18	133	10	0	21	0	10	0	23	4	23	0	457
	NL	τN	NR	NN	SL	ST	SR	SU	EL	Ш		EU	ML	MT	WR	NN	TOTAL
TOTAL VOLUMES :	89	1844	85	14	161	1481	144	0	144	22		0	160	34	164	0	4395
APPROACH %'s :	4.38%	90.75%	4.18%	0.69%	9.01%	82.92%	8.06%	%00.0	65.75%	10.05%	24.20%	0.00%	44.69%	9.50%	45.81%	0.00%	
PEAK HR :	The second second	04:15 PM - 05:15 PM	05:15 PM								14.18						TOTAL
PEAK HR VOL :	43	1017	46	6	83	792	72	0	71	10	26	0	82	12	81	0	2344
PEAK HR FACTOR :	0.60	0.918	0.767	0.750	0.669	0.921	0.818	0.000	0.934	0.833	0.650	0.000	0.820	0.750	0.844	0.000	010 0
		0.929	6			0.94	3			0.83	9			0.95	51		066.0

### Intersection Turning Movement Count

TOTAL 81 109 109 TOTAL 101AL 16 14 8 8 8 11 10 10 7 9 9 TOTAL 0.800 8 110 112 114 114 114 118 64 WU 0 0.00% WU 0 0.00% 0.000 0 WU 0 00000000 00000000 Project ID: 20-120220-003 Date: 10/1/2020 WR 0 0.00% 12.50% 1 0.250 WR WR. Morningside Dr 000 0000 0 WR 0000 0000 WESTBOUND WESTBOUND 0.500 WT 0 0.00% 12.50% 00000 05 05 0000000 5 00000000 WL 6 75.00% WL 2 100.00% 3 0.375 M 0 0 0 1 0 0 0 M o X 0000000 EU 0 0.00% EU 0 0.00% 0.000 0000 020000 0000 O D 0000 25.00% 50.00% 1 0.250 Morningside Dr R 000000 R EASTBOUND 0 8 0 0000 0 E EASTBOUND 0.250 ET 0 0.00% 25.00% 0.000 0 0000000 山 50.00% 00000 2 E 0 .... 0 1 0000 리 -00000000 000 둪 SU 0 0.00% SU 0 0.00% 0.000 00000 0000 SU o 000000000 SR 0 0.00% SR 2 5.00% 0.000 SOUTHBOUND 0 0 ST SR SOUTHBOUND 0 0 ST SR SR 0 000 0000 00000 0 US 301 0.969 95.74% ST 38 95.00% 31 0.969 **ST** 10000N NO 400004 4.26% SL 0 0.00% 0.000 110000011 SL 2 NU 0 0.00% NU 0 0.00% 0.000 O N 00000000 0NN 00000000 14.00% 07:30 AM - 08:30 AN 0.333 NORTHBOUND 0 0 NT NR NORTHBOUND O N N F NN ~ 0 ¥ 0 0 ₩ T 00 HO -00000 US 301 Location: US 301 & Morningside Dr City: Dade City Control: Signalized 0.636 NT 42 84.00% 24 0.750 0 5 36 36 1000 4 10 4 N 50 m d 4 4 m NL 0 0.00% NL 1 2.00% 0.000 000000 10 00000000 o Z 이키 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:30 AM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:37 PM 5:37 PM PEAK HR VOL : PEAK HR FACTOR : NS/EW Streets: TOTAL VOLUMES : TOTAL VOLUMES : APPROACH %'s PEAK HR AM PM

TOTAL 39

0.696

0.000

0.000

0.000

1 0.250

0.000

1 0.250

0.000

1 0.250

0.000

0.000

15 0.625

0.000

0.000

0.250

20 0.556

0.00

PEAK HR VOL : PEAK HR FACTOR :

0.583

2.70%

97.30%

APPROACH %'s :

PEAK HR

- 05:15

04-15

0.625

ć

50.00%

0.500

0.250

### Intersection Turning Movement Count

Location: US 301 & Morningside Dr City: Dade City Control: Signalized

Project ID: 20-120220-003 Date: 10/1/2020

L	1							Bikes	es					-	0202 /T /01		
NS/EW Streets:		US 301	01			US 301	01			Morningside Dr	side Dr			Morningside Dr	Iside Dr		
		NORTHBOUND	BOUND			SOUTHBOUND	BOUND			EASTI	EASTBOUND			WESTE	WESTBOUND		
AIVI	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
「「ない」の「「「「ない」」の	NL	NT	NR	NU	SL	ST	SR	SU	Ц	Ш	ER	EU	ML	TW	WR	MIN	TOTAI
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	C	0	C	C	
7:15 AM	0	1	0	0	0	1	0	0	0	C	C	0					
7:30 AM	0	0	0	0	0	-	0	0	0	0	0 0						J +
7:45 AM	0	0	0	0	0	0	0	0			0 0						
8:00 AM	0	0	0	0	0	0	0	0	0	0	0						
8:15 AM	0	0	0	0	0	0	C	0 0	0 0								
8:30 AM	0	0	0	0	0	0	0	0	0	0	00						
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	00	00	0 0	00	00
		T.M.	-		ō												
	NL	N	NK	NN	۲	2	SK	SU	Щ	Ш	æ	B	ML	T N	WR	MU	TOTAL
TOTAL VOLUMES :	0	H	0	0	0	2	0	0	0	0	0	0	0	0	0	0	m
APPROACH %'s :	0.00%	100.00%	0.00%	%00.0	%00.0	100.00%	0.00%	0.00%									
PEAK HR :	<b>)</b>	07:30 AM - 08:30 AM	08:30 AM	States of	5-1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1- 1-	199 19 19	New Street	and the second	1		- 1. 25 × 21	A Contraction	AS O LAN				TOTAL
PEAK HR VOL :	0	0	0	0	0	1	0	0	0	0	0	0	0	0	c	c	-
PEAK HR FACTOR :	0.000	0.000	0.000	0.000	0.000	0.250 (	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.250
						7.0	0									No. of Street,	
「「「「「「「」」」」」」」」」」」」」」」」」」」」」」」」」」」」」														A INC. IN CALL			
NG	C			c	C			(	(	ILCY J		. 1		MEDIE	BUUND		
<b>TIM</b>				0		D	D	D	0	0	0	0	0	0	0	0	
100 1	NL	Z	NK	NN	SL	ST	SR	SU	Ц	ш	ER	EU	ML	TW	WT WR	MU	TOTAL
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	C	C
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	0	
5:30 PM	0	3	0	0	0	1	1	0	0	0	0	0	C	C	C	C	( LC
5:45 PM	0	1	0	0	0	1	0	0	0	0	1	0	C	C	C	C	
	ç																)

TOTAL

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TOTAL 9

NN 0

WR 0

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N O

EU 0 0.00%

ER 1 100.00%

ET 0 0.00%

EL 0 0.00%

SU 0 0.00%

SR 1 25.00%

ST 3 75.00%

SL 0 0.00%

NU 0 0.00%

NR 0 0.00%

۲ **4** 

NL 0 0.00% 04:15 PM - 05:15 PI

TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR :

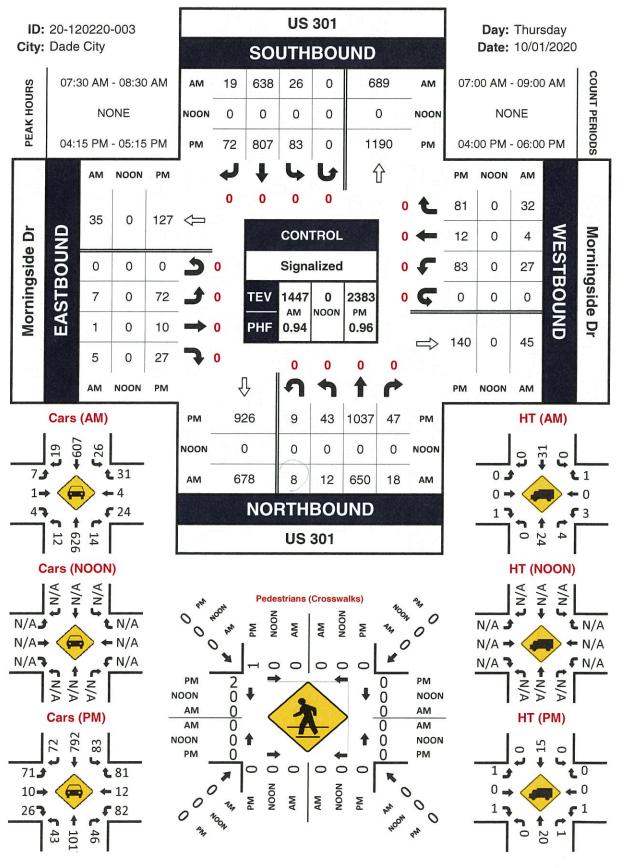
100.00%

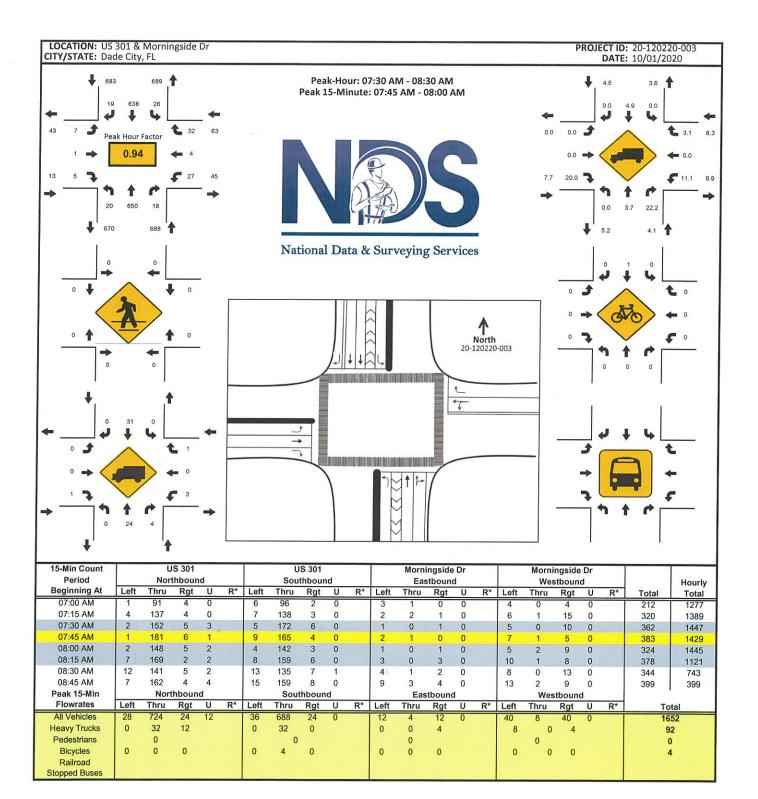
# Location Interpretent Date City: Dade City: Dade City: Dade City Dade City Pedestrians (Crosswalks)

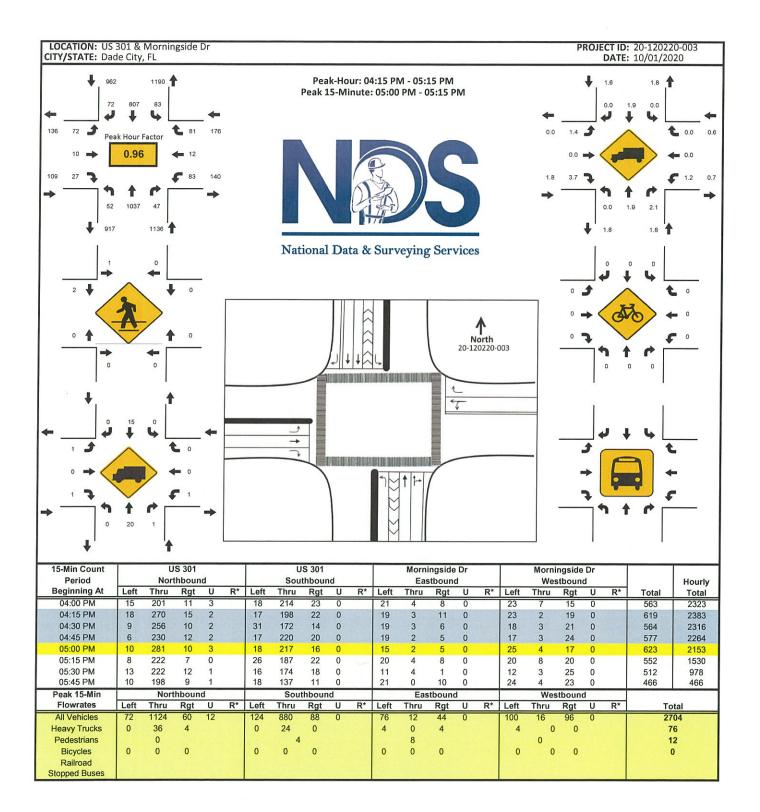
		Pedestrians	(Crosswaiks)		
NS/EW Streets:	US 301	US 301	Morningside Dr	Morningside Dr	
MM	NORTH LEG	SOUTH LEG	EAST LEG	WEST LEG	
	EB WB	EB WB	NB SB	NB SB	TOTAL
7:00 AM		0 1	0 0	1 0	2
7:15 AM		0 0	0 0	0	0
7:30 AM	0	0 0	0	0	0
7:45 AM	0	0	0	0	0
8:00 AM		0	0		0
8:15 AM		0 0	0 0	0	0
8:30 AM	0 0	0 0	0 0		0
8:45 AM		0 0	0	0 0	0
				(	1
	EB WB				TOTAL
<b>TOTAL VOLUMES :</b>	0	0 1	0 0	1 0	2
APPROACH %'s :		0.00% 100.00%		100.00% 0.00%	
PEAK HR :	07:30 AM - 08:30 AM				TOTAL
PEAK HR VOL :	0 0	0	0	0	0
<b>PEAK HR FACTOR :</b>					
20.0	NORTH LEG	SOUTH LEG	FAST LEG	WESTIEG	
PM	EB WB	EB WB	NB SB	NB SB	TOTAL
4:00 PM	0 0	0 1	0	0	1
4:15 PM	1 0	0 0	0 0	0 0	
4:30 PM	0	0	0 0	0 2	2
4:45 PM	0 0	0 0	0 0	0 0	0
5:00 PM	0	0	0	0	0
5:15 PM	0	0 0	0 0	0 0	0
	•				

### US 301 & Morningside Dr

### Peak Hour Turning Movement Count







APPENDIX - C

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D FACTOR



	D Factor MB	0.51	0.51	0.51										
	D Fa EB	0.49	0.49	0.49										
	AVG WB	145	113	Avg		• .				 • • .	·	-	· .	
	EB	138	107											
de (East of SR 52) (48 Hour Machine Counts)	Day 2 WB	135	114											
de (East of (48 Hour N	Da EB	128	106											
Morning Side (East of SR 52) (48 Hour Machin	Day 1 WB	154	112						·					
	EB	148	108											
		7:00-8:00	5:00-6:00											
		AM	M											

	ctor	WB	0.56	0.55	0.55
	D Factor	EB	0.44	0.45	0.45
	ŋ	WB	49	144	Avg
	AVG	EB	38	120	
unts)					
US 301) 1achine Co	y 2	WB	49	139	
Side (East of US 301) (48 Hour Machine Counts)	Day 2	EB	39	124	
Morning Side (East of US 301) (48 Hour Machine	1	WB	48	148	
	Day 1	8	37	115	
			7:30-8:30	4:15-5:15	

МЧ

AM

### T-FACTOR

1

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### Truck Percentage-T Factor

Road)
King F
Б.
from SR 52 to F
m SR
fro
Ş
e Drive
ingside Drive
<b>Morningside Drive</b>

Intersection	AM Total Approach Existing Traffic (1)	AM Total Approach Existing Truck Traffic (1)	%Trucks	PM Total Approach Existing Traffic (1)	PM Total Approach Existing Truck Traffic (1)	%Trucks
Morningside Dr And SR 52/Adair Rd	146	ъ	3%	144	2	1%
Morningside Dr And Fort King Road	142	20	14%	142	7	5%
0		Avg	%6		Avg	3%
					Avg AM and PM	%9

Avg AM and PM (1) Based on Exiting Turning movement counts-Westbound Approach Volumes at Morningside Dr and SR52 intersection And Eastbound Approach Volumes at Moningside Dr and Fort King Road Intersection

SEASONAL FACTORS

•



-	PEAK SEASON FACTOR CATEGORY ORY: 1400 PASCO COUNTYWIDE	REPORT - REPO	RT TYPE:	ALL		•
WEEK	DATES	SF	MOCF: 0 PSCF	.95		
WEEK 123456789011234567890112345678901222222222222222222222222222222222222	DATES 01/01/2019 - 01/05/2019 01/06/2019 - 01/12/2019 01/13/2019 - 01/12/2019 01/20/2019 - 01/26/2019 02/03/2019 - 02/03/2019 02/10/2019 - 02/16/2019 02/17/2019 - 02/23/2019 02/24/2019 - 03/02/2019 03/03/2019 - 03/02/2019 03/10/2019 - 03/23/2019 03/10/2019 - 03/23/2019 03/12/2019 - 03/30/2019 03/12/2019 - 03/30/2019 03/24/2019 - 03/30/2019 04/07/2019 - 04/20/2019 04/21/2019 - 04/20/2019 04/21/2019 - 04/27/2019 04/22/2019 - 05/18/2019 05/12/2019 - 05/18/2019 05/12/2019 - 05/18/2019 05/12/2019 - 06/01/2019 06/02/2019 - 06/15/2019 06/09/2019 - 06/22/2019 06/09/2019 - 06/22/2019 06/23/2019 - 06/22/2019 06/30/2019 - 07/13/2019 07/14/2019 - 07/20/2019 07/14/2019 - 07/20/2019 07/21/2019 - 07/20/2019 07/22/2019 - 08/33/2019 08/04/2019 - 08/32019 08/04/2019 - 08/31/2019 08/11/2019 - 08/17/2019 08/11/2019 - 08/17/2019 08/11/2019 - 08/17/2019 08/04/2019 - 08/31/2019 08/04/2019 - 08/10/2019 08/04/2019 - 08/22/2019 08/04/2019 - 08/22/2019 09/05/2019 - 09/07/2019 09/01/2019 - 09/07/2019 09/01/2019 - 09/07/2019 09/022/2019 - 10/22/2019 10/06/2019 - 10/12/2019 10/06/2019 - 10/22/2019 10/06/2019 - 10/22/2019 10/06/2019 - 10/22/2019 10/06/2019 - 10/22/2019 10/06/2019 - 10/22/2019 10/06/2019 - 10/22/2019 10/06/2019 - 10/22/2019 10/02/2019 - 11/02/2019 11/02/2019 - 11/02/2019	0.98 1.00 1.03 1.01 1.00 0.98 0.97 0.96 0.95 0.94 0.93 0.93 0.93 0.94 0.93 0.94 0.95 0.94 0.95 0.96 0.97 0.98 0.99 1.01 1.02 1.02 1.02 1.02 1.02 1.03 1.04 1.04 1.04 1.04 1.05 1.05 1.05 1.06 1.06 1.06 1.06 1.08 1.08 1.08 1.03 1.03 1.03 1.04 1.05 1.05 1.06 1.06 1.06 1.05 1.03 1.03 1.04 1.05 1.05 1.06 1.06 1.06 1.06 1.06 1.05 1.03 1.01 1.03 1.03 1.01 1.00 1.03 1.03 1.01 1.00 1.03 1.03 1.03 1.03 1.04 1.05 1.05 1.06 1.06 1.05 1.03 1.03 1.03 1.03 1.04 1.05 1.05 1.06 1.06 1.05 1.03 1.03 1.01 1.00 1.03 1.03 1.01 1.00 1.03 1.03 1.01 1.00	PSCF 1.03 1.05 1.08 1.06 1.05 1.02 1.01 1.00 0.99 0.99 0.99 0.99 0.99 0.99 0.99 1.00 1.01 1.02 1.03 1.04 1.06 1.07 1.08 1.09 1.09 1.09 1.09 1.09 1.01 1.02 1.03 1.04 1.06 1.07 1.08 1.09 1.09 1.09 1.09 1.01 1.02 1.03 1.04 1.06 1.07 1.08 1.09 1.09 1.09 1.09 1.01 1.02 1.03 1.04 1.06 1.05 1.04 1.02 1.11 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.08 1.06 1.05 1.04 1.08 1.05 1.04 1.08 1.09 1.09 1.01 1.11 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.13 1.14 1.14 1.06 1.05 1.04 1.03	FDOT	48 hour 48 hour movent c	
46	11/10/2019 - 11/16/2019	0.99	1.04			

\* PEAK SEASON

14-FEB-2020 15:39:31

830UPD

7\_1400\_PKSEASON.TXT

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AXLE FACTORS



2019 WEEKLY AXLE FACTOR CATEGORY REPORT - REPORT TYPE: DISTRICT

-

COUNTY: 14 - PASCO

1404 SR52 - HERNAND 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98
1403         SR41, SR52       - HERNAND         0.92       0.92         0.92 <t< td=""></t<>
I 402 I 402 0 . 96 0 . 96
75, HILLS C0 = 1401 C0 = 0.90 0.90 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.88 0.99 0.88 0.99
WEek DATES DATES To 101/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 02/12/2019 - 03/12/2019 - 01/12/2019 - 01/12/2019 - 11/12/2019 - 11/12/2019 - 11/12/2019 - 11/12/2019 - 12/21/2019 -

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2019 WEEKLY AXLE FACTOR CATEGORY REPORT - REPORT TYPE: DISTRICT

COUNTY: 14 - PASCO

1408	10000000	୶୶୶୶୶୶୶୶	າດດດດດດ	<u>್ ಎ ಎ ಎ ಎ ಎ ಎ</u>	\		
1407	। ରଗରଗରଗର	, , , , , , , , , , , , , , , , , , ,	ຑຓຓຓຓຓຓຓ	موموموم	, , , , , , , , , , , , , , , , , , ,	0000000000	0.97 0.97 0.97 0.97 0.97 0.97 0.97
1406	ၣၯၯၹၹၹၹၯ	ڡ؋؋؋؋؋؋	စ္ ထဲ ထဲ ထဲ ထဲ ထဲ ထဲ ထဲ				000000000000000000000000000000000000000
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WEEK DATES	01/01/2019 - 01/05/2019 01/06/2019 - 01/12/2019 01/13/2019 - 01/19/2019 01/20/2019 - 01/26/2019 01/27/2019 - 02/02/2019 02/03/2019 - 02/09/2019	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 05/26/2019 = 06/04/201 3 06/02/2019 = 06/08/201 4 06/09/2019 = 06/15/201 5 06/16/2019 = 06/22/201 6 06/22/2019 = 06/22/201 7 06/30/2019 = 07/06/201 8 07/07/2019 = 07/13/201	9 $07/14/2019 - 07/20/201$ 1 $07/21/2019 - 07/27/201$ 1 $07/28/2019 - 08/03/201$ 2 $08/04/2019 - 08/10/201$ 3 $08/11/2019 - 08/17/201$ 4 $08/11/2019 - 08/17/201$ 5 $08/25/2019 - 08/31/201$ 6 $09/01/2019 - 09/07/201$	7 $09/08/2019 - 09/14/201$ 8 $09/15/2019 - 09/21/201$ 9 $09/22/2019 - 09/28/201$ 0 $09/29/2019 - 10/05/201$ 1 $10/06/2019 - 10/12/201$ 2 $10/13/2019 - 10/19/201$ 3 $10/20/2019 - 10/19/201$ 4 $10/27/2019 - 11/02/201$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

SR54, CK581 - 1412 0.999 0.990 0.9990 0.9990 0.9900 0.9900 0.9990 0.9900 0.99900 0.99000 0.99000 0.99000 0.990000 0.9900000000
1411 1411 1411 1411 1411 1411 1411 141
I410 SR54, US41 - 1410 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.9
1409         1400         0.90         0.90         0.89 <t< td=""></t<>
WEEK DATES DATES TO 1/10/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 02/01/20/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/01/202019 - 02/01/202/2019 - 02/01/202/2019 - 02/01/202/2019 - 02/01/202/2019 - 02/01/202/2019 - 02/01/202/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/01/202/2019 - 02/02/202/202/2019 - 02/01/202/202/2019 - 02/01/202/2019 - 02/01/2

	1416 52 CDE77 CDE2	๎๎๛๎๛๎๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛
	то 14 14	2 C C S S S S S C C C C C S S S S S S S S
TOTUICIO . TILEP. INCLUS	1414 SR52 CR587 - CR581	
TYPE THE THE TYPE THE TYPE THE	141 1519 - CR	
- PASCO	S	01/15/2019 01/15/2019 02/16/2019 02/16/2019 02/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 03/16/2019 04/13/2019 05/111/2019 06/12/2019 06/12/2019 06/12/2019 06/12/2019 07/2019 06/12/2019 09/01/2019 09/01/2019 09/01/2019 09/01/2019 09/01/2019 09/01/2019 09/01/2019 09/01/2019 00/12/2019 00/12/2019 00/12/2019 00/12/2019 00/12/2019 00/21/2019 00/21/2019 00/21/2019 00/21/2019 00/21/2019 00/21/2019 00/21/2019 00/21/2019 00/22/2019 00/21/2019 00/22/2019 00
COUNTY: 14	WEEK DATE	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

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1420         0.99 <t< th=""><th>, o o o</th></t<>	, o o o
SR575, US 0.90 0.89 0.89 0.89 0.89 0.89 0.89 0.89	തതയ
1418 1418	000
R533, US301 1417 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94	<u> </u>
WEEK DATES SR State 101/01/2019 - 01/13/2019 - 01/13/2019 - 01/13/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 03/10/2019 - 04/12/2019 - 04/12/2019 - 04/12/2019 - 04/12/2019 - 04/12/2019 - 04/12/2019 - 05/11/2019 - 05/12/2019 - 05/11/2019 - 05/12/2019 - 05/12/2019 - 07/10/2019 - 01/10/2019 - 03/10/2019 - 01/10/2019 - 03/10/2019 - 00/12/2019 - 03/10/2019 - 00/12/2019 -	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

SR 39, H1L24 0.89 0.89 0.89 0.89 0.89 0.89 0.89 0.89	
SR 700, US 31-PASCO 1423 1433 143	
1422 US41, CR583 - HERN 0.90 0.90 0.89 0.89 0.89 0.89 0.89 0.89	
1421 1421 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.98	
WEEK DATES BR 101/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 01/12/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 02/02/2019 - 03/02/2019 - 04/02/2019 - 04/02/2019 - 04/02/2019 - 04/02/2019 - 04/02/2019 - 04/02/2019 - 04/02/2019 - 04/02/2019 - 02/	

신문		ααα		တ္တ	ບຸບຸ	αα	ιωα		οœ	œ,α		۳œ.	ωα		 	ι Ψ.	νœ.	ω.α		ω.α		ω.ο		ω.		010				ω.
1427 PASCO CENTRAL HPMS	06.00	ω ω α		م،م،	ຸຸ	ω.α			°	œα		°.0	ωα		».α	°.°	°. w	œα		ω.α		°, o	°. C	°,	<u>, o</u>	ົ່ວ	<u>, o</u>	െറ്	<u>م</u> و ،	ω.
1426 PASCO EASTERN HPMS 2	0.0000000000000000000000000000000000000	$\infty \infty \infty$	600	<u>າ</u> ດ,	<u>,                                    </u>	α α	,		° œ	ω.α		0.00	ω.α	• • • •	».α.	<i>с</i> , с	°°°	ω.α	°	ω.α		ω, o	• ••••	ω ¢	n or	പ്പ	<u>)</u> ດ.	<u>م</u> م	<u>م</u> .	œ
42 H	0.00 0.00 0.80 0.80 0.80	88.8	<u>م</u> ص	ກດຸດ	<u>, o</u>	œ.α	ωα	, co. a				• ••	ω.α		°. w	æ, c	°	ω α	. ~.	ω,α	· ~ .	ω a	• •• •	ω. c	, <b>.</b> ,	ი o	<u>, .</u>	<u>ە</u> .	<u> </u>	°,
EK DATES	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	01/27/2019 - 02/02/201 02/03/2019 - 02/09/201 02/10/2019 - 02/16/201	8 02/17/2019 - 02/23/201 9 02/24/2019 - 03/02/201	1 03/10/2019 = 03/09/201	3 03/24/2019 - 03/20/201	4 03/31/2019 - 04/06/201 5 04/07/2019 - 04/13/201	6 04/14/2019 - 04/20/201 7 04/21/2019 - 04/27/201	8 04/28/2019 - 05/04/201 9 05/05/2019 - 05/11/201		1 05/19/2019 - 05/25/201 2 05/26/2019 - 06/01/201	3 06/02/2019 - 06/08/201 0 06/00/2019 - 06/15/201	5 06/16/2019 - 06/22/201	6 06/23/2019 - 06/29/201 7 06/30/2019 - 07/06/201		9 07/21/2019 - 07/27/201	1 07/28/2019 - 08/03/201	3 08/11/2019 - 08/11/201	4 08/18/2019 - 08/24/201 5 08/25/2019 - 08/31/201	6 09/01/2019 - 09/07/201	7 09/08/2019 - 09/14/201 8 09/15/2019 - 09/21/201	9 09/22/2019 - 09/28/201	0 09/29/2019 - 10/05/201 1 10/06/2019 - 10/12/201	2 10/13/2019 - 10/19/201	3 10/20/2019 - 10/26/201	5 11/03/2019 - 11/09/201	$\begin{cases} 6 & 11/10/2019 - 11/16/201 \\ 7 & 11/17/2019 - 11/23/201 \\ \end{cases}$	8 11/24/2019 - 11/30/201	9 12/01/2019 - 12/07/201 0 12/08/2019 - 12/14/201	12/15/2019 - 12/21/201 12/22/2019 - 12/28/201	3 12/29/2019 - 12/31/201

1431	
43	
142 142	
DATES	99999999999999999999999999999999999999
WEEK D	$\begin{array}{c} 1 \\ 1 \\ 2 \\ 3 \\ 3 \\ 0 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$

APPENDIX - D

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INTERSECTION ANALYSIS (EXISTING)



		ŀ	ICS7	Two	-Way	/ Sto	p-Co	ntro	Rep	ort								
General Information							Site	Infor	matio	n								
Analyst							Inter	section		·	Τ							
Agency/Co.							Juris	diction			1							
Date Performed	11/5,	/2020					East/	West Str	eet		Morr	ingside Drive/Adair						
Analysis Year	2020	)					Nort	h/South	Street		SR 52	2						
Time Analyzed	AM F	Peak					Peak	Hour Fa	ctor		0.81							
Intersection Orientation	Nort	h-South					Anal	ysis Time	Period	(hrs)	0.25							
Project Description	Existi	ing Peak	Season				•				1							
Lanes																		
					in in Majo	ן די אונע אונע Street No	計創品											
Vehicle Volumes and Ad	justme	nts																
Approach		Easth	ound		<u> </u>	West	bound		ļ	North	ibound	<b>.</b>	ļ	South	bound	<del></del>		
Movement	Ų	L	Т	R	υ	L	T	R	U	L_	Т	R	υ	L	Т	R		
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6		
Number of Lanes		0	1	0		1	1	0	0	1	1	0	0	1	1	0		
Configuration			LTR			L		TR		L		TR	ļ	L		TR		
Volume (veh/h)		32	36	44		67	10	85		23	345	58		49	392	18		
Percent Heavy Vehicles (%)		3	3	3		3	3	3		3				3				
Proportion Time Blocked																		
Percent Grade (%)		I	0				0											
Right Turn Channelized																		
Median Type   Storage				Undi	vided													
<b>Critical and Follow-up H</b>	eadwa	ys																
Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1				
Critical Headway (sec)		7.13	6.53	6.23		7.13	6.53	6.23		4,13				4.13				
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2				
Follow-Up Headway (sec)		3.53	4.03	3.33		3.53	4.03	3.33		2.23				2.23				
Delay, Queue Length, an	d Leve	l of Se	ervice									<i>.</i>						
Flow Rate, v (veh/h)			138			83		117		28				60				
Capacity, c (veh/h)			204			113		482		1053				1061				
v/c Ratio			0.68			0.73		0.24		0.03				0.06				
95% Queue Length, Q95 (veh)			4.2			<b>4.0</b>		0.9		0.1				0.2				
Control Delay (s/veh)			53.4			95.0	)	14.9		8.5				8.6				
Level of Service (LOS)			F		i l	F		В		А				А				
Approach Delay (s/veh)		53	.4			48	3.0			0	.5			0	.9			
Approach LOS		ŀ	:				=											

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HCSTM TWSC Version 7.8 AM Peak SR 52 and Morningside.xtw Generated: 11/23/2020 10:00:57 AM

						/ Sto										
General Information							Site	Infor	natio	n						
Analyst								section								
Agency/Co.							Juriso	liction								
Date Performed	11/5,	2020					East/	West Stro	eet		Morn	ingside	Drive/Ac	dair		
Analysis Year	2020						North	n/South :	Street		SR 52	2				
Time Analyzed	PM P	eak					Peak	Hour Fac	ctor		0.86					
Intersection Orientation	Nort	n-South					Analy	sis Time	Period (	(hrs)	0.25					
Project Description	Existi	ng Peak	Season													
Lanes																
					กเฉล											
Vehicle Volumes and Adj	ustme	nts			Majo	r Street: No	rth-South									
Approach		Eastb	ound			West	bound			North	bound			South	bound	
Movement	U	L	т	R	U	L	т	R	U	L	Т	R	U	Ļ	Т	R
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		1	1	0	0	1	1	0	0	1	1	0
Configuration			LTR			L		TR		L		TR		L		TI
Volume (veh/h)		24	33	56		87	30	43		40	573	82		59	485	53
Percent Heavy Vehicles (%)		3	3	3		3	3	3		3				3		
Proportion Time Blocked												1				
Percent Grade (%)			)				0									
Right Turn Channelized																
Median Type   Storage				Undi	vided											
Critical and Follow-up H	eadwa	ys														
Base Critical Headway (sec)	Т	7.1	6.5	6.2		7.1	6.5	6.2		4.1		<u> </u>		4.1		
Critical Headway (sec)	1	7.13	6.53	6.23		7.13	6.53	6.23		4.13				4.13		1
Base Follow-Up Headway (sec)	1	3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)	1	3.53	4.03	3.33		3.53	4.03	3.33		2.23				2.23		
Delay, Queue Length, an	d Leve	of Se	ervice	<u></u>		•								-	-	•
Flow Rate, v (veh/h)			131			101		85		47	[		1	69		1
Capacity, c (veh/h)			121			47		177		951				846		┢
v/c Ratio			1.09	· .		2.17		0.48		0.05				0.08		┢
95% Queue Length, Q <sub>95</sub> (veh)			7.7			10.5		2.3		0.03				0.3		$\vdash$
Control Delay (s/veh)			177.8			726.3		42.7		9.0				9.6		$\vdash$
Level of Service (LOS)			F			, <u>20</u> .5		Ε		э.о., А				A		
Approach Delay (s/veh)		17	7.8	L			4.4				.5	L			.0	L
					E		····			υ.			1			

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HCS TW TWSC Version 7.8 PM Peak SR 52 and Morningside Drive.xtw Generated: 11/23/2020 10:02:14 AM

		ŀ	ICS7	Two	-Way	/ Sto	p-Co	ntro	l Rep	ort						
General Information						I	Site	Infor	matio	n						
Analyst							Inter	section			ſ					
Agency/Co.							Juris	diction								
Date Performed	11/5/	/2020					East/	West Str	eet		Morn	ingside	Drive			
Analysis Year	2020			-			Nort	n/South	Street		Fort !	King Roa	d			
Time Analyzed	AM P	eak					Peak	Hour Fa	ctor		0.68					
Intersection Orientation	Norti	n-South					Analy	/sis Time	Period	(hrs)	0.25					
Project Description	Existi	ng Peak	Season				•									
Lanes																
					<b>们面</b> Majo	a street. No	Alight Strike									
Vehicle Volumes and Adj	justme	nts							-						<u> </u>	
Approach		Eastb	ound			West	bound	-		North	bound		ļ	South	lbound	1
Movement	U	L	Т	R	U	L	Т	R	U	L	Τ	R	U	L	Т	R
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6
Number of Lanes		1	0	1		0	0	0	0	0	1	0	0	0	1	0
Configuration		L		R						LT	<u> </u>					TR
Volume (veh/h)		67		91						105	248				213	60
Percent Heavy Vehicles (%)		3		3						3						
Proportion Time Blocked																
Percent Grade (%)			2													
Right Turn Channelized		N	lo													
Median Type   Storage				Undi	vided											
Critical and Follow-up H	eadwa	ys														
Base Critical Headway (sec)		7.1		6.2	ľ			Γ		4.1			ľ			
Critical Headway (sec)		6.43		6.23						4.13						
Base Follow-Up Headway (sec)		3.5		3.3						2.2						
Follow-Up Headway (sec)		3.53		3,33						2.23						
Delay, Queue Length, an	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)		99		134			[	<b></b>		154	Γ					[
Capacity, c (veh/h)		214		685				[		1152	<b>1</b>	·				-
v/c Ratio		0.46		0.20						0.13						
95% Queue Length, Q <sub>95</sub> (veh)		2.2		0.7		[		Ì		0.5				1	[	1
Control Delay (s/veh)		35.4		11.5		<u>_</u>	[			8.6	1			· ···-		
Level of Service (LOS)		E		В			1			A					1	1
Approach Delay (s/veh)		21	.7	<b>L</b>			E	•		3	.6				•	·
Approach LOS		(	_						i				i — — —			

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HCSTM TWSC Version 7.8 AM peak Fortking and Morningside.xtw Generated: 11/23/2020 10:41:18 AM

		 ]	ICS7	Two	-Way	/ Sto	p-Co	ntro	l Rep	ort						
General Information							Site	Infor	matio	n						
Analyst							Inter	section			Γ					
Agency/Co.							Juris	diction								
Date Performed	11/5	/2020					East/	West Str	eet		Mor	ningside	Drive			
Analysis Year	2020	)					Nort	h/South	Street		Fort	King Roa	d			
Time Analyzed	PM P	Peak					Peak	Hour Fa	ctor		0.87					
Intersection Orientation	Nort	h-South					Anal	sis Time	e Period	(hrs)	0.25					
Project Description	Existi	ing Peak	Season				<b></b>									
Lanes																
					Alajo Majo	r Street No	the South									
Vehicle Volumes and Ad	justme	nts			_											
Approach	_	Easth	bound			West	bound	1	ļ	1	bound	T	<u> </u>	1	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Ť	R	U	L	Τ	R
Priority		10	11	12	ļ	7	8	9	1U	1	2	3	4∪	4	5	6
Number of Lanes		1	0	1	ļ	0	0	0	0	0	1	0	0	0	1	0
Configuration		L		R				ļ	ļ	LT		<u> </u>				TR
Volume (veh/h)		30		128	<b>_</b>		ļ	<u> </u>	<u> </u>	123	198			<u> </u>	264	48
Percent Heavy Vehicles (%)		3		3						3	<u> </u>		<u> </u>		<u> </u>	<u> </u>
Proportion Time Blocked	_								<u> </u>				ļ			[
Percent Grade (%)			0													
Right Turn Channelized		N	10						<u> </u>							
Median Type   Storage				Undi	vided											
<b>Critical and Follow-up H</b>	eadwa	ys														
Base Critical Headway (sec)		7.1		6.2						4.1						
Critical Headway (sec)		6.43		6.23						4.13						
Base Follow-Up Headway (sec)		3.5		3.3						2.2						
Follow-Up Headway (sec)		3.53		3.33						2.23						
Delay, Queue Length, an	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)		34		147					[	141	<u> </u>					
Capacity, c (veh/h)		288		708				·		1195		·			1	İ
v/c Ratio		0.12		0.21						0.12						1
95% Queue Length, Q <sub>95</sub> (veh)		0.4		0.8				<u> </u>		0.4	i					
Control Delay (s/veh)		19.2	<u> </u>	11.4						8.4			1			<u> </u>
Level of Service (LOS)		с		В					ļ	A						1
Approach Delay (s/veh)	1	12	.9					• • • • •		3	.9	1			•	
Approach LOS	1		3													

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02/01/2021
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	1	1		ર્લ	1	7	<b>†</b> Þ		7	<b>†</b> †	7
Traffic Volume (vph)	8	1	6	30	4	36	22	722	20	29	708	21
Future Volume (vph)	8	1	6	30	4	36	22	722	20	29	708	21
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	220		200	0		155	425		0	290		355
Storage Lanes	1		1	0		1	1		0	1	S. States	1
Taper Length (ft)	25			25			50			50		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.95	1.00	0.95	1.00
Frt	1100	1100	0.850		1100	0.850		0.996	0.00		0.00	0.850
Flt Protected	0.950				0.957	N.L. MARKEN	0.950	STAR OF		0.950		
Satd. Flow (prot)	1770	1863	1583	0	1783	1583	1770	3525	0	1770	3539	1583
Flt Permitted	0.733	1000	1000		0.749	1000	0.348	0010		0.326		1000
Satd. Flow (perm)	1365	1863	1583	0	1395	1583	648	3525	0	607	3539	1583
Right Turn on Red	1000	1000	Yes		1000	Yes	010	0020	Yes	001		Yes
Satd. Flow (RTOR)			158			158		3	100			104
Link Speed (mph)		30	100		30	100		50			50	104
Link Distance (ft)		822		S. AND	1313			868			935	
Travel Time (s)		18.7			29.8			11.8			12.8	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	9	1	7	33	4	39	24	785	22	32	770	23
Shared Lane Traffic (%)	3		1	00	т	00	24	700	22	UZ	110	20
Lane Group Flow (vph)	9	1	7	0	37	39	24	807	0	32	770	23
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)	Len	12	night	Len	12	night	Len	12	night	Len	12	night
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane		10			10			10			10	
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
	1.00	1.00	9	1.00	1.00	9	15	1.00	9	1.00	1.00	9
Turning Speed (mph) Number of Detectors	15	2	9	10	2	1	10	2	9	15	2	9
Detector Template	Left	Thru	Right	Left	Thru	Right	Left	Thru		Left	Thru	Right
	20	100	nigrit 20	20	100	night 20	20	100		20	100	night 20
Leading Detector (ft)			and a second second		Contraction of State	COLOR PEOPLE	10 March 10 12 11	The second second	Cores Const			100000000000000000000000000000000000000
Trailing Detector (ft)	0	0	0	0	0	0	0	0		0	0	0
Detector 1 Position(ft)	20	6	0 20	20	0	0 20	20	0 6		20	0 6	0 20
Detector 1 Size(ft)		CI+Ex	CI+Ex	CI+Ex		CI+Ex	CI+Ex	o Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Type	CI+Ex	UI+EX	CI+EX	CI+EX	Cl+Ex	CI+EX	CI+EX	CI+EX		CI+EX	CI+EX	CI+Ex
Detector 1 Channel	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 2 Position(ft)		94			94			94			94	
Detector 2 Size(ft)		6			6			6			6	CONTRACTOR OF THE OWNER
Detector 2 Type		CI+Ex	a cover sea		CI+Ex			Cl+Ex			CI+Ex	
Detector 2 Channel	Service and the service of the servi											
Detector 2 Extend (s)		0.0			0.0	-	MASSIN	0.0	A State	- Internation	0.0	-
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	Perm
Protected Phases		4			8	Charles and	5	2		1	6	
Permitted Phases	4		4	8		8	2			6		6

AM Peak 02/01/2021 Existing Peak Season

Synchro 10 Report Page 1

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Detector Phase	4	4	4	8	8	8	5	2		1	6	f
Switch Phase												
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0		5.0	5.0	5.0
Minimum Split (s)	25.6	25.6	25.6	25.6	25.6	25.6	11.8	24.8		11.8	24.8	24.8
Total Split (s)	40.0	40.0	40.0	40.0	40.0	40.0	20.0	50.0		30.0	60.0	60.0
Total Split (%)	33.3%	33.3%	33.3%	33.3%	33.3%	33.3%	16.7%	41.7%		25.0%	50.0%	50.0%
Maximum Green (s)	32.4	32.4	32.4	32.4	32.4	32.4	13.2	43.2		23.2	53.2	53.2
Yellow Time (s)	4.8	4.8	4.8	4.8	4.8	4.8	4.8	4.8		4.8	4.8	4.8
All-Red Time (s)	2.8	2.8	2.8	2.8	2.8	2.8	2.0	2.0		2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.6	7.6	7.6		7.6	7.6	6.8	6.8		6.8	6.8	6.8
Lead/Lag							Lag	Lead		Lag	Lead	Lead
Lead-Lag Optimize?							Yes	Yes		Yes	Yes	Yes
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0	3.0
Recall Mode	None	None	None	None	None	None	None	Max		None	Max	Max
Walk Time (s)	7.0	7.0	7.0	7.0	7.0	7.0		7.0			7.0	7.0
Flash Dont Walk (s)	11.0	11.0	11.0	11.0	11.0	11.0		11.0			11.0	11.0
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0			0	0
Act Effct Green (s)	7.7	7.7	7.7		7.7	7.7	60.6	57.6		66.0	61.3	61.3
Actuated g/C Ratio	0.09	0.09	0.09		0.09	0.09	0.72	0.69		0.79	0.73	0.73
v/c Ratio	0.07	0.01	0.02		0.29	0.14	0.04	0.33		0.05	0.30	0.02
Control Delay	36.9	36.0	0.2		42.4	1.0	4.3	9.8		3.5	6.6	0.0
Queue Delay	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	36.9	36.0	0.2		42.4	1.0	4.3	9.8		3.5	6.6	0.0
LOS	D	D	А		D	А	А	А		А	А	A
Approach Delay		21.7			21.1			9.6			6.3	
Approach LOS		С			С			А			А	
Intersection Summary							- The lost					
	Other									State State		
Cycle Length: 120												
Actuated Cycle Length: 83.8								Sec. S. M.		State Sta		
Natural Cycle: 65												
Control Type: Actuated-Unco	oordinated											
Maximum v/c Ratio: 0.33												
Intersection Signal Delay: 8.					tersection							
ntersection Capacity Utilizat	ion 47.3%			IC	CU Level o	of Service	A					
Analysis Period (min) 15												
Splits and Phases: 4: Mor	ningside D	rive & US	301									

<b>₫</b> <i>ø</i> 2	Ø1	- <b>-</b> 004	
50 s	30 s	40 s	
<b>↓</b> Ø6		<b>1</b> ø5 <b>♥</b> ø8	
60 s	20	) s 40 s	

02/01/2021

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	٦	1	1		र्स	7	٦	<b>↑</b> ⊅		7	**	7
Traffic Volume (vph)	80	11	30	91	13	90	58	1151	52	92	896	80
Future Volume (vph)	80	11	30	91	13	90	58	1151	52	92	896	80
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	220		200	0		155	425		0	290		355
Storage Lanes	1		1	0		1	1		0	1		1
Taper Length (ft)	25			25			50			50		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.95	1.00	0.95	1.00
Frt			0.850			0.850		0.993				0.850
Flt Protected	0.950		STAR STAR		0.958		0.950			0.950		
Satd. Flow (prot)	1770	1863	1583	0	1785	1583	1770	3514	0	1770	3539	1583
Flt Permitted	0.684	1000	1000		0.744	1000	0.239		SALE OF	0.123		
Satd. Flow (perm)	1274	1863	1583	0	1386	1583	445	3514	0	229	3539	1583
Right Turn on Red		1000	Yes		1000	Yes			Yes	19475555		Yes
Satd. Flow (RTOR)			158			158		4	100			104
Link Speed (mph)		30	100		30	100		50	CENT MARSON		50	101
Link Distance (ft)		822			1313			868			935	
Travel Time (s)		18.7	a to the first		29.8			11.8		121203.0	12.8	91512171
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
	87	12	33	99	14	98	63	1251	57	100	974	87
Adj. Flow (vph)	07	12	00	99	14	90	00	1201	57	100	5/4	07
Shared Lane Traffic (%)	87	12	33	0	113	98	63	1308	0	100	974	87
Lane Group Flow (vph)	87 No	No	No	No	No	90 No	No	No	No	No	974 No	No
Enter Blocked Intersection							Left			Left	Left	
Lane Alignment	Left	Left	Right	Left	Left	Right	Len	Left	Right	Leit	12	Right
Median Width(ft)		12			12			12			0	
Link Offset(ft)		0			0		VIRGINIE	0				
Crosswalk Width(ft)		16			16			16	A CONTRACTOR		16	
Two way Left Turn Lane	1.00	1.00	1.00	1.00	1 00	1 00	1 00	1.00	1 00	1 00	1.00	1.00
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15	-	9	15	-	9	15	0	9	15	-	9
Number of Detectors	1	2	1	1	2	1	1	2		1	2	1
Detector Template	Left	Thru	Right	Left	Thru	Right	Left	Thru		Left	Thru	Right
Leading Detector (ft)	20	100	20	20	100	20	-20	100		20	100	20
Trailing Detector (ft)	0	0	0	0	0	0	0	0		0	0	0
Detector 1 Position(ft)	0	0	0	0	0	0	0	0		0	0	0
Detector 1 Size(ft)	20	6	20	20	6	20	20	6		20	6	20
Detector 1 Type	CI+Ex	CI+Ex	CI+Ex	CI+Ex	Cl+Ex	Cl+Ex	CI+Ex	CI+Ex		CI+Ex	CI+Ex	CI+Ex
Detector 1 Channel												
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0
Detector 2 Position(ft)		94			94		Sec. Sec.	94			94	
Detector 2 Size(ft)		6			6			6			6	
Detector 2 Type		CI+Ex			CI+Ex			CI+Ex			Cl+Ex	
Detector 2 Channel												
Detector 2 Extend (s)		0.0			0.0			0.0			0.0	
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	Perm
Protected Phases		4	3103105		8		5	2		1	6	
Permitted Phases	4		4	8	a strong to all of the	8	2			6		6

PM Peak 11/06/2020 Existing Peak Season

Synchro 10 Report Page 1

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Detector Phase	4	4	4	8	8	8	5	2		1	6	6
Switch Phase												
Minimum Initial (s)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0		5.0	5.0	5.0
Minimum Split (s)	25.6	25.6	25.6	25.6	25.6	25.6	11.8	24.8		11.8	24.8	24.8
Total Split (s)	40.0	40.0	40.0	40.0	40.0	40.0	20.0	50.0		30.0	60.0	60.0
Total Split (%)	33.3%	33.3%	33.3%	33.3%	33.3%	33.3%	16.7%	41.7%		25.0%	50.0%	50.0%
Maximum Green (s)	32.4	32.4	32.4	32.4	32.4	32.4	13.2	43.2		23.2	53.2	53.2
Yellow Time (s)	4.8	4.8	4.8	4.8	4.8	4.8	4.8	4.8		4.8	4.8	4.8
All-Red Time (s)	2.8	2.8	2.8	2.8	2.8	2.8	2.0	2.0		2.0	2.0	2.0
Lost Time Adjust (s)	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Lost Time (s)	7.6	7.6	7.6		7.6	7.6	6.8	6.8		6.8	6.8	6.8
Lead/Lag							Lag	Lead		Lag	Lead	Lead
Lead-Lag Optimize?							Yes	Yes		Yes	Yes	Yes
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0		3.0	3.0	3.0
Recall Mode	None	None	None	None	None	None	None	Max		None	Max	Max
Walk Time (s)	7.0	7.0	7.0	7.0	7.0	7.0		7.0			7.0	7.0
Flash Dont Walk (s)	11.0	11.0	11.0	11.0	11.0	11.0		11.0			11.0	11.0
Pedestrian Calls (#/hr)	0	0	0	0	0	0		0			0	0
Act Effct Green (s)	12.7	12.7	12.7		12.7	12.7	52.2	46.1		64.3	53.7	53.7
Actuated g/C Ratio	0.14	0.14	0.14		0.14	0.14	0.57	0.51		0.71	0.59	0.59
v/c Ratio	0.49	0.05	0.09		0.59	0.27	0.18	0.73		0.25	0.47	0.09
Control Delay	46.7	34.5	0.5		50.0	3.0	8.7	23.6		13.3	12.8	1.9
Queue Delay	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0
Total Delay	46.7	34.5	0.5		50.0	3.0	8.7	23.6		13.3	12.8	1.9
LOS	D	С	А		D	А	А	С		В	В	A
Approach Delay		34.1			28.2			23.0			12.0	
Approach LOS		С			С			С			В	S. Selection
Intersection Summary												
Area Type:	Other											
Cycle Length: 120												
Actuated Cycle Length: 91												
Natural Cycle: 75												
Control Type: Actuated-Ur	ncoordinated											
Maximum v/c Ratio: 0.73												
Intersection Signal Delay:	19.4			In	tersection	LOS: B						
Intersection Capacity Utiliz	zation 68.6%			IC	CU Level of	of Service	С					
Analysis Period (min) 15												
0 10 10			0.0.1									

### Splits and Phases: 4: Morningside Drive & US 301

↑ø2	▶ <sub>Ø1</sub>	
50 s	30 s	40 s
<b>↓</b> Ø6	<b>1</b> ø5	<b>◆</b> Ø8
60 s	20 s	40 s

02/01/2021

# APPENDIX - E

1



FDOT GENERALIZED CAPACITY TABLES



# Generalized **Peak Hour Two-Way** Volumes for Florida's Urbanized Areas<sup>1</sup>

2020

					Urbar	nized Are	as'			January 202
and the second	INTERF	RUPTED F	LOW FAC	ILITIES			UNINTER	RUPTED FLO	W FACILITIE	
	STATE S	IGNALI	ZED ART	FERIAL	S			FREEWA	YS	
	Class I (40 r	nph or hig	ther posted	speed lim	it)			Core Urbani	ized	
Lanes	Median	B	Ċ	D	E	Lanes	В	С	D	Е
2	Undivided	*	1,510	1,600	**	4	4,050	5,640	6,800	7,420
4	Divided	*	3,420	3,580	**	6	5,960	8,310	10,220	11,150
6	Divided	*	5,250	5,390	**	8	7,840	10,960	13,620	14,850
8	Divided	*	7,090	7,210	**	10	9,800	13,510	17,040	18,580
	Close II (25	mmh or ala	war postod	anood line	.;+)	12	11,600	16,350	20,930	23,200
Lanes	Class II (35 n Median	B	C	D D	E E			Urbanize	Ч	
	Undivided	*	660	1,330	1,410	Lanes	В	C	D	Е
2	Divided	*	1,310	2,920	3,040	Lanes 4	4,130	5,640	7,070	7,690
4	Divided	*	2,090	4,500	4,590	6	6,200	8,450	10,510	11,530
6		*					8,270	11,270	13,960	15,380
0	Divided		2,880	6,060	6,130	8 10	10,350	14,110	17,310	19,220
						10	10,350	14,110	17,310	19,220
	Non-State Si	gnalized	Roadway	Adjustme	nts		F	reeway Adjus	tments	
	(Alte	r correspond	ing state volu				Auxiliary Land		Ramp	
			ted percent.)	100/		Pres	ent in Both Dire		Meterin	
	Non-State	Signalized	Roadways	- 10%			+1,800		+ 5%	
	Median		ane Adju			Ι.		UPTED FLO		AVC
		Exclusive			djustment					
Lanes	Median	Left Lane	-		Factors	Lanes	Median	B		E
2	Divided	Yes	N		+5%	2	Undivided		520 2,180	
2 Multi	Undivided Undivided	No Yes	N N		-20% -5%	4	Divided		730 5,960	
Multi	Undivided	No	N		-25%	6	Divided	4,910 7,0	90 8,950	10,180
_		_	Ye		+ 5%		Uninterrunt	ed Flow High	way Adjustm	onte
						Lanes	Median	Exclusive left		tment factors
			ity Adjust			2	Divided	Yes	inites riajus	+5%
			nding two-di			Multi	Undivided	Yes		-5%
	vo	lumes in thi	is table by 0.0	5		Multi	Undivided	No		-25%
	1	BICYCL	E MODE <sup>2</sup>			<sup>1</sup> Values s	shown are presented	as peak hour direction	onal volumes for lev	els of service and
			nes shown be	low by numb	erof	are for th	e automobile/truck	modes unless specific	cally stated. This tab	le does not
9	directional roadw	ay lanes to d	letermine two	-way maxim	um service			uld be used only for this table is derived		
		volu	nes.)			planning	applications. The ta	ble and deriving com	puter models should	not be used for
	Paved							n, where more refine ns of the HCM and th		
Shoul	der/Bicycle					Service M		is of the frew and t	te Transit Capacity i	ind Quanty of
Lane	coverage	В	С	D	E			cle and pedestrian m ber of bicyclists or pe		
	0-49%	*	260	680	1,770	1.1.2.3.19.0.5				Market Street
5	0-84%	190	600	1,770	>1,770	Contract Contractory of the	er hour shown are onl	y for the peak hour in	the single direction of	the higher traffic
8:	5-100%	830	1,700	>1,770	**	flow.				
	PE	DESTRI	AN MODE	22		* Cannot	be achieved using t	able input value defa	ults.	
(M	ultiply vehicle vo							el of service letter gr		
	ctional roadway l				service			service D become F mode, the level of se		
		volur	nes.)			achievabl	le because there is n	o maximum vehicle		
Sidewa	alk Coverage	В	С	D	E	value def	aults.			
	)-49%	*	*	250	850	Source:				
	0-84%	*	150	780	1,420		Department of Transp Implementation Offi			
[	5-100%	340	960	1,560	>1,770	https://ww	ww.fdot.gov/plannin	g/systems/		
	BUS MOD									
			r in peak direc			No. 13				
Sidewa	lk Coverage	В	C	D	E					
	)-84%	> 5	≥4	≥ 3	≥2					
	5-100%	> 4	$\geq 3$	$\geq 2$	$\geq 1$	an in the				
<u> </u>	20070			_ ~	- •	Prostant Contractor			ACTIVITY OF A DECK	A CONTRACTOR OF A CONTRACTOR

### TABLE 4 (continued)

## Generalized Peak Hour Two-Way Volumes for Florida's

Urbanized Areas

	Unir	terrupted	Flow Faci	lities				Flow Facil	Flow Facilities		
INPUT VALUE ASSUMPTIONS	Freeways	Core	High		Cla	State A	Arterials	ass II	Bicycle	ass I Pedestria	
		Freeways	, ingit								
ROADWAY CHARACTERISTICS					<b>_</b>						
Area type (urban, rural)	urban	urban									
Number of through lanes (both dir.)	4-10	4-12	2	4-6	2	4-8	2	4-8	4	4	
Posted speed (mph)	70	65	50	50	45	50	30	30	45	45	
Free flow speed (mph)	75	70	55	55	50	55	35	35	50	50	
Auxiliary Lanes (n,y)	n	n									
Median (d, twlt, n, nr, r)				d	n	r	n	r	r	r	
Terrain (1,r)	1	1	1	1	1	1	1	1	1	1	
% no passing zone			80								
Exclusive left turn lane impact (n, y)			[n]	У	у	у	У	у	у	у	
Exclusive right turn lanes (n, y)					n	n	n	n	n	n	
Facility length (mi)	3	3	5	5	2	2	1.9	1.8	2	2	
TRAFFIC CHARACTERISTICS											
Planning analysis hour factor (K)	0.090	0.085	0.090	0.090	0.090	0.090	0.090	0.090	0.090	0.090	
Directional distribution factor (D)	0.55	0.55	0.55	0.55	0.550	0.560	0.565	0.560	0.565	0.565	
Peak hour factor (PHF)	0.95	0.95	0.95	0.95	1.000	1.000	1.000	1.000	1.000	1.000	
Base saturation flow rate (pcphpl)	2,400	2,400	1,700	2,200	1,950	1,950	1,950	1,950	1,950	1,950	
Heavy vehicle percent	4.0	4.0	2.0	2.0	1.0	1.0	1.0	1.0	2.5	2.0	
Speed Adjustment Factor (SAF)	0.975	0.975		0.975							
Capacity Adjustment Factor (CAF)	0.968	0.968		0.968							
% left turns	01200				12	12	12	12	12	12	
% right turns					12	12	12	12	12	12	
CONTROL CHARACTERISTICS										-	
Number of signals	1	1			4	4	10	10	4	6	
Arrival type (1-6)					3	3	4	4	4	4	
					c	C	c +	c +	c +	c +	
Signal type (a, c, p)					120	150	120	120	120	120	
Cycle length (C)					0.44	0.45	0.44	0.44	0.44	0.44	
Effective green ratio (g/C)					0.44	0.45	0.44	0.44	0.44	0.44	
MULTIMODAL CHARACTERIST	ICS										
Paved shoulder/bicycle lane (n, y)									n, 50%, y		
Outside lane width (n, t, w)									t	t	
Pavement condition (d, t, u)									t		
On-street parking (n, y)											
Sidewalk (n, y)										n, 50%,	
Sidewalk/roadway separation(a, t, w)										t	
Sidewalk protective barrier (n, y)										n	
		LEVEL	OF SERV	ICE THR	ESHOLD	S					
	Freeways	High	ways		Arte	rials		Bicycle	Ped	Bus	
Level of		Two-Lane		Cla	ss I	Clas	ss II				
Service	Density	%ffs	Density					Score	Score	Buses/h	
P	< 17	> 83.3			ats ats 1 mph > 22 mph		≤ 2.75	< 2.75	66		
B	≤ 17		≤ 17 < 24				-		$\leq 2.75$	$\leq 6$	
<u> </u>	≤ 24	> 75.0	≤ 24		23 mph > 17 mph		≤ 3.50	≤ 3.50	$\leq 4$		
D	≤ 31	> 66.7	≤ 31		18 mph > 13 mph		≤ 4.25	≤ 4.25	< 3		
E	≤ <b>3</b> 9	> 58.3	≤ 35	> 15	mph > 10 mph		mph	$\leq 5.00$	$\leq 5.00$	< 2	

% ffs = Percent free flow speed ats = Average travel speed

APPENDIX - F

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2045 MODEL ADJUSTMENTS



# ADopted LRTP

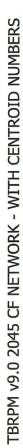
# Morningside Route Study Socioeconomic Data

Zone	Dwelling Units	Population	Industrial Employees	Commercial Employees	Service Employees	Total Employees	K-12 Students	College Students
2172	787	2052	117	24	39	180	0	0
2176	105	247	10	18	2	30	0	0
2177	635	1176	28	4	166	198	0	0
2178	134	271	8	2	117	127	0	0
2263	21	41	4	0	482	486	0	8342
2265	355	826	16	107	190	313	0	0
2356	686	1742	15	191	70	276	1365	0
2357	411	941	8	127	7	142	0	0
2358	505	1024	20	10	27	57	0	0
2359	612	1371	134	263	197	594	0	0
2361	755	1757	31	62	11	104	0	0
2362	871	2600	24	183	345	552	442	0
2363	845	1773	41	319	664	1024	0	0
2388	576	1484	152	36	61	249	0	0
2389	126	269	19	3	6	28	0	0
2390	276	810	16	5	100	121	0	1566
2391	315	887	165	18	76	259	0	0
2392	547	1325	1101	152	863	2116	0	0
2393	394	1232	31	30	49	110	0	0
2394	5	10	113	0	117	230	0	0
2395	909	2153	133	0	67	200	0	0
2396	870	2367	4	7	118	129	0	0
2397	483	796	49	169	593	811	487	0
2398	13	18	15	111	1052	1178	0	0
2399	194	469	18	11	124	153	142	0
2400	909	1972	24	36	509	569	0	0
2400	204	461	8	12	215	235	0	0
2401	617	1256	33	93	756	882	1594	0
2403	196	447	37	59	601	697	0	0
2403	623	1525	73	4	225	302	3033	197
2404	271	549	87	243	712	1042	0	0
2405	390	961	26	6	167	199	0	0
2400	307	573	53	318	130	501	0	0
2407	616	772	73	670	389	1132	0	0
2408	297	715	19	0	6	25	0	0
2409	10	23	15	0	0	15	0	0
2410	31	50	21	0	9	30	0	0
There are	976	1498	31	2	34	67	0	0
2412	11	37	108	2	0	108	0	0
2413	27	69	108	10	12	108	0	0
2414						340	1339	0
2416	684 1512	1523 3255	38 91	12 16	290 61	168	0	0

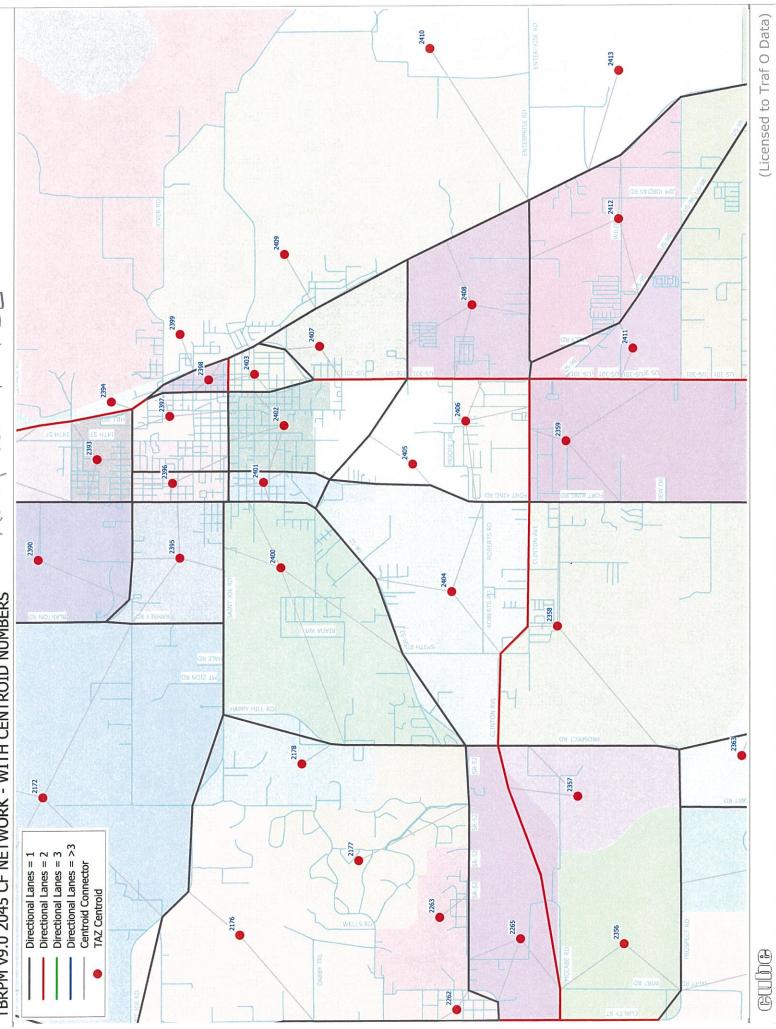
# PROPOSED CHANGES

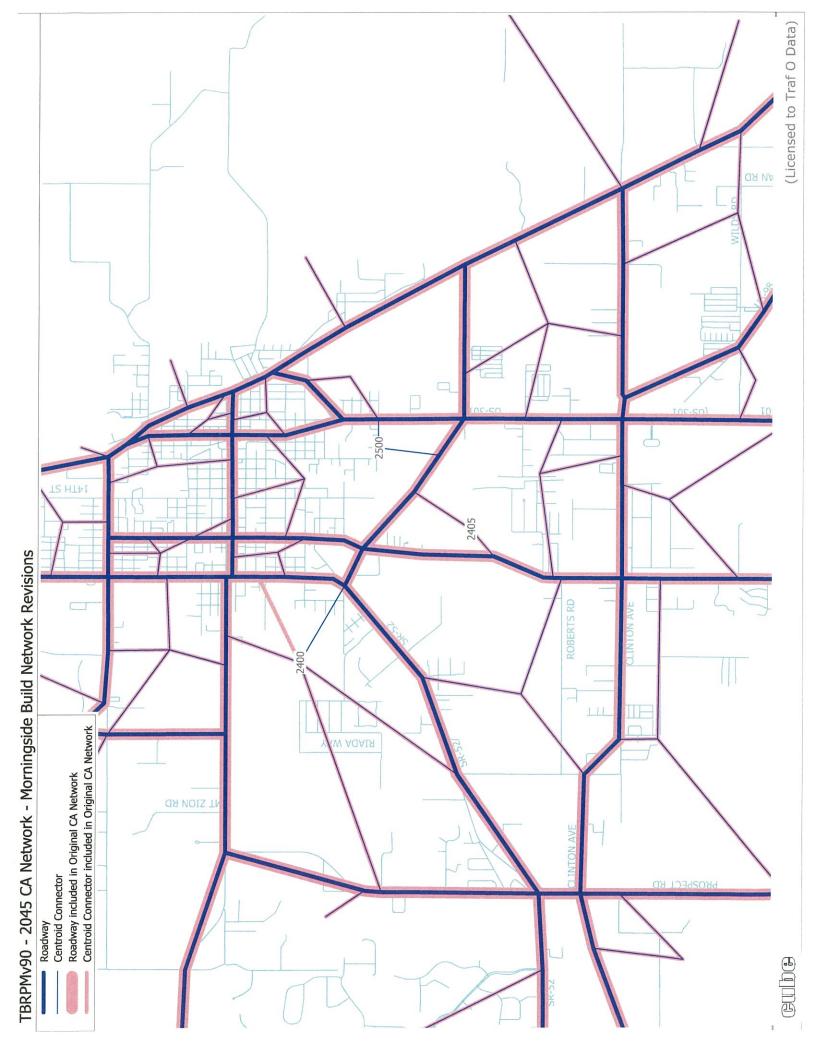
#### Morningside Route Study 2045 Socioeconomic Data

Zone	Dwelling	Population	Industrial	Commercial	Service	Total	K-12	College
Zone	Units	ropulation	Employees	Employees	Employees	Employees	Students	Students
2172	787	2052	117	24	39	180	0	0
2176	105	247	10	18	2	30	D	0
2177	635	1176	28	4	166	198	0	0
2178	134	271	8	2	117	127	0	0
2263	21	41	4	0	482	486	0	8342
2265	355	826	16	107	190	313	0	0
2356	686	1742	15	191	70	276	1365	0
2357	411	941	8	127	7	142	0	0
2358	505	1024	20	10	27	57	0	0
2359	612	1371	134	263	197	594	0	0
2361	755	1757	31	62	11	104	0	0
2362	871	2600	24	183	345	552	442	0
2363	845	1773	41	319	664	1024	0	0
2388	576	1484	152	36	61	249	0	0
2389	126	269	19	3	6	28	0	0
2390	276	810	16	5	100	121	0	1566
2391	315	887	165	18	76	259	0	0
2392	547	1325	1101	152	863	2116	0	0
2393	394	1232	31	30	49	110	0	0
2394	5	10	113	0	117	230	0	0
2395	909	2153	133	0	67	200	0	0
2396	870	2367	4	7	118	129	0	0
2397	483	796	49	169	593	811	487	0
2398	13	18	15	111	1052	1178	0	0
2399	194	469	18	11	124	153	142	0
2400	909	1972	24	36	509	569	0	0
2401	204	461	8	12	215	235	0	0
2402	617	1256	33	93	756	882	1594	0
2403	196	447	37	59	601	697	0	0
2404	623	1525	73	4	225	302	3033	197
2405	201	468	0	0	0	0	0	0
2406	390	961	26	6	167	199	0	0
2407	307	573	53	318	130	501	0	0
2408	616	772	73	670	389	1132	0	0
2409	297	715	19	0	6	25	0	0
2410	10	23	15	0	0	15	0	0
2411	31	50	21	0	9	30	0	0
2412	976	1498	31	2	34	67	0	0
2413	11	37	108	0	0	108	0	0
2414	27	69	107	10	12	129	0	0
2416	684	1523	38	12	290	340	1339	0
2417	1512	3255	91	16	61	168	0	0
2500	250	581	87	243	712	1042	0	0



ALOPTED NODEL

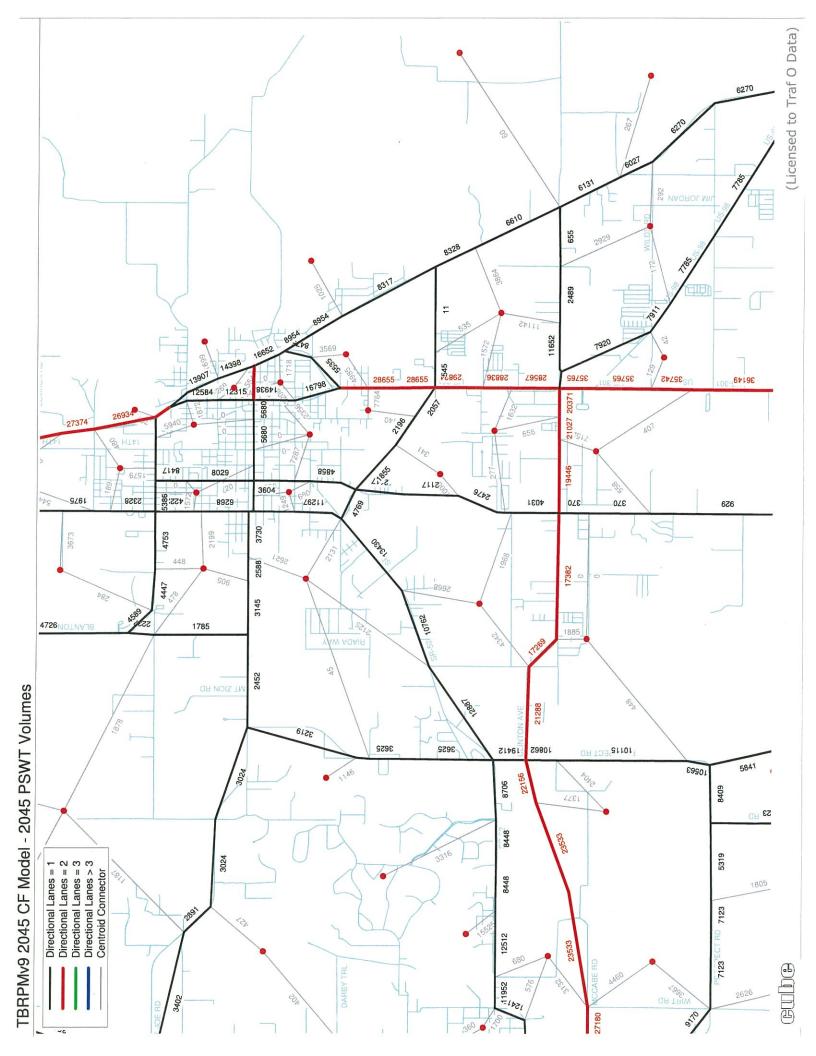




2045 MODEL VOLUMES

(WITH MORNINGSIDE EXTENSION)

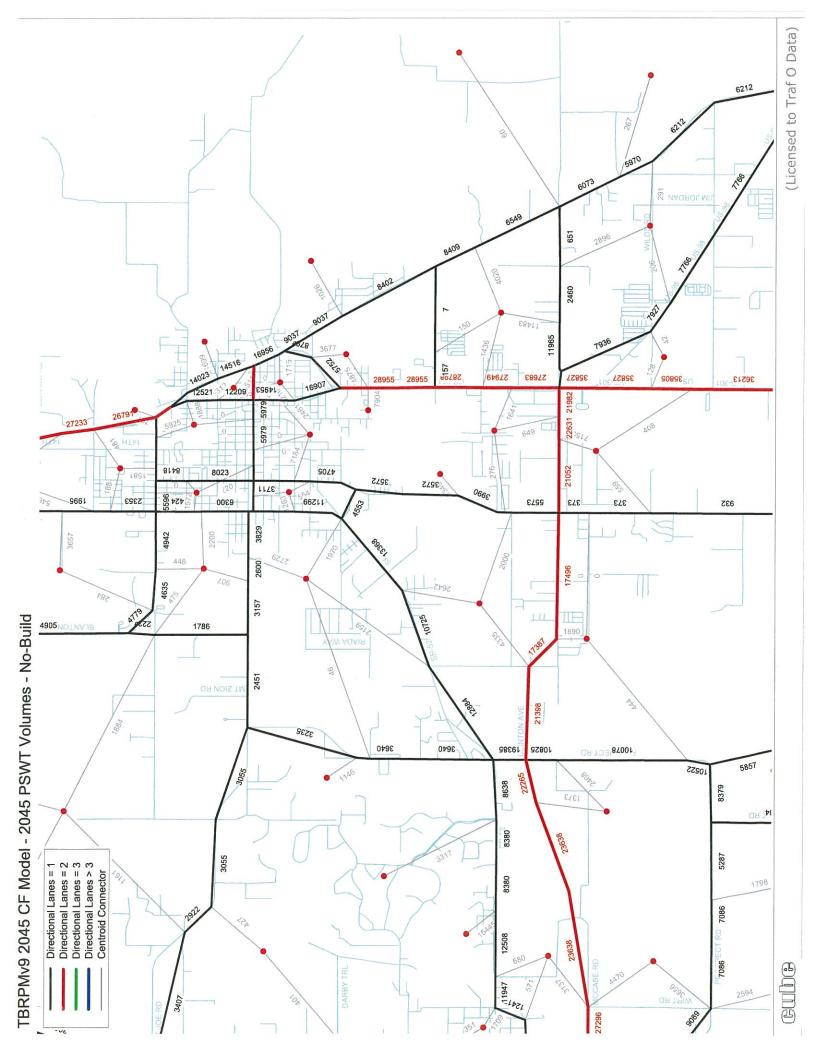




2045 MODEL VOLUMES

(WITHOUT MORNINGSIDE EXTENSION)

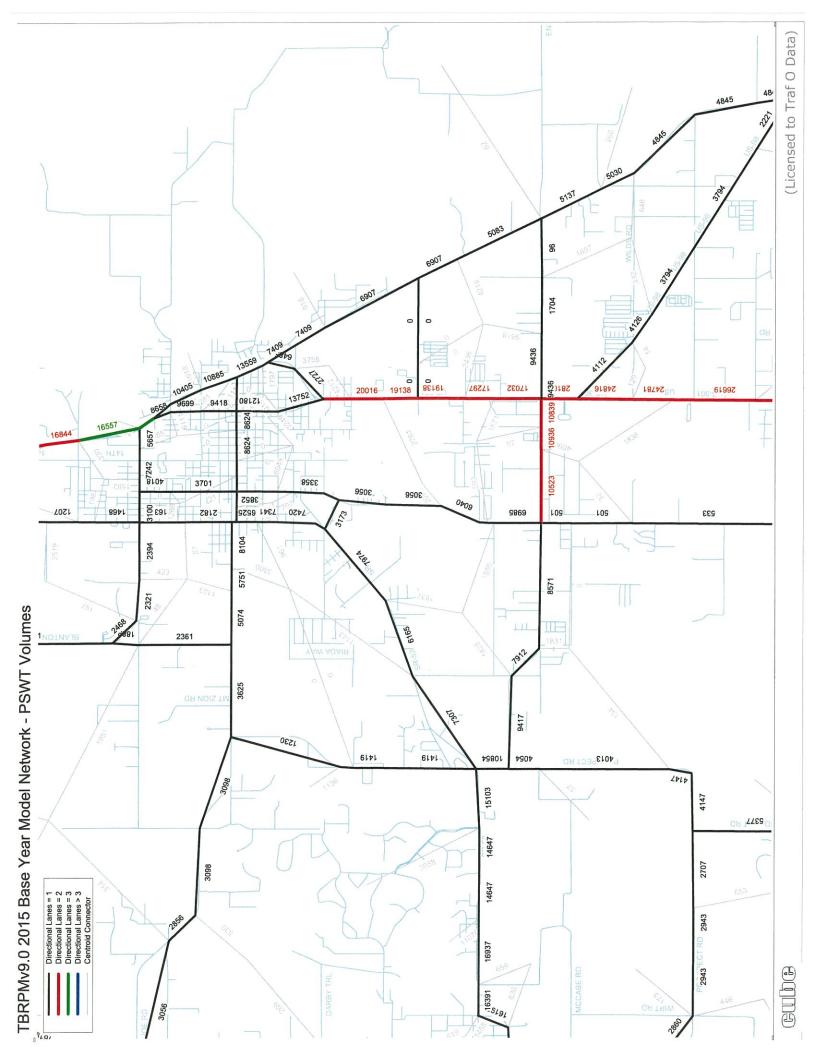




2015 MODEL VOLUMES

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MODEL CORRECTION FACTOR



2019 PEAK SEASON FACTOR CATEGORY REPORT - REPORT TYPE: ALL

CATEGO	DRY: 1400 PASCO COUNTYWIDE		
WEEK	DATES	SF	MOCF: 0.95 PSCF
* * * * * * * * * * * * * * * * * * *	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{c} 0.98\\ 1.03\\ 1.01\\ 1.00\\ 9.97\\ 0.998\\ 0.998\\ $	$     \begin{array}{c}       1.03 \\       1.05 \\       1.08 \\       1.06 \\       1.05 \\       1.03 \\       1.02 \\       1.01 \\       1.00 \\       0.99 \\       0.98 \\       0.99 \\       0.99 \\       0.99 \\       1.00 \\       1.01 \\       1.02 \\       1.03 \\       1.04 \\       1.06 \\       1.06 \\       1.06 \\       1.06 \\       1.06 \\       1.06 \\       1.07 \\       1.08 \\       1.08 \\       1.09 \\       1.09 \\       1.09 \\       1.09 \\       1.09 \\       1.09 \\       1.11 \\       1.11 \\       1.12 \\       1.12 \\       1.13 \\       1.13 \\       1.13 \\       1.14 \\       1.12 \\       1.13 \\       1.13 \\       1.14 \\       1.12 \\       1.13 \\       1.13 \\       1.14 \\       1.12 \\       1.13 \\       1.06 \\       1.05 \\       1.05 \\       1.05 \\       1.03 \\       1.03 \\       1.03 \\       1.03 \\       1.03 \\       1.03 \\       1.03 \\       1.03 \\       1.05 \\       1.08        $

\* PEAK SEASON

14-FEB-2020 15:39:31

830UPD 7\_1400\_PKSEASON.TXT

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APPENDIX - G



LINCKS & ASSOCIATES, INC.

INTERSECTION ANALYSIS

(2045)



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		ŀ	ICS7	Two	-Way	y Sto	p-Cc	ontro	l Rep	ort						
General Information							Site	Infor	matio	n						
Analyst							Intersection									
Agency/Co.							Juris	diction								
Date Performed	11/5	/2020					East/	West Str	eet		Morr	ningside	Drive/A	dair		
Analysis Year	2020	l					Nort	h/South	Street		SR 52	2				
Time Analyzed	AM F	Peak- Op	otion A				Peak	Peak Hour Factor 0.92								
Intersection Orientation	Nort	North-South							Period	(hrs)	0.25					
Project Description	2045	2045 Traffic														
Lanes																
				ojrekterkusta. Lizerterus		1 L										
Vehicle Volumes and Ad	justme	nts														
Approach		Easti	bound			West	bound			North	nbound			South	ibound	
Movement	U	L	Т	R	U	L	Т	R	υ	L	Т	R	υ	L	Т	R
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		1	1	0	0	1	1	0	0	1	1	0
Configuration			LTR			L		TR		L		TR		L		TR
Volume (veh/h)		44	49	60		92	13	116		32	473	80		67	537	24
Percent Heavy Vehicles (%)		3	3	3		3	3	3		3	ļ			3	<u> </u>	
Proportion Time Blocked																
Percent Grade (%)			0				0									
Right Turn Channelized																
Median Type   Storage				Undi	vided									<u>.</u>		
<b>Critical and Follow-up H</b>	eadwa	ys														
Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.13	6.53	6.23		7.13	6.53	6.23		4.13				4.13		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2,2				2.2		
Follow-Up Headway (sec)		3.53	4.03	3.33		3.53	4.03	3.33		2.23				2.23		
Delay, Queue Length, an	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)			166			100		140		35				73		
Capacity, c (veh/h)			134			59	1	401		964				971		1
v/c Ratio			1.25			1.69		0.35		0.04				0.07		
95% Queue Length, Q <sub>95</sub> (veh)			10.2			9.2		1.5		0.1				0.2		
Control Delay (s/veh)			221.9			484.4		18.7		8.9				9.0		
Level of Service (LOS)			۶			F		с		Α				A	<u> </u>	
Approach Delay (s/veh)			21	212.6 0.				.5			1	.0				
Approach LOS		F					F									

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HCS TW TWSC Version 7.8 AM Peak SR 52 and Morningside(2045).xtw Generated: 1/26/2021 1:57:26 PM

General Information							Site	Infor	matio	n						
Analyst							Inter	section						(		
Agency/Co.							Juris	diction								
Date Performed	11/5/	/2020					East/	West Str	eet		Morr	ningside	Drive/A	dair		
Analysis Year	2020						Nort	h/South	Street		SR 52	2				
Time Analyzed	PM P	eak-Opt	ion A				Peak	Hour Fa	ctor		0.92					
Intersection Orientation	Norti	h-South					Anal	ysis Time	Period	(hrs)	0,25					
Project Description	2045	Traffic														
Lanes																
	-			in an	(A) A) Majo	1 F	the South									
Vehicle Volumes and Ad	justme	nts														
Approach		Eastb	ound			West	bound		ļ	North	bound			South	bound	<u> </u>
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	10	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		1	1	0	0	1	1	0	0	1	1	0
Configuration			LTR			L		TR		L	·	TR		L		TF
Volume (veh/h)		33	45	77		120	41	59		55	786	112		81	665	73
Percent Heavy Vehicles (%)		3	3	3		3	3	3		3				3		
Proportion Time Blocked																
Percent Grade (%)		1	0				0									
Right Turn Channelized																
Median Type   Storage				Undi	vided											
Critical and Follow-up H	eadway	ys														
Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.13	6.53	6.23		7.13	6.53	6.23		4.13				4.13		
Base Follow-Up Headway (sec)		3.5	4.0	3,3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.53	4.03	3.33		3.53	4.03	3.33		2.23				2.23		
Delay, Queue Length, an	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)			168			130		109		60				88		1
Capacity, c (veh/h)			20					96		817				703		$\square$
v/c Ratio			8.48					1.14		0.07				0.13		<u> </u>
95% Queue Length, Q <sub>95</sub> (veh)			21.5					7.3		0.2				0.4		1
Control Delay (s/veh)			3745.2					215.4		9.8				10.9		<u>†                                    </u>
Level of Service (LOS)			F					F		A				В		<u> </u>
																1
Approach Delay (s/veh)		374	5,2							0.	.6			1	.1	

Lanes, Volumes, Timings 3: SR 52/Morningside Dr & Adair Rd

01/26/2021

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4		٦	ĥ		٦	ĵ.		٦	¢Î,	
Traffic Volume (vph)	44	49	60	92	13	116	32	473	80	67	537	24
Future Volume (vph)	44	49	60	92	13	116	32	473	80	67	537	24
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	0		0	185		0	185		0	212		0
Storage Lanes	0		0	1		0	1		0	1		0
Taper Length (ft)	25			50			50			50		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.947			0.865			0.978			0.994	
Flt Protected		0.986	1888 (A.2.	0.950			0.950			0.950		
Satd. Flow (prot)	0	1739	0	1770	1611	0	1770	1822	0	1770	1852	0
Flt Permitted	an wat	0.858		0.596	<b>NEW STREET</b>		0.379		TAX OF ST	0.384	Sol And	000500
Satd. Flow (perm)	0	1514	0	1110	1611	0	706	1822	0	715	1852	0
Right Turn on Red		1011	Yes	1110	1011	Yes	100	TOLL	Yes		1002	Yes
Satd. Flow (RTOR)		47	100		126	100		21	100		5	100
Link Speed (mph)		30	1034630423		30		1.1.1.1.1.1.1	30			30	
Link Distance (ft)		866			1084			642			581	
Travel Time (s)		19.7	10 X 202 19		24.6	anna ann		14.6	S. LANGER		13.2	00000000
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	48	53	65	100	14	126	35	514	87	73	584	26
Shared Lane Traffic (%)	40	55	05	100	14	120	00	514	07	10	504	20
	0	166	0	100	140	0	35	601	0	73	610	0
Lane Group Flow (vph) Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
	Left	Left		Left	Left		Left	Left		Left	Left	
Lane Alignment	Len	12	Right	Leit		Right	Leit	12	Right	Len		Right
Median Width(ft)		0			12 0			0			12 0	
Link Offset(ft)		16			16			16			16	
Crosswalk Width(ft)		10			10			10			10	
Two way Left Turn Lane	1 00	1 00	1 00	1.00	1.00	1.00	1 00	1 00	1.00	1 00	1 00	1.00
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15	-	9	15	0	9	15	0	9	15	0	9
Number of Detectors	1	2		1	2		1	2	Carl Section 199	1	2	es acesare
Detector Template	Left	Thru		Left	Thru		Left	Thru		Left	Thru	
Leading Detector (ft)	20	100		20	100		20	100		20	100	
Trailing Detector (ft)	0	0		0	0		0	0		0	0	
Detector 1 Position(ft)	0	0		0	0		0	0		0	0	
Detector 1 Size(ft)	20	6		20	6	al and a second	20	6		20	6	
Detector 1 Type	Cl+Ex	CI+Ex		CI+Ex	CI+Ex		Cl+Ex	Cl+Ex		CI+Ex	CI+Ex	
Detector 1 Channel					Statistics Statistics							
Detector 1 Extend (s)	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Detector 2 Position(ft)		94			94			94			94	States of
Detector 2 Size(ft)		6			6			6	Charles States and		6	Concernation of the local distance of the lo
Detector 2 Type		Cl+Ex			CI+Ex			Cl+Ex			CI+Ex	
Detector 2 Channel												
Detector 2 Extend (s)		0.0			0.0			0.0			0.0	
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		4			8			2			6	
Permitted Phases	4			8			2			6		

Signalized-Option B 11/20/2020 AM Peak Hour -2045 Traffic

Synchro 10 Report Page 1

# Lanes, Volumes, Timings 3: SR 52/Morningside Dr & Adair Rd

01/	26/2	021

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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Detector Phase	4	4		8	8		2	2		6	6	
Switch Phase												
Minimum Initial (s)	5.0	5.0		5.0	5.0		5.0	5.0		5.0	5.0	
Minimum Split (s)	22.5	22.5		22.5	22.5		22.5	22.5		22.5	22.5	
Total Split (s)	25.0	25.0		25.0	25.0		45.0	45.0		45.0	45.0	
Total Split (%)	35.7%	35.7%		35.7%	35.7%		64.3%	64.3%		64.3%	64.3%	
Maximum Green (s)	20.5	20.5		20.5	20.5		40.5	40.5		40.5	40.5	
Yellow Time (s)	3.5	3.5		3.5	3.5		3.5	3.5		3.5	3.5	
All-Red Time (s)	1.0	1.0		1.0	1.0		1.0	1.0		1.0	1.0	
Lost Time Adjust (s)		0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Total Lost Time (s)		4.5		4.5	4.5		4.5	4.5		4.5	4.5	
Lead/Lag												
Lead-Lag Optimize?												
Vehicle Extension (s)	3.0	3.0		3.0	3.0		3.0	3.0		3.0	3.0	
Recall Mode	None	None		None	None		Max	Max		Max	Max	
Walk Time (s)	7.0	7.0		7.0	7.0		7.0	7.0		7.0	7.0	
Flash Dont Walk (s)	11.0	11.0		11.0	11.0		11.0	11.0		11.0	11.0	
Pedestrian Calls (#/hr)	0	0		0	0		0	0		0	0	
Act Effct Green (s)		10.5		10.5	10.5		43.4	43.4		43.4	43.4	
Actuated g/C Ratio		0.17		0.17	0.17		0.69	0.69		0.69	0.69	
v/c Ratio		0.57		0.54	0.38		0.07	0.48		0.15	0.48	
Control Delay		24.0		33.8	8.8		4.7	6.5		5.2	6.7	
Queue Delay		0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Total Delay		24.0		33.8	8.8		4.7	6.5		5.2	6.7	
LOS		С		С	А		А	А		А	Α	
Approach Delay		24.0			19.2			6.4			6.5	
Approach LOS		С			В			А			А	
Intersection Summary		-				C. Second		a the second				Selection of the
Area Type:	Other											
Cycle Length: 70												
Actuated Cycle Length: 62	.9											
Natural Cycle: 55												
Control Type: Actuated-Un	ncoordinated											
Maximum v/c Ratio: 0.57												
Intersection Signal Delay:	9.9				tersection							
Intersection Capacity Utiliz	ation 65.4%			IC	CU Level o	f Service	С					
Analysis Period (min) 15												
Splits and Phases: 3: SF	R 52/Morning	side Dr &	Adair Ro	4								
		,					1.4					

45 s	25 s
<b>↓</b> ø6	₹_Ø8
45 s	25 s

Movement	EB	WB	WB	NB	NB	SB	SB
Directions Served	LTR	L	TR	L	TR	L	TR
Maximum Queue (ft)	127	88	77	67	173	60	171
Average Queue (ft)	69	54	48	26	101	33	105
95th Queue (ft)	124	91	85	77	177	66	178
Link Distance (ft)	832		1050		608		547
Upstream Blk Time (%)							
Queuing Penalty (veh)							
Storage Bay Dist (ft)		185		185		212	
Storage Blk Time (%)					0		0
Queuing Penalty (veh)					0		0

### Network Summary

Network wide Queuing Penalty: 0

# Lanes, Volumes, Timings 3: SR 52/Morningside Dr & Adair Rd

01/26/2021	
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	LUL	4	LDIT	T T	1	WDIT	٦ ۲	1	NUT	5	1	ODIT
Traffic Volume (vph)	33	45	77	120	41	59	55	786	112	81	665	73
Future Volume (vph)	33	45	77	120	41	59	55	786	112	81	665	73
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Storage Length (ft)	1900	1900	0	185	1900	0	185	1900	0	212	1900	1900
Storage Lanes	0		0	105		0	105		0	1		0
	25		U	50		0	50		0	50		U
Taper Length (ft)		1 00	1 00		1 00	1 00		1 00	1 00		1 00	1 00
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.933		0.050	0.912		0.050	0.981	0101010000	0.050	0.985	CALCULAR DE LA
Flt Protected	•	0.989	0	0.950	1000	•	0.950	1007	-	0.950	1005	-
Satd. Flow (prot)	0	1719	0	1770	1699	0	1770	1827	0	1770	1835	0
Flt Permitted		0.912		0.577			0.262			0.167		
Satd. Flow (perm)	0	1585	0	1075	1699	0	488	1827	0	311	1835	0
Right Turn on Red		E CONTRA	Yes			Yes			Yes	The Palati		Yes
Satd. Flow (RTOR)		68			64			19		okur oktore o	15	
Link Speed (mph)		30			30			30			30	
Link Distance (ft)		866			1084			642			581	
Travel Time (s)		19.7			24.6			14.6			13.2	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	36	49	84	130	45	64	60	854	122	88	723	79
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	169	0	130	109	0	60	976	0	88	802	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		12			12			12			12	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Number of Detectors	1	2		1	2		1	2		1	2	
Detector Template	Left	Thru		Left	Thru		Left	Thru		Left	Thru	
Leading Detector (ft)	20	100		20	100		20	100		20	100	
Trailing Detector (ft)	0	0		0	0		0	0		0	0	
Detector 1 Position(ft)	0	0		0	0		0	0		0	0	
Detector 1 Size(ft)	20	6		20	6		20	6		20	6	Sec. 1
Detector 1 Type	CI+Ex	CI+Ex		CI+Ex	CI+Ex		CI+Ex	CI+Ex		CI+Ex	CI+Ex	
Detector 1 Channel	OTTEX	OTTEX		OTTEX	OTTEX		OTEX	OTTEX		OTTEX	OTTEX	
Detector 1 Extend (s)	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Queue (s)	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	(Constant)
And the second	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Detector 1 Delay (s)	0.0	94		0.0	94		0.0	94		0.0	94	
Detector 2 Position(ft)					94			94 6				
Detector 2 Size(ft)		6 CLIEV							Contraction of		6 CLEV	
Detector 2 Type		CI+Ex			CI+Ex	The State Reads		CI+Ex	NO SALAN		CI+Ex	al state of
Detector 2 Channel		0.0			0.0		an gine soon	0.0			0.0	CONSURA.
Detector 2 Extend (s)	P	0.0		D	0.0		D	0.0		D	0.0	
Turn Type	Perm	NA		Perm	NA		Perm	NA		Perm	NA	
Protected Phases		4			8			2			6	
Permitted Phases	4			8			2			6		

Signalized-Option B 11/20/2020 PM Peak Hour -2045 Traffic

Synchro 10 Report Page 1

# Lanes, Volumes, Timings 3: SR 52/Morningside Dr & Adair Rd

01/20/2021	01	/26/2021	
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Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Detector Phase	4	4		8	8		2	2		6	6	
Switch Phase												
Minimum Initial (s)	5.0	5.0		5.0	5.0		5.0	5.0		5.0	5.0	
Minimum Split (s)	22.5	22.5		22.5	22.5		22.5	22.5		22.5	22.5	
Total Split (s)	22.5	22.5		22.5	22.5		47.5	47.5		47.5	47.5	
Total Split (%)	32.1%	32.1%		32.1%	32.1%		67.9%	67.9%		67.9%	67.9%	
Maximum Green (s)	18.0	18.0		18.0	18.0		43.0	43.0		43.0	43.0	
Yellow Time (s)	3.5	3.5		3.5	3.5		3.5	3.5		3.5	3.5	
All-Red Time (s)	1.0	1.0		1.0	1.0		1.0	1.0		1.0	1.0	
Lost Time Adjust (s)		0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Total Lost Time (s)		4.5		4.5	4.5		4.5	4.5		4.5	4.5	
Lead/Lag												
Lead-Lag Optimize?												
Vehicle Extension (s)	3.0	3.0		3.0	3.0		3.0	3.0		3.0	3.0	
Recall Mode	None	None		None	None		Max	Max		Max	Max	
Walk Time (s)	7.0	7.0		7.0	7.0		7.0	7.0		7.0	7.0	
Flash Dont Walk (s)	11.0	11.0		11.0	11.0		11.0	11.0		11.0	11.0	
Pedestrian Calls (#/hr)	0	0		0	0		0	0		0	0	
Act Effct Green (s)		12.5		12.5	12.5		45.9	45.9		45.9	45.9	
Actuated g/C Ratio		0.19		0.19	0.19		0.68	0.68		0.68	0.68	
v/c Ratio		0.48		0.65	0.30		0.18	0.78		0.42	0.64	
Control Delay		18.6		40.0	12.7		6.8	14.8		14.0	9.9	
Queue Delay		0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Total Delay		18.6		40.0	12.7		6.8	14.8		14.0	9.9	
LOS		В		D	В		А	В		В	А	
Approach Delay		18.6			27.6			14.3			10.3	
Approach LOS		В			С			В			В	
Intersection Summary			and the second			a starting						
Area Type: (	Other											
Cycle Length: 70												
Actuated Cycle Length: 67.5												
Natural Cycle: 70												
Control Type: Actuated-Unco	ordinated											
Maximum v/c Ratio: 0.78												
Intersection Signal Delay: 14	.5			In	tersection	LOS: B						
Intersection Capacity Utilizati	ion 83.2%			IC	U Level o	f Service	E					
Analysis Period (min) 15												
Splits and Phases: 3: SR 5	52/Morning	icido Dr &	Adair Po	r								
		SILLE DI &	Audii Au									

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47.5 s	22.5 s
Ø6	<b>★</b> <i>Ø</i> 8
47.5 s	22.5 s

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# Intersection: 3: SR 52/Morningside Dr & Adair Rd

Movement	EB	WB	WB	NB	NB	SB	SB
Directions Served	LTR	L	TR	L	TR	L	TR
Maximum Queue (ft)	124	102	87	152	411	133	259
Average Queue (ft)	77	66	49	52	233	75	154
95th Queue (ft)	132	107	89	151	443	154	267
Link Distance (ft)	832		1050		608		547
Upstream Blk Time (%)					0		
Queuing Penalty (veh)					0		
Storage Bay Dist (ft)		185		185		212	
Storage Blk Time (%)					11	1	2
Queuing Penalty (veh)					6	9	2

# Network Summary

Network wide Queuing Penalty: 16